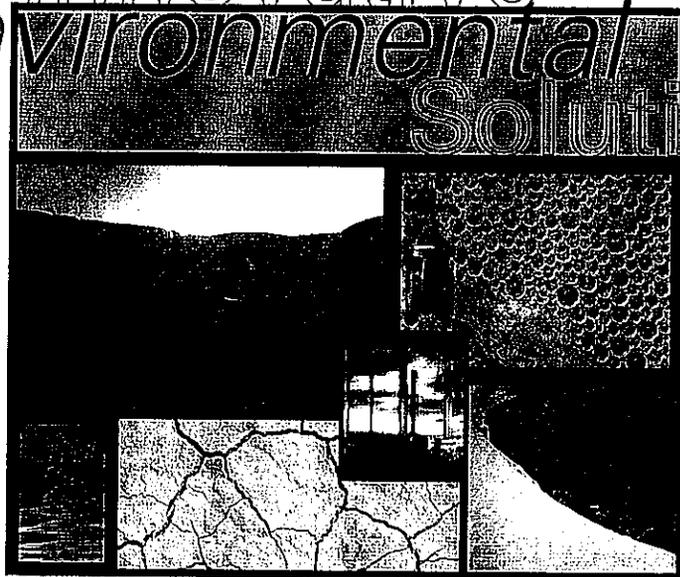


Appendix K

Post-mining Water Geochemistry Report

Innovative
Environmental
Solutions



Post-Mining
Groundwater Chemistry
Pogo Mine
Alaska



Adrian Brown
Groundwater Hydrology • Geochemistry • Remediation

Post-Mining
Groundwater Chemistry
Pogo Mine
Alaska

Prepared for:

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June 24, 2001

Project No. 1543A



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Teck Corporation is proposing to develop the Pogo gold orebody, located east of Fairbanks, Alaska, using underground mining methods. In the proposed development, the Pogo Orebody will be mined, and the mine void will be filled with cemented and uncemented tailings, being a mixture of flotation tailings and cyanide-processed tailings. After closure, the mine voids will refill with water, and groundwater will then flow through the backfill materials. Post-closure flow through the mine will be predominantly to the northwest. Groundwater will ultimately flow through the mine voids, and move slowly through the country rock. As this flow passes through the rockmass downgradient of the mine, the dissolved concentration of the constituents dissolved in the moving groundwater will reduce due to interaction with the bedrock, dilution, and dispersion. The groundwater flow will ultimately emerge in the alluvium of the Goodpaster River, and will there mix with the groundwater flowing in the alluvium. The combined seepage will finally be discharged to and mix with the flow in the Goodpaster River, at and downstream of the minesite.

Post-closure groundwater chemistry conditions have been quantified by modeled integration of groundwater hydrology information obtained from the site, the proposed development and closure strategy, and the chemical characteristics of the orebody, host rock, and backfill. In particular, chemical fate and transport parameters for key chemical species have been determined by testing of site materials with pore fluids released by the mine backfill materials; these parameters have been used in the evaluation.

As a result of discharges of dissolved species from the mine backfill, concentrations of dissolved species will be temporarily increased in bedrock groundwater downgradient of the mine. However, the hydraulic conductivity of the materials in this area has been shown to be sufficiently low as to prevent usable water supply flows to be obtained from these materials, and the pre-mining quality of these waters in general exceed drinking water standards. Accordingly, these changes are not considered to be significant due to the lack of accessibility and potability of the water.

The first locations where groundwater could be extracted for consumption or emerge at the surface are the alluvium of the Goodpaster River valley or the surface water flow of the Goodpaster River. The expected post-mining changes in concentration of selected key species in the alluvium and surface water of the Goodpaster River are presented in the following table, together with the time for the peak concentration to be reached:

| Parameter: | TDS | CN | As | Cd | Ni | Sb | Se |
|-------------------|------------|-----------|-----------|-----------|-----------|-----------|-----------|
| Slope (mg/L) | 291 | 0.023 | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 |
| Valley (mg/L) | 16 | 0.001 | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 |
| River (mg/L) | 1 | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 |
| Time (years) | 140 | 140 | 270,000 | 1,420,000 | 270,000 | 30,000 | 82,500 |

There are predicted to be small but generally undetectable elevations in concentrations of major ion species and metals in the alluvium and surface water of the Goodpaster River. The changes would occur in approximately a century for unretarded species (such as total dissolved solids and cyanide), to millennia for trace metals. In general, these predicted changes will not cause the water quality status in the alluvium or the Goodpaster River or the alluvium to change.

1. Introduction

Teck Corporation (Teck) is developing the Pogo Project, a gold mine and processing facility located 90 miles east of Fairbanks, Alaska. This project comprises an underground mine, a milling facility, and a surface dry-stack tailings storage facility. Mining will be by underground stoping; stopes will be backfilled with either cemented or uncemented tailings. After mining is completed, the mine will be decommissioned, the access drifts and shafts will be plugged, and the backfilled mine will be allowed to resaturate with groundwater. This report presents an evaluation of the post-closure impact of the mine to water resources in the vicinity of the mine.

2. Setting

2.1 Topography

The Pogo orebody is located on the east flank of the valley of the Goodpaster River, between Liese Creek and Pogo Creek (Plate 1). Surface drainage from the orebody area is primarily to Liese Creek.

2.2 Climate

The climate of the project is cold and dry. The average maximum summer temperatures are 68°F to 77°F. Temperatures of less than -40°F occur on an average of 14 days per year.

Precipitation is light. Teck believes site and regional data supports a precipitation estimate approximating 12 inches on an annual average. Published USGS maps for the region indicate a value of approximately 19 inches on an annual average. For the purposes of this evaluation, the 19-inch value will be used.

Evapotranspiration is highly seasonal, with a total annual evapotranspiration estimated to be 9.20 inches (EBA, 1998).

2.3 Geology

The geology of the orebody area has been evaluated in detail, based on surface drilling, installation of an underground exploration drift, and the drilling of in excess of 20,000 feet of underground exploration coreholes. The ore is located in two approximately parallel tabular quartz vein systems, averaging approximately 15 feet thick, and separated by approximately 400 feet vertically. The upper orebody is located approximately 400 feet below ground surface. The extent of the orebodies is indicated in Plate 1, and two sections through the orebodies are shown in Plate 3.

The quartz ore veins are located within a metamorphic rock package, of which the predominant rock type is gneiss. The geologic system is complexly folded and faulted (Teck, 1999).

The geologic investigation and inspection of the development drift indicates that there are large scale faults and fault zones located in the host rockmass; one major fault zone intersects the orebody from north to south (the Mid-Ridge Fault), and another appears to run approximately parallel to the

exploration drift. A structural feature also appears to lie approximately beneath Liese Creek (the Liese Creek Fault). These features have been intersected in underground exploration developments and underground drilling, and generally appear to be barriers to flow across the features (ABC, 2001). The Liese Creek Fault and the Mid-Ridge Fault strike approximately northwest, and have been identified as being associated with zones of enhanced permeability and measurable inflows to the underground openings, and to drill holes extending from those openings. The significance of these features to underground flow has been evaluated in detail in the mine inflow evaluation (ABC, 2001).

2.4 Groundwater

2.4.1 Groundwater Head and Flow

Before mining development, groundwater was encountered at a depth of approximately 300 feet below ground surface at the orebody location. The pre-mining piezometric surface in the site area has been determined based on the available data, and is shown on Plate 2. Permafrost is present above approximately this level on the north-facing slopes; intermittent permafrost exists on the south-facing slopes to approximately the same depth.

The groundwater contours show that the flow in the groundwater system is generally to the west-northwest, with flow from the mines passing through country rock, and ultimately entering the alluvial material in the valley of the Goodpaster River. Flow near the Liese Creek fault disrupts the general flow pattern in the vicinity of Liese Creek, resulting in a portion of the underground flow being captured in the alluvium of the creek. Based on pre-mining groundwater quality data (see Section 2.7.1 below), it appears that little bedrock flow enters the Liese Creek alluvium or surface flow.

2.4.2 Hydraulic conductivity

Testing of the site area hydrogeology has been performed over the life of the development. The testing programs that have been undertaken are as follows:

1. Alluvial area well tests (Golder, 1998; Teck-Sumitomo, 2000). A number of pumping tests of groundwater flow were conducted in 1998 to determine the availability of groundwater resources for project development, and the effects of injection of treated project discharge water to the alluvium of the Goodpaster River. In summary, the testing indicated that the hydraulic conductivity of the alluvial materials in the valley of the Goodpaster River averaged approximately 50,000 ft/yr¹, with a considerable range due to heterogeneities in the valley fill materials.

¹ The units used for hydraulic conductivity in this report are feet per year (ft/yr). This is consistent with the use of the Imperial unit system for the report. Conversion to metric units can be made using the following factors:

$$1 \text{ ft/yr} = 1.0 \times 10^{-6} \text{ cm/sec}$$

$$1 \text{ ft/yr} = 1.0 \times 10^{-8} \text{ m/sec}$$

2. Surface well tests of bedrock (Golder, 1998). During the drilling of the surface exploration program, a total of 41 hydrogeology tests were performed exploration coreholes, in particular those that were vertical. This testing comprised hydraulic conductivity testing using packer technology, and installation of permanent completions to allow measurement of groundwater pressure. The tested holes were concentrated in the vicinity of the orebodies. The median hydraulic conductivity of the rock evaluated in these tests was 5 ft/yr, with values ranging from 0.01 ft/yr to 500 ft/yr. In general the higher values were encountered in the rock down to 500 feet below ground surface, and the lower values were encountered at deeper levels, in the vicinity of the orebody.
3. Tailings area tests (Agra, 1999). The shallow bedrock in the vicinity of the proposed paste tailings disposal area to the southeast of the orebody has been extensively tested for hydraulic conditions, using tests in a total of 14 drill holes. The conductivity is approximately an order of magnitude higher than the deeper rock values, with an arithmetic mean hydraulic conductivity of approximately 50 ft/yr.
4. Underground testing (ABC, 2001). As a part of the study that comprised this evaluation, extensive testing of the rockmass was undertaken from the underground exploration drift system. This testing comprised measurement of flow and water quality to the drift, and testing of a total of in excess of 50 drill holes. This testing comprises both single-hole flow tests and multi-well flow response tests. The geometric mean hydraulic conductivity from the single-hole tests was 4.9 ft/yr, with a median of 19 ft/yr. Most of these drill holes intersected the relatively high permeability ore materials, which range in hydraulic conductivity from 10-100 ft/yr, while hydraulic conductivities measured in holes drilled in country rock range from 0.1 to 1 ft/yr.

The results of analysis of all the bedrock test data are presented in cumulative form in . The gneiss rocks that characterize the site have a low effective hydraulic conductivity; for this evaluation a range of 0.2 ft/yr to 0.75 ft/yr has been used, to reasonably bracket the impact of transport of dissolved constituents to the Goodpaster Valley. Within these rocks are located the tabular quartz veins that comprise the orebody, which have a relatively high hydraulic conductivity in the order of 100 ft/yr; before mining these units acted as conduits for groundwater flow within the system. However, this material is largely removed and replaced by backfill during mining, so its characteristics are replaced by the characteristics of the backfill.

2.4.3 Storage characteristics

Groundwater storage in the alluvial materials is expected to be high; a value of 30% is assumed for the purpose of computing volume of water in the alluvium.

Groundwater storage in the rockmass is limited. Based on the response of the groundwater system to the driving of the access decline for underground development, the drainable porosity of the rock appears to be in the order of 0.3% (ABC, 2001). Based on testing being performed in the underground development, the drainable porosity of the rockmass appears to be in the order of 0.1% (ABC, 2001). These relatively low values are consistent with the generally low hydraulic conductivity of the rockmass.

2.5 Surface Water

The site is located adjacent to and east of the Goodpaster River. To the north of the orebody is Liese Creek, and to the south is Pogo Creek. Both creeks are considered to be perennial, although surface flow does not always occur in the stream channels, due to flow in the moderate to highly permeable valley fill sediments, and due to infiltration into fan deposits at the mouths of each creek.

Regional evaluations indicate that the flow in streams is related to catchment area. Average streamflow is estimated to total the equivalent of 7.46 inches annual runoff (EBA, 1998). Most of the runoff occurs in the spring freshet. Flow in the Goodpaster River has been gauged downstream of the Pogo site at Big Delta since 1998. For the period of August 1998 to September 2000, the average flow in the Goodpaster River for the 677 square mile catchment has been 356 cubic feet per second (cfs), which is the equivalent of 7.15 inches per year of productivity.

Baseflow in streams in the area has been evaluated using stream flows in the period December to March, when surface flow to the streams is at a minimum, and most of the streamflow is expected to be the result of emerging groundwater. Using the baseflow as a gauge of deep groundwater infiltration, stream baseflow is estimated to be equivalent to a production rate of 1.0 inches per year (ABC, 2001).

Baseflow in the Goodpaster can be estimated from the three years of available record. For the months of January through March, the average flow in the Goodpaster (at Delta Junction, downstream of the site) is 33.3 cfs, which is the equivalent of 0.67 inches per year basin productivity. For the lowest flow month (March), the average flow is 24.8 cfs, or 0.50 inches per year.

2.6 Water Quality

A large number of water quality samples have been taken at the Pogo Project. These samples include coverage of the surface water in the Goodpaster River, the groundwater in the Goodpaster Alluvium, groundwater in the country rock, and groundwater in the orebody materials. A summary of the average water quality for waters of significance to this evaluation is presented in Table 2.

Surface water quality in the project area is good. The surface water is calcium-sulfate dominated, with total dissolved solids content of approximately 70 mg/L. Dissolved metal concentrations in the surface water are generally below or close to detection levels.

Groundwater in the valley sediments at the site area has a somewhat higher dissolved content, grading from 600 mg/L near the valley slope ("slope alluvium") to 300 mg/L near the river ("valley alluvium"). The chemistry of these waters is predominantly calcium-magnesium-bicarbonate-sulfate, with some iron and traces of other metals.

Groundwater in the gneiss rock away from the orebody is higher in dissolved solids with approximately 550 mg/L TDS. The water is calcium-magnesium-sulfate-bicarbonate water, and is hard. Arsenic is present in the water, at a concentration in the order of 0.05 mg/L. Other metals are predominantly below detection levels in this water.

Groundwater from locations where there is no orebody displays moderate dissolved solids content, with approximately 500 mg/L TDS. This is calcium-magnesium-sulfate-bicarbonate water, and is quite hard.

Arsenic is somewhat elevated in this water, averaging 0.05 mg/L. Some other metals are also present in the water at low levels, in particular iron, aluminum, cobalt, strontium, and zinc.

Groundwater in and near the orebody displays the highest dissolved solids content of all project waters, with approximately 1000 mg/L TDS calcium-magnesium-sulfate-bicarbonate water, and is very hard. Arsenic is elevated in this water, at concentrations ranging between 0.5 mg/L to 4 mg/L, and averaging around 1.6 mg/L. Some other metals are also present in the water at low levels, in particular zinc.

2.7 Water Dating

In order to obtain an understanding of the flow regime that exists at the Pogo site, a program of isotopic sampling and evaluation was performed in February 2001. Samples of water were taken from surface streams, shallow monitor wells, deep monitor wells, and from inflows to the underground exploration facility, and sent for chemical and isotopic analysis. The results are presented below (for species that showed significant differences between sample locations):

| LOCATION | 00U098C | 00U098D | 00U099 | 00U100 | LT-009 | SW-23 |
|--------------------------------------|--|---|--|--|--|-----------------------------|
| DESCRIPTION | Under-ground hole to Liese Creek Fault (high flow) | Under-ground hole to Liese Creek Fault (low flow) | Under-ground geology-drain hole near Mid-Ridge Fault | Under-ground geology-drain hole near Mid-Ridge Fault | Shallow alluvial well beside Liese Creek | Goodpaster River above Camp |
| DATE | 26-Feb-01 | 26-Feb-01 | 26-Feb-01 | 26-Feb-01 | 25-Feb-01 | 28-Feb-01 |
| Tritium | 15.80 | 1.34 | 13.70 | 13.00 | 15.40 | 16.20 |
| $\delta^{18}\text{Oxygen}$ (per mil) | -19.90 | -19.45 | -20.08 | -19.90 | -19.42 | -20.22 |
| $\delta^2\text{Hydrogen}$ (per mil) | -159.31 | -155.04 | -158.22 | -158.56 | -160.90 | -160.49 |
| COND-L ($\mu\text{S}/\text{cm}$) | 477 | 1540 | 503 | 521 | 267 | 140 |
| pH-L (pH units) | 7.93 | 7.78 | 7.91 | 7.96 | 7.94 | 7.84 |
| TDS (mg/L) | 292 | 1150 | 315 | 311 | 167 | 82 |
| ALK-T (mg/L) | 168 | 441 | 170 | 168 | 98 | 47 |
| SO4 (mg/L) | 99 | 510 | 113 | 119 | 41 | 18 |
| NO3 (mg/L) | 0.044 | 0.005 | 0.005 | 0.005 | 1.1 | 0.365 |
| CA-D (mg/L) | 51 | 148 | 40 | 41 | 40 | 16 |
| MG-D (mg/L) | 24 | 113 | 33 | 35 | 8 | 4 |
| NA-D (mg/L) | 10 | 37 | 13 | 15 | 3 | 3 |
| AS-D ($\mu\text{g}/\text{L}$) | 108 | 2930 | 150 | 217 | 3.8 | 0.1 |
| FE-D (mg/L) | 0.14 | 2.48 | 0.22 | 0.38 | 0.03 | 0.03 |
| MN-D ($\mu\text{g}/\text{L}$) | 62 | 32 | 32 | 23 | 1 | 4 |
| SR-D ($\mu\text{g}/\text{L}$) | 978 | 7200 | 1250 | 1330 | 155 | 86.1 |

2.7.1 Chemical Analysis

The chemical analyses indicate that the pre-mining concentration of constituents in the subsurface increase as the orebody is approached. The pre-drainage orebody groundwater had water quality that is

indicated by the underground drain hole 00U98D, a low flow hole drilled into an undisturbed area northeast of the exploration development. This water is mineralized, with 1540 mg/L TDS, and a range of dissolved minerals.

The remainder of the water chemistry indicates that the water entering the underground through the exploration holes (which have in general been allowed to drain for the last year or more) are relatively good quality, suggesting recent introduction of that water from the surface. This is consistent with the head information obtained in wells in the vicinity of the underground development, which show that the water table near the underground workings has dropped to a location close to the elevation of the workings.

Finally, the water in the alluvial well close to Liese Creek contains low concentrations of dissolved solids. This indicates that the groundwater in this location is predominantly derived from surface water, with only a small component of deep bedrock groundwater discharge to the alluvium (less than 25%). Liese Creek is in a groundwater discharge location, based on the groundwater level data, so it was expected that in the winter period when the sample was taken, bedrock groundwater discharge would dominate the quality of the water in the alluvium, as there would be no surface water flow available to dilute the discharge to the alluvium from the bedrock. The results indicate that there is only limited outflow of groundwater from the bedrock system to the alluvium, which is consistent with the observed low inflow to the underground workings, the low hydraulic conductivities measured in the country rock at the site, the low computed infiltration to the bedrock system, and the low baseflow from the bedrock in the region.

2.7.2 Stable Isotopic Evaluation

The abundances of stable isotopes of hydrogen and oxygen were evaluated for each of the samples taken. The results are compared with the isotopic abundances from Standard Mean Ocean Water (SMOW), and are expressed as differences in parts per thousand (per mil). The data for both the hydrogen and oxygen isotopes of water indicate that the waters are of very similar origin, and have not been significantly altered differentially by evaporation or other processes that would alter the isotopic abundances of the water.

The only water that is somewhat different isotopically is the sample from the low-flow underground hole, 00U98D. This water appears to have been introduced to the groundwater system when the precipitation was somewhat isotopically lighter than it has been in recent times. As it takes significant climatic changes to alter long-term precipitation isotopic abundances in a given location, this difference suggests that this may be considerably older than the other water in the system (perhaps hundreds or thousands of years).

2.7.3 Tritium Evaluation

Tritium is an unstable isotope of hydrogen, and has a half-life of 12.4 years. It was introduced into the atmosphere in large quantity as a result of atmospheric testing of thermonuclear devices from 1952 to 1965. Tritium levels in precipitation peaked in the mid-1960s, at levels in excess of 1,000 tritium units (TU) worldwide. Today, tritium in precipitation varies, but ranges from 10 to 20 TU. Water that has

been in the groundwater system for more than 50 years (i.e. pre-bomb water) has essentially no tritium, due to the low pre-bomb tritium levels (estimated at 5 TU), and subsequent decay.

The tritium testing results provide the following conclusions:

1. Surface water (and presumably precipitation) at the Pogo site has about 16.2 TU.
2. Water in the Liese Creek alluvium has about 15.4 TU, which suggests that this is approximately 5% bedrock water (old) and 95% surface water (new).
3. Groundwater in the vicinity of the underground development, which has been subjected to drainage, has about 13.5 TU, which suggests that it is approximately 20% old water, and 80% new. This would be the result of removal of the old stored water by the drainage, and drawing of water infiltrated in the last 50 years into the drainage system.
4. Groundwater in the vicinity of the Liese Creek fault has about 15.8 TU, which is close to the tritium content of surface water, and higher than the Liese Creek alluvial water. This indicates that this water is largely surface water that has been transported through the Liese Creek fault from the Liese Creek alluvium and Liese Creek to the drainhole, and also indicates that the water removed from the drain hole has been sufficient to remove the (old) pre-exploration water from the fault.

The tritium data indicates that the Liese Creek fault is permeable, and acts as a conduit for surface water to enter subsurface workings when they intersect it. It also demonstrates that the drainage that has taken place to date in the vicinity of the underground exploration has been effective in removing stored water from the system in that area.

2.8 Mining and Ore Processing

Mining is currently planned to remove gold ore from two orebodies, the L1 and L2, the locations of which are shown on Plate 1. These orebodies are tabular, approximately 15 feet thick, and dip at approximately 30° to the northwest. They are separated by approximately 400 feet of country rock, with the L2 being stratigraphically below the L1. Mining will be by underground stoping, and will involve essentially total extraction of the orebody materials.

The ore produced by mining will be ground and processed using flotation to produce a sulfide concentrate, which will comprise approximately 10% of the material processed. The flotation underflow will be thickened and filtered to produce a flotation tailing paste. The concentrate will be reground and processed to extract gold by cyanidation. After cyanidation, and the resulting sulfide waste will be processed to remove cyanide, and dewatered to form a sulfide-bearing tailing fraction. This will be mixed with flotation tailings in the ratio of approximately 1 part sulfide tailings to 4 parts flotation tailings, and the resulting mixture will be used for cemented and uncemented backfill for the underground mine. The remaining (non-sulfide) flotation tailings paste will be disposed of in a surface facility located in Liese Creek (Plate 1).

The underground mine voids will be backfilled with cemented and uncemented tailings material. At closure, all remaining underground openings will be backfilled, and all access openings (shafts, declines) will be plugged.

The quality of water that will be entrained in the backfill after closure has been tested and evaluated, and the results of this reconstruction are presented in Table 2. The interstitial water will have concentrations of TDS, pH, alkalinity, arsenic, molybdenum, and nickel that will be higher than currently exist in the groundwater in the orebody.

3. Evaluation Method

3.1 Approach

The post-mining groundwater chemistry evaluation has been performed using a mixing-cell geochemical transport model. This model is as follows:

1. The flow domain from the mine to the Goodpaster River is subdivided into a series of twelve cells, starting at the L2 orebody location, passing through the L1 orebody location, and proceeding through the river alluvium to the river, which is the final cell.
2. Groundwater flows downgradient from cell to cell at a rate consistent with the actual flow in the system, with infiltration to the ground surface in the location of each cell being added to the flow within the cell. In some cells, flow into the cell from the side ("side flow") is also considered (for example flow in the Goodpaster alluvium). The side flow is considered to enter the cell at right angles to the overall groundwater flow system, and then flows downgradient within the cell flow system, adding to the flow rate in the direction of the groundwater flow from the mine to the river.
3. While the water is within each cell, it is mixed and equilibrated with the solid phase material in that cell, resulting in either the uptake of chemical constituents to the liquid phase from the solid phase, or the transfer of chemical constituents from the liquid on the solid phase.
4. Water moves downgradient from cell to cell, with the water ultimately discharging from the last cell of the model (the Goodpaster River opposite the minesite) to the Goodpaster River downstream of the minesite location.

The mixing cell model has been built within a Microsoft Excel Spreadsheet Workbook. A copy of the workbook containing the mixing cell model, and summaries of the results of all the analyses performed for this evaluation, is provided in Attachment 2 to this report.

3.2 Chemistry

3.2.1 Chemical Process Modeled

The chemical processes that are modeled are:

1. Mixing. Mixing of groundwater within each cell is modeled as a conservative process, in which all constituents are assumed to remain in solution after the mixing occurs.
2. Adsorption. Adsorption of constituents onto the solid phase materials in each cell is modeled as a first-order linear, reversible equilibrium process. The process is controlled by the lumped

distribution coefficient (K_d) for each constituent and each solid phase material. K_d values have been determined by laboratory experiment for the Pogo site materials and key chemical constituents. Distribution of constituents between the solid phase and the liquid phase is governed by the following equation:

$$\text{Concentration in solid phase (mg/kg)} = K_d * \text{Concentration in the liquid phase (mg/L)}$$

No other chemical processes are explicitly modeled, although the laboratory determination of the lumped parameter K_d may include the effects of processes in addition to adsorption, including oxidation, reduction, dissolution, and precipitation. Assuming that all the removal of material from solution in the laboratory testing is reversible is in general conservative with respect to impact of dissolved materials on groundwater, in that many of the chemical processes that actually occur in the groundwater transport system have the effect of permanently removing chemical mass from the transport system, reducing the dissolved concentration of the constituents that precipitate. Oxidation of sulfides is not considered, because it is not expected that significant oxidation will occur in the mine voids after closure and refilling.

The possibility that chemical constituents might dissolve from the backfill in perpetuity has been considered by performing some analyses using a very high K_d in the mine backfill material. This has the effect of creating an essentially permanent source of dissolved constituents at the mine location.

3.2.2 Adsorption behavior

The effective adsorption behavior of the constituents of concern in the groundwater evaluation was established by laboratory testing of the materials found at the minesite, using liquors that simulate those that are expected to be created by the mine backfilling process. The laboratory testing performed, and the results obtained, are presented in detail in Attachment 1. In summary, the testing involved the following:

1. Crushing of the rock cores of site material.
2. Contacting the crushed material with synthetic liquor that approximates the fluids that will be encountered at the minesite, in particular lixiviant from the milling and cementing processes.
3. Measuring the changes in the concentrations of the constituents of concern in the liquor after contact with the crushed rock.
4. Computation of the distribution coefficient for the constituent and the rock type tested.

This process was carried out for the following cases:

1. The range of pH encountered or expected in the Pogo system.
2. A range of grainsizes of the test sample (to allow application to the rockmass).
3. The range of ionic strength solutions expected at the site.
4. The range of rock types found at the site.

In addition, the site rock materials were tested for leachable metal constituents using a distilled water lixiviant, to determine if any of the metals of concern were capable of being leached from the site rocks (as distinct from the mine backfill materials).

The results of the distribution coefficient testing were used to develop the values that are used in the model; these are presented in Table 1.

3.2.3 Rock and water chemistry

The water chemistry for the components present at the Pogo site was developed from information obtained at the site, and during testing of the tailings. The components are:

1. Cemented and uncemented backfill. Backfill materials were crushed and tested by leaching². The original concentrations of constituents in the interstitial waters in the original backfill materials were computed by re-concentrating the constituents measured in the initial leach of these materials in the humidity cell tests back into the original moisture content in the sample³.
2. Country rock. The water quality in the country rock (that is non-ore rock) was evaluated from analyses of water samples from wells completed in the rock remote from the orebody.
3. Alluvium. Alluvial water quality in the Goodpaster Valley was evaluated from tests of water sampled from alluvial wells located upgradient from disposal wells at the minesite.
4. Goodpaster River. Water quality in the Goodpaster River was evaluated from tests of surface water samples taken above and below the minesite during the exploration period.

Rock chemistry was determined by aquaregia digestion tests of the rock material.

The results are presented in Table 2.

3.3 Model

3.3.1 Construction

The model comprises twelve cells, arranged sequentially as shown conceptually in

. The cells are in general tabular, inclined at 30 degrees from the horizontal, generally parallel with the orebodies and with the steeper surface slopes in the mine area. The cells are oriented normal to the groundwater flow. Details of the cellular transport model are presented in Attachment 2.

² The samples were taken in the initial flush of Humidity Cell Tests of all the materials relevant to the study. This is a 20:1 leach with distilled water, which is considered to remove all the leachable material from the sample, and to leave only a very limited amount of soluble material adsorbed to the backfill material.

³ It is recognized that in concentrating the leached constituents back into the original porewater volume, some of the constituent concentrations may exceed the solubility of those constituents in the porewater solution. Assuming that all constituents remain soluble in the original porewater in the re-concentrated solution is conservative in that it maximizes the concentrations that will report to the receiving waters in the system.

3.3.2 Input Parameters

Input parameters for the modeling comprise a “base” case value, which is considered to be the value of the parameter that best reflects the actual behavior of the site area. In addition, an upper and lower value has been selected to characterize the range of each parameter; these values represent the reasonable range of the parameter that could occur at the site. These ranges in general include most of the available data, and are used in sensitivity evaluations of the system.

The parameters for the model were as follows:

1. **Geometry.** The model domain was divided 12 cells, in order to subdivide the model volume into discrete analysis portions. The cells represented (from upper to lower): the L2 backfilled mine (15 ft thick); the L1-L2 interburden (400 feet thick); the L1 backfilled mine (15 feet thick); country rock downgradient of the mine (6 cells totaling 2,800 ft thick); the alluvium of the Goodpaster River valley close to the slope (the “slope alluvium”, 100 feet thick); the alluvium of the Goodpaster River valley close to the river (the “valley alluvium”, 100 feet thick); and the Goodpaster River itself. Each cell was 2000 feet wide (i.e. the horizontal dimension normal to the flow direction), while thicknesses and depths varied according to the real material dimensions.
2. **Hydraulic conductivity.** The following conductivity values were selected:
 - a. **Country Rock.** Based on measurement and the results of calibration of the Pogo flow model (ABC, 2000; ABC, 2001), the hydraulic conductivity of the bedrock was found to be between 0.2 ft/yr and 0.75 ft/yr; the base case value used in this evaluation was 0.5 ft/yr. This value enters into the analysis only in the computation of flow from rock above the modeled domain into the uppermost cell of the model; that is above the location of the L2 orebody.
 - b. **Slope Alluvium.** A base case hydraulic conductivity value of 2,000 ft/yr was used for the slope alluvium; the range used was 1,000 ft/yr to 5,000 ft/yr. These values are somewhat lower than measured values of hydraulic conductivity for alluvium, reflecting the expectation that alluvium close to the edge of the valley will be less permeable than alluvium in the center of the valley, for which data have been obtained. This value enters into the evaluation only in the computation of the “side” flow in the portion of the alluvium close to the edge of the valley.
 - c. **Valley Alluvium.** A base case hydraulic conductivity value of 40,000 ft/yr was selected for the valley alluvium, which is the approximate average of measured values for the hydraulic conductivity of the alluvium. The range of values is from 5,000 ft/yr to 72,000 ft/yr. This value is only used to compute the “side” flow in the portion of the alluvium adjacent to the river.
3. **Porosity.** The following base porosity values and porosity ranges were used for the transport analysis:
 - a. **Rock:** 0.3% (0.1%-0.5%)
 - b. **Backfill:** 25% (20%-50%)

- c. Alluvium: 30% (25%-40%)
4. Infiltration: A base infiltration rate of 0.5 inches per year was selected, based on the productivity of the Goodpaster River and other information (ABC, 2001). The infiltration range selected was 0.18 in/yr to 0.75 in/yr, based on modeling and other evaluations of the flow at the Pogo site (ABC, 2000; ABC, 2001).
5. Goodpaster River flow. The Goodpaster River flow passes through the final cell in the model as "side" flow. The flow rate used for this evaluation is 33.3 cfs (14,952 gpm), the average low flow measured at Big Delta for the period of record.

3.3.3 Source Term

3.3.3.1 Expected source term

The expected source term for each constituent is set equal to the amount of each constituent that is leachable from the backfill material, using a 20:1 distilled water leach. This leachate was obtained in the first flush of the Humidity Cell Tests for the site materials, as noted above. The concentration used in the analysis was computed by numerically re-concentrating the constituents obtained in the leachate back into the moisture content in the original sample. The source concentrations of constituents thus computed are presented in Table 3, along with the computed K_d values used in the analysis. As this is considered to be the total amount of source constituents in the backfill, in the expected case analysis the backfill is given a K_d of zero, so that no additional material will be adsorbed onto the backfill (in the computation). This is equivalent to assuming that no further material is produced by, or leachable from, the backfill material.

3.3.3.2 Maximum source term

It is possible that after removal of the soluble materials from the backfill, long-term dissolution and/or decomposition of some of the solids in the backfill may occur. In particular, dissolution of the cementitious material used in the backfill might occur in the very long term. The maximum amount of source term material that could be dissolved has been computed for each constituent from the information in Table 3, using the following assumptions:

1. TDS. It is assumed that all the calcium and magnesium would be dissolved from the matrix as their respective carbonates, along with the arsenic as arsenite.
2. Metals. It is assumed that the maximum source term for each metal analyzed is the amount of metal that can be mobilized by aquaregia digestion.

As the source constituents will be leached from the backfill material, in the computation the source term was cast in terms of effective K_d (distribution coefficient) values. To achieve this, the computed available solid-phase source concentration for each constituent was divided by the computed concentration of each constituent in the interstitial liquid of the backfill material. These maximum source concentrations of constituents evaluated in this analysis are presented in Table 3, along with the computed K_d values used in the analysis. This computational approach has the effect that the constituents are removed or displaced from the backfill initially at the concentration that is computed to

exist at mine closure time. Thereafter, the constituents that are computed to be available in the long term are removed from the backfill into the groundwater, at gradually decreasing concentrations, until all the potentially mobilizable materials are transported into the downgradient groundwater system.

4. Results

4.1 Constituents Evaluated

The model was run for seven chemical species: TDS, cyanide, arsenic, antimony, cadmium, nickel, and selenium. The selected parameters were based on those that were significantly present in the backfill material, and those for which drinking water and cold water aquatic standards were low. All other parameters have no human health or environmental impact potential at the concentrations at which they are present at source. The rationale for selection of these parameters is presented in more detail in the Bench Scale Testing Report (Attachment 1).

4.2 Flow

The flow conditions in the model are summarized as follows (for the expected case; flows are similar in all cases):

1. Groundwater inflow from above the mine. The expected groundwater inflow above the mine is computed to be 7 gallons per minute (gpm) through the mine cross-section.
2. Infiltration to the flow pathway. Infiltration from the ground surface takes place along the entire flow from the mine to the river. Total infiltration to the flow system in the expected case is 3 gpm. This water results in dilution of the mine water by approximately 1.4:1 by the time the flow exits the bedrock system.
3. Slope alluvial flow. The flow entering the slope alluvium from the bedrock is approximately 10 gpm. In the slope alluvium cell it mixes with a flow of 28 gpm in the alluvium from up-river. This mixing results in a dilution of the incoming rock water of 4:1, and a dilution of the original mine water of about 5:1. All outflow from the cell is assumed to be towards the river⁴.
4. Valley alluvial flow. The alluvial flow in the center of the valley is computed to be approximately 1,140 gpm in the expected case, moving parallel to the river in the vicinity of the mine. This flow is assumed to mix with the 38 gpm of flow from the slope alluvium, resulting in a dilution at mixing of 30:1, and a total dilution of the original mine water of 170:1.
5. River flow. The expected flow in the Goodpaster River is 33.3 cubic feet per second, or approximately 15,000 gpm. This is the approximate low flow for the river. A total of 1,178 gpm of groundwater flows out of the valley alluvium into the river opposite the minesite in the

⁴ It is recognized that in the real situation most of the discharge from the cell would be as groundwater flowing parallel to the river. However the model discharges all the flow from each cell toward the river, to ensure that in the model all the chemical mass from the vicinity of the mine is discharged into the river adjacent to the minesite. This assumption produces the greatest computed concentration changes in the river alluvium and the river, so is conservative.

expected case. The river water dilutes this water by a (minimum) factor of approximately 13:1. As the original mine water is already diluted in the incoming water by a factor of 170:1, the total (minimum) dilution of the mine water seepage in the river opposite the mine is approximately 2,300:1. These dilutions are minima because the river flow used is the minimum.

4.3 Expected Case

The “expected case” evaluation comprises the expected condition for the post-mining groundwater and surface water effects resulting from the mining and backfilling of the Pogo Mine. This case uses the expected values of each of the parameters that control post-closure groundwater system behavior, and the expected source term for each constituent. The results are presented for each of the constituents considered.

The analyzed maximum increases in concentration in the groundwater flow system after the cessation of mine operation and backfilling are summarized by species in the following table.

| Location | TDS | CN | As | Cd | Ni | Sb | Se |
|---------------------|------|--------|---------|-----------|---------|--------|--------|
| | mg/L | mg/L | mg/L | mg/L | mg/L | mg/L | mg/L |
| Backfill | 5158 | 0.4 | 4.4 | <0.001 | 0.348 | 0.052 | 0.049 |
| Bedrock (mid-path) | 2591 | 0.20 | 0.001 | <0.001 | <0.001 | <0.001 | <0.001 |
| Slope Alluvium | 291 | 0.023 | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 |
| Valley Alluvium | 16 | 0.001 | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 |
| River | 1 | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 | <0.001 |
| Years to reach peak | 140 | 140 | 270,000 | 1,420,000 | 270,000 | 30,000 | 82,500 |

These changes result in the following peak concentrations in the indicated locations:

| Location | TDS | CN | As | Cd | Ni | Sb | Se |
|---------------------|------|--------|---------|-----------|---------|--------|--------|
| | mg/L | mg/L | Mg/L | mg/L | mg/L | mg/L | mg/L |
| Backfill | 5691 | 0.4 | 4.5 | <0.001 | 0.363 | 0.053 | 0.050 |
| Bedrock (mid-path) | 3124 | 0.20 | 0.053 | <0.001 | 0.015 | 0.001 | 0.001 |
| Slope Alluvium | 892 | 0.023 | 0.053 | <0.001 | 0.002 | <0.001 | 0.002 |
| Valley Alluvium | 310 | 0.001 | 0.030 | <0.001 | 0.002 | <0.001 | 0.001 |
| River | 71 | <0.001 | 0.006 | <0.001 | 0.001 | <0.001 | 0.001 |
| Years to reach peak | 140 | 140 | 270,000 | 1,420,000 | 270,000 | 30,000 | 82,500 |

The results indicate that there will be some increase in concentrations of species at and close to the backfilled mine, but these effects are expected to reduce rapidly with distance away from the mine. None of these changes in water concentration would cause a change in the use of the water, or would cause the water to exceed relevant regulatory standards.

4.3.1 TDS

After closure and refill of the mine voids, materials dissolved in the backfill will be transported downgradient through the flow system by groundwater flow, resulting in increases in dissolved solids content downgradient of the mine. The amount of soluble material at source has been computed by reconcentrating the dissolved solids in a leached sample back into the moisture content of the original sample.

Total dissolved solids concentrations that are expected in the backfill are 5,691 mg/L, which is computed from the results of initial leaching of humidity cell testing. This concentration is 5,158 mg/L higher than the average TDS in groundwater in the country rock. In the Goodpaster alluvium against the valley wall, the increase in TDS is computed to be 291 mg/L; this would occur in a location where the groundwater naturally exceeds the TDS drinking water standard. The effect of this water quality change would be to somewhat increase the area of the alluvium where the TDS exceeds the secondary drinking standard of 500 mg/L (which the slope alluvium currently exceeds in places). A small increase of 16 mg/L is computed to occur in the alluvium beside the Goodpaster River, while there is computed to be no detectable concentration change in the Goodpaster. The results are presented in Figure 3.

4.3.2 Cyanide

Total cyanide concentrations are expected to be relatively low in the backfill: an average of 0.4 mg/L in the interstitial liquid (cyanide destruction will reduce the concentration of cyanide to 2 mg/L concentration in the sulfide fraction; this is 20% of the backfill material). It is assumed that the same concentration will exist in the backfill solids. Based on this input, the peak concentration of cyanide in the slope alluvium is computed to be 0.023 mg/L, and in the valley alluvium is 0.001 mg/L. Neither value approaches the drinking water concentration of 0.200 mg/L. No measurable change is expected in the Goodpaster River. It is computed that these peak values will be reached approximately 140 years after the end of the mining.

4.3.3 Arsenic

Arsenic concentrations in the interstitial waters in the backfill are expected to be high: nearly 4.5 mg/L. This dissolved arsenic will be displaced from the backfill with the seepage through the mine, and will migrate slowly towards the Goodpaster River, as arsenic is strongly adsorbed to the rockmass materials. Changes in the concentration of arsenic are expected to be undetectable in the slope alluvium, the valley alluvium, and the river; any change would take approximately 270,000 years to reach its peak, due to the high attenuation of arsenic in this system. The computed change in arsenic concentration in the river in the expected case is provided as Figure 4.

In the actual system, essentially no arsenic will actually be transported through this system to the alluvium. The actual source will be significantly lower than the maximum source, and in the long period of travel it is likely that geochemical processes not evaluated in the testing will occur which would result in the removal of arsenic from the groundwater. This is occurring now; the pre-mining information indicates that elevated arsenic only occurs in the groundwater system close to the orebody.

4.3.4 Other Metals

All the other metals evaluated for the expected case have no detectable increase in concentration in the alluvium or the water of the Goodpaster River. All changes are below 0.001 mg/L, which would be below any detectable levels when compared with the background metal levels in the river.

4.4 Maximum Source Case

Greater geochemical impacts result if the maximum source term is assumed for the backfill material. The summary of the changes in concentration for selected parameters for this case are presented below:

| Location | TDS | CN | As | Cd | Ni | Sb | Se |
|---------------------|-------|--------|-----------|-----------|-----------|---------|---------|
| | mg/L | mg/L | mg/L | mg/L | mg/L | mg/L | mg/L |
| Backfill | 5158 | 0.400 | 4.432 | <0.001 | 0.348 | 0.052 | 0.049 |
| Bedrock (mid-path) | 4520 | 0.334 | 3.893 | <0.001 | 0.305 | 0.046 | 0.042 |
| Slope Alluvium | 576 | 0.042 | 0.496 | <0.001 | 0.039 | 0.006 | 0.005 |
| Valley Alluvium | 32 | 0.002 | 0.027 | <0.001 | 0.002 | <0.001 | <0.001 |
| River | 2 | <0.001 | 0.002 | <0.001 | <0.001 | <0.001 | <0.001 |
| Years to reach peak | 1,000 | 280 | 1,600,000 | 3,200,000 | 1,400,000 | 300,000 | 450,000 |

These changes result in the following peak concentrations in the indicated locations:

| Location | TDS | CN | As | Cd | Ni | Sb | Se |
|---------------------|-------|-------|-----------|-----------|-----------|---------|---------|
| | mg/L | mg/L | Mg/L | mg/L | mg/L | mg/L | mg/L |
| Backfill | 5691 | 0.400 | 4.482 | 0.000 | 0.363 | 0.053 | 0.050 |
| Bedrock (mid-path) | 5053 | 0.334 | 3.943 | 0.000 | 0.320 | 0.046 | 0.043 |
| Slope Alluvium | 1,177 | 0.042 | 0.549 | 0.000 | 0.041 | 0.006 | 0.007 |
| Valley Alluvium | 326 | 0.002 | 0.057 | 0.000 | 0.005 | 0.000 | 0.001 |
| River | 72 | 0.000 | 0.008 | 0.000 | 0.001 | 0.000 | 0.001 |
| Years to reach peak | 1,000 | 280 | 1,600,000 | 3,200,000 | 1,400,000 | 300,000 | 450,000 |

4.4.1 TDS

Under the maximum source term assumption, the TDS concentration in the backfill is still 5,691 mg/L. In the Goodpaster slope alluvium the increase in TDS is computed to be 576 mg/L, in the valley alluvium it is 32 mg/L, and in the river it is 2 mg/L. If this maximal source term were to occur, TDS would somewhat increase the area of the alluvium where the TDS currently exceeds the secondary drinking standard of 500 mg/L (which the slope alluvium currently exceeds in places). The increases in the valley alluvium and the river would not be detectable due to current variations in TDS. The results of the maximum source analysis for TDS are presented in Figure 5.

4.4.2 Cyanide

The peak concentration of cyanide in the slope alluvium for the maximum source is computed to be 0.042 mg/L, and in the valley alluvium is 0.002 mg/L. Neither value approaches the drinking water

concentration of 0.200 mg/L. No measurable change would occur in the Goodpaster River. It is computed that these peak values will be reached approximately 280 years after the end of the mining.

4.4.3 Arsenic

Under the maximum source assumption, the peak concentration of arsenic in the slope alluvium is computed to be 0.549 mg/L, and 0.047 mg/L in the valley alluvium. The computed change 0.002 mg/L in the river would not be detectable against the background of 0.006 mg/L. It is computed that in this case the peak value will not be reached for approximately 1,600,000 years after the end of the mining, due to the high attenuation of arsenic in this system. The results of the analysis are presented in Figure 6.

4.4.4 Other Metals

All the other metals evaluated for the maximum source case have no detectable increase in concentration in the alluvium or the water of the Goodpaster River. All changes are at or close to detection, except in the slope alluvium, where concentrations remain below drinking water standards. It is computed to take hundreds of thousands or millions of years for peak concentrations to be reached under this source scenario, which would be sufficient time for geologic mineralization processes to occur to remove metals from solution.

4.5 Sensitivity

The above analysis of the post-closure water quality in the vicinity of the Pogo Underground Mine presents the expected case, and the maximum source case. Some of the parameters that were used to develop the results are subject to uncertainty, so a series of sensitivity analyses were conducted to determine the sensitivity of the results to those uncertainties. The results of these analyses are presented in Table 4, and the changes in concentrations are summarized for TDS and arsenic in the river materials below:

| Species Location Unit | Change in TDS | | | Change in Arsenic | | |
|-------------------------------|---------------|----------------|---------------|-------------------|----------------|---------------|
| | Slope mg/L | Valley mg/L | River mg/L | Slope mg/L | Valley mg/L | River mg/L |
| Base Case | 291 | 16 | 1 | <0.001 | <0.001 | <0.001 |
| Low Hydraulic Conductivity | 276 | 53 | 1 | <0.001 | <0.001 | <0.001 |
| High Hydraulic Conductivity | 90 | 11 | 2 | <0.001 | <0.001 | <0.001 |
| Low Porosity | 345 | 19 | 1 | <0.001 | <0.001 | <0.001 |
| High Infiltration | 291 | 16 | 1 | <0.001 | <0.001 | <0.001 |
| Low Distribution Coefficients | 291 | 16 | 1 | <0.001 | <0.001 | <0.001 |
| No Adsorption | 291 | 16 | 1 | 0.250 | 0.014 | 0.001 |
| Maximum Source | 576 | 32 | 2 | 0.496 | 0.027 | 0.002 |
| Maximum Source, No Kd | 577 | 32 | 2 | 0.497 | 0.027 | 0.002 |

4.5.1 Hydraulic Conductivity

The hydraulic conductivities of all materials including rock and river alluvium were set at the highest and lowest values consistent with the data. Increasing the hydraulic conductivity increases the mass rate of transport of dissolved materials from the backfill (by greater flow through the fill) but increases the dilution by flow in the alluvial materials. As a result, the high conductivity case decreases the concentrations in the alluvium, and increases the concentration in the river (and the opposite changes occur with reduction of the hydraulic conductivity). The changes are modest; below detection in the river, and not significant with respect to impacts.

4.5.2 Porosity

Reducing the porosity from the expected value to the lowest value in the range for all materials produced an increase in predicted concentrations in the Goodpaster Valley by up to 12%. These changes would not be detectable.

4.5.3 Infiltration

Increasing the infiltration to the highest values in the range for all materials produced a reduction in predicted concentrations in the Goodpaster alluvium of up to 50%, and an increase in predicted concentrations in the Goodpaster River of up to 50%. Decreasing the infiltration by a corresponding amount resulted in the opposite effects. None of the computed changes would be detectable.

4.5.4 Distribution Coefficient

Distribution coefficients of all materials were set at the lowest value consistent with the laboratory data. This reduced the extent to which metals are adsorbed, and increased the speed of transit and increases the concentrations in the Goodpaster Valley. The results were essentially unchanged, with concentration changes increasing approximately 2%, which is not detectable.

To evaluate the significance of the laboratory-determined distribution coefficients on the results, distribution coefficients for all species were set to zero. This eliminates adsorption of the rockmass and the alluvium. Peak concentration changes in the river valley increased by as much as four orders of magnitude in some cases as a result of this change; however the concentrations that resulted would still not be detectable except in the case of arsenic. Transit times for all species also dropped to about a century.

4.6 Summary

The results of the evaluation of solute transport at the Pogo site after mine closure are as follows:

1. In general, no measurable post-closure increases in concentration of mine-related constituents are expected to occur in the Goodpaster River or the riverside alluvial materials.

2. An increase in TDS may occur in alluvium close to the valley wall in about 100 years; this change may slightly increase the area of the alluvium in which the water exceeds the secondary drinking water standard for TDS of 500 mg/L.
3. A slight increase in cyanide concentrations may occur in the alluvium close to the valley wall in about 100 years; the computed change is 0.013 mg/L, which is well below the drinking water MCL of 0.200 mg/L. However it is expected that the cyanide will undergo some degradation in transit, so no change is likely to be identifiable.
4. A slight increase in arsenic is predicted for the alluvium close to the valley wall, but this will take geologic times to occur. This change would not be expected to be identifiable by site measurement.
5. Consideration of the maximum variation in all site parameters and of the source term does not significantly change the results of these analyses.

In summary, no significant change is expected to occur in concentrations of groundwater constituents, and no measurable change is expected to occur in concentrations of surface water constituents as a result of post-closure seepage through the Pogo Mine backfill.

5. Conclusions

The impact of backfilling the Pogo Mine with cemented and uncemented processed ore materials has been evaluated using a solute transport analysis model. As a result of the low hydraulic conductivity of the host rock, the high ability of the host rock and alluvium to adsorb metals, and the high dilution of the groundwater flow when it enters the Goodpaster River valley, no significant chemical impacts will occur to water resources in the Goodpaster River or its alluvium as a result of the backfilling and closure of the proposed underground mine.

6. References

- ABC, 1999. *Pogo Project Mine Inflow Evaluation, Alaska*, preliminary consultant report prepared for Teck Corporation, December 1.
- ABC, 2000. *Pogo Project Mine Inflow, Alaska*, consultant report prepared for Teck Corporation, July 15.
- ABC, 2001. *Pogo Project Mine Inflow, Alaska*, consultant report prepared for Teck Corporation, June 15.
- Golder, 1998. *Technical Memorandum No. 1, Field Investigations and Results, Pogo Project, Alaska*, consultant report submitted to Teck Corporation, October.
- Golder, 2000. *Phase I Laboratory Investigation to Determine the Effect of Blending of Flotation and Leachate Tailings on Paste Backfill Strength, Pogo Project, Alaska*, consultant report submitted to Teck Corporation, February.

Golder, 2000a. *Phase I Laboratory Investigation of Hydraulic Conductivity of Blended Flotation: Leachate Tailings in Paste Backfill, Pogo Project, Alaska*, consultant report submitted to Teck Corporation, March.

EBA, 1998. *Water Balance Evaluation, Pogo Project, Alaska*, Elmer Brooker and Associates, Vancouver.

Teck, 1999. *Pogo Project – Draft Pre-Feasibility Study - Geology*, September 30.

Teck-Pogo, 2000. *Pogo Project – Water Management Plan*, Teck-Pogo Inc, Pogo Project Documentation, August.

Teck-Sumitomo, 2000. *Pogo Project – Environmental Baseline Document*, Teck Resources, Inc. and Sumitomo Metal Mining America, 8 volumes, April.

Table 1 – Laboratory Distribution Coefficients of Site Materials

| Analyte Unit | TDS ml/g | CN ml/g | As ml/g | Cd ml/g | Ni ml/g | Sb ml/g | Se ml/g |
|-----------------|----------|---------|---------|---------|---------|---------|---------|
| Rock | 0 | 0 | 4.5 | 45 | 4.5 | 0.5 | 1.4 |
| Backfill | 0 | 0 | 3 | 30 | 3 | 0.3 | 0.9 |
| Alluvium-Slope | 0 | 0 | 6 | 60 | 6 | 0.6 | 1.8 |
| Alluvium-Valley | 0 | 0 | 6 | 60 | 6 | 0.6 | 1.8 |
| River | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

Table 2 - Water and Solid Chemistry Results

| Parameter | Unit | Good-paster River Water (1) | Valley Alluvium Ground-Water (2) | Slope Alluvium Ground-Water (3) | Non-Orebody Ground-water (4) | Orebody Ground-water (5) | Cemented Tailings Liquor (6) | Cemented Tails Solids (7) |
|--------------|----------|-----------------------------|----------------------------------|---------------------------------|------------------------------|--------------------------|------------------------------|---------------------------|
| Conductivity | µS/cm | 71 | 383 | 854 | 766 | 1,416 | 7081 | |
| pH | pH units | 7.37 | 6.57 | 6.98 | 7.90 | 7.44 | 9.32 | 9.3 |
| TDS | mg/L | 70 | 294 | 601 | 553 | 987 | 5691 | |
| TSS | mg/L | 10 | 13 | 48 | 183 | 20 | | |
| Turbidity | NTU | 2 | 7 | 224 | 89 | 24 | | |
| Bicarbonate | mg/L | 38.6 | 75.5 | 205 | 410 | 338 | | |
| Alkalinity | mg/L | 38.2 | 74.4 | 191 | 369 | 338 | 63 | |
| Hardness | mg/L | 53.0 | 188.8 | 513 | 408 | 709 | | |
| Ca | ppm | 14.5 | 48.6 | 120 | 81 | 117 | 1545 | 25,500 |
| Fe | ppm | 0.04 | 11.4 | 27 | 0.9 | 1.1 | 1.0 | 30,600 |
| K | ppm | 2.8 | 2.2 | 3.0 | 3.5 | 3.3 | 69 | 2,200 |
| Mg | ppm | 3.7 | 16.3 | 50 | 49 | 99 | 16 | 4,100 |
| Na | ppm | 2.5 | 6.9 | 13 | 30 | 41 | 230 | 100 |
| P | ppm | 0.02 | 0.08 | 0.22 | 0.30 | 0.5 | 0.3 | 240 |
| Cl | ppm | 0.4 | 10.3 | 1.1 | 3.8 | | 29 | |
| NH3 | ppm | | 0.3 | 0.35 | 0.40 | 0.1 | | |
| NO3 | ppm | 0.27 | 0.09 | 0.04 | 0.05 | 0.1 | | |
| SO4 | ppm | 15.5 | 111.3 | 332 | 168 | 431 | 3714 | |
| CN | ppm | | | | | | 0.4 | |
| Si | ppm | | 5.9 | 5.7 | 7.9 | | 13 | |
| F | ppm | 0.1 | 0.1 | 0.17 | 1.2 | 0.6 | | |
| Ag | ppb | -0.02 | -0.02 | -0.02 | -0.02 | -0.02 | 181 | 800 |
| Al | ppb | 19 | 69 | 6 | 127 | 6 | 1,584 | 7,000,000 |
| As | ppb | 0.30 | 30 | 53 | 50 | 1,645 | 4,482 | 7,080,000 |
| Ba | ppb | 15.6 | 67.3 | 173 | 53 | 17 | 109 | 50,000 |
| Be | ppb | 2.1 | 0.5 | 0.9 | 0.7 | | -0.2 | -500 |
| B | ppb | | 2.8 | 2.9 | 11 | 11 | 167 | |
| Bi | ppb | | 0.5 | 0.75 | 0.70 | 0.6 | -0.2 | 82,000 |
| Cd | ppb | 0.04 | 0.07 | 0.07 | 0.11 | 0.034 | -0.2 | -500 |
| Co | ppb | 0.1 | 3.5 | 0.4 | 13 | 1.0 | 31 | 12,000 |
| Cr | ppb | 1.1 | 4.0 | 2.6 | 1.7 | 4.1 | 29 | 164,000 |
| Cu | ppb | 0.7 | 1.2 | 1.8 | 0.8 | 1.3 | 63 | 198,000 |
| Fe | ppb | 40 | 11,432 | 26,833 | 859 | 1,108 | 1,279 | 30,600,000 |
| Hg | ppb | | 0.05 | 0.04 | 0.02 | 0.02 | -0.4 | -10,000 |
| Mn | ppb | 4 | 981 | 1,089 | 319 | 57 | 4.74 | 295,000 |
| Mo | ppb | 0.32 | 0.31 | 1.39 | 12 | 6.3 | 783 | 5,000 |
| Ni | ppb | 0.82 | 2.45 | 1.7 | 15 | 6.4 | 363 | 22,000 |
| Pb | ppb | 0.03 | 0.15 | 0.08 | 0.67 | 0.1 | -9 | 42,000 |
| Sb | ppb | 0.10 | 0.14 | 0.12 | 0.76 | 2.4 | 53 | 4,000 |
| Se | ppb | | 1.08 | 1.5 | 1.4 | 1.2 | 50 | 200(9) |
| Sn | ppb | 0.40 | 0.12 | 0.15 | 0.14 | 0.1 | 6 | |
| Sr | ppb | 83 | 266 | 843 | 1,172 | 4,980 | 2,070 | 54,000 |

| Parameter | Unit | Good-paster River Water (1) | Valley Alluvium Ground-Water (2) | Slope Alluvium Ground-Water (3) | Non-Orebody Ground-water (4) | Orebody Ground-water (5) | Cemented Tailings Liquor (6) | Cemented Tails Solids (7) |
|-----------|------|-----------------------------|----------------------------------|---------------------------------|------------------------------|--------------------------|------------------------------|---------------------------|
| Ti | ppb | | 0.026 | 0.065 | -10 | | -43 | 300,000 |
| Tl | ppb | | 10 | 10 | 0 | 0.02 | 0.11 | -10,000 |
| U | ppb | 0.41 | 2.70 | 8.3 | 4.8 | 20 | 0.41 | -10,000 |
| V | ppb | 0.40 | 2.47 | 1.7 | 1.5 | 0.9 | 23 | 22,000 |
| Zn | ppb | 2.36 | 6.49 | 7.6 | 124 | 8.1 | 18 | 36,000 |

NOTES:

- (1) Goodpaster River data averaged from locations SW-23 (upstream) and SW-15 (downstream) (n=26)
- (2) Valley alluvium averaged from MW98-03 (shallow) and MW98-15 (deep) (n=20)
- (3) Slope alluvium averaged from MW98-10A (n=6)
- (4) Non-ore groundwater from MW98-80, -81, and -82 (n=20). Note elevated cobalt, zinc.
- (5) Orebody groundwater samples are taken from flow from underground drill holes (n=42)
- (6) Re-concentrated from Initial Humidity Cell Test leachate
- (7) Tailings from Tests 37, 38, and 39 of the Humidity Cell Test sequence; values are for solids
- (8) Negative sign means "less than"
- (9) Solid phase selenium value taken from total tailings analysis
- (10) Except as noted, all values are for dissolved concentration (filtered with a 0.45 micron filter)

Table 3 – Maximum Source Term Constituent Availability

| Parameter | Cemented Tailings Liquor (mg/L) | Cemented Tailings Solid (mg/Kg) | Effective Kd (4) (Distribution Coeff) (L/Kg) |
|-----------|---------------------------------|---------------------------------|--|
| TDS | 5,679 | 78,000 (1) | 14 |
| CN | 0.4 | 0.4 (2) | 1 |
| As | 4.5 | 7,080 | 1,573 |
| Cd | <0.001 (3) | <0.5 (3) | 500 |
| Ni | 0.4 | 22 | 55 |
| Sb | 0.053 | 4 | 75 |
| Se | 0.050 | 0.2 | 4,000 |

(1) Computed from expected soluble and leachable constituents from Table 2

(2) Solid phase concentration assumed to be the same as liquid phase

(3) Concentrations set at detection limits

(4) Effective distribution coefficient = maximum concentration in solid /concentration in liquid

Table 4 - Results of Sensitivity Analyses

| Species | Location | Unit | Base Case | High Hydraulic Conductivity | Low Distribution Coefficients | No Adsorption | Low Porosity | High Infiltration | Low Hydraulic Conductivity | Maximum Source | Maximum Source, No Kd | |
|---------|----------|-------|-----------|-----------------------------|-------------------------------|---------------|--------------|-------------------|----------------------------|----------------|-----------------------|-------|
| TDS | Backfill | mg/L | 5158 | 5158 | 5158 | 5158 | 5158 | 5158 | 5158 | 5158 | 5158 | |
| | Rock | mg/L | 2591 | 2554 | 2591 | 2591 | 2985 | 2591 | 2418 | 4520 | 4530 | |
| | Slope | mg/L | 291 | 90 | 291 | 291 | 345 | 291 | 276 | 576 | 577 | |
| | Valley | mg/L | 16 | 11 | 16 | 16 | 19 | 16 | 53 | 32 | 32 | |
| | River | mg/L | 1 | 2 | 1 | 1 | 1 | 1 | 1 | 2 | 2 | |
| | Time | years | 140 | 100 | 140 | 140 | 60 | 140 | 290 | 1000 | 390 | |
| CN | Backfill | mg/L | 0.400 | 0.400 | 0.400 | 0.400 | 0.400 | 0.400 | 0.400 | 0.400 | 0.400 | |
| | Rock | mg/L | 0.201 | 0.198 | 0.201 | 0.201 | 0.231 | 0.201 | 0.188 | 0.334 | 0.336 | |
| | Slope | mg/L | 0.023 | 0.007 | 0.023 | 0.023 | 0.027 | 0.023 | 0.021 | 0.042 | 0.043 | |
| | Valley | mg/L | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.004 | 0.002 | 0.002 | |
| | River | mg/L | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| | Time | years | 140 | 100 | 140 | 140 | 60 | 140 | 290 | 280 | 250 | |
| As | Backfill | mg/L | 4.432 | 4.432 | 4.432 | 4.432 | 4.432 | 4.432 | 4.432 | 4.432 | 4.432 | |
| | Rock | mg/L | 0.001 | 0.001 | 0.002 | 2.226 | 0.001 | 0.001 | 0.001 | 0.001 | 3.893 | 3.898 |
| | Slope | mg/L | 0.000 | 0.000 | 0.000 | 0.250 | 0.000 | 0.000 | 0.000 | 0.496 | 0.497 | |
| | Valley | mg/L | 0.000 | 0.000 | 0.000 | 0.014 | 0.000 | 0.000 | 0.000 | 0.027 | 0.027 | |
| | River | mg/L | 0.000 | 0.000 | 0.000 | 0.001 | 0.000 | 0.000 | 0.000 | 0.002 | 0.002 | |
| | Time | years | 270000 | 190,000 | 190,000 | 140 | 270,000 | 270,000 | 540,000 | 1,600,000 | 720 | |
| Cd | Backfill | mg/L | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| | Rock | mg/L | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| | Slope | mg/L | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| | Valley | mg/L | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| | River | mg/L | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| | Time | years | 1420000 | 1420000 | 500000 | 140 | 2700000 | 2700000 | 5400000 | 3200000 | 540 | |
| Ni | Backfill | mg/L | 0.348 | 0.348 | 0.348 | 0.348 | 0.348 | 0.348 | 0.348 | 0.348 | 0.348 | |
| | Rock | mg/L | 0.000 | 0.000 | 0.000 | 0.175 | 0.000 | 0.000 | 0.000 | 0.305 | 0.306 | |
| | Slope | mg/L | 0.000 | 0.000 | 0.000 | 0.020 | 0.000 | 0.000 | 0.001 | 0.039 | 0.039 | |
| | Valley | mg/L | 0.000 | 0.000 | 0.000 | 0.001 | 0.000 | 0.000 | 0.000 | 0.002 | 0.002 | |
| | River | mg/L | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| | Time | years | 270000 | 190000 | 150000 | 140 | 270000 | 270000 | 540000 | 1400000 | 680 | |
| Sb | Backfill | mg/L | 0.052 | 0.052 | 0.052 | 0.052 | 0.052 | 0.052 | 0.052 | 0.052 | 0.052 | |
| | Rock | mg/L | 0.000 | 0.000 | 0.000 | 0.026 | 0.000 | 0.000 | 0.000 | 0.046 | 0.046 | |
| | Slope | mg/L | 0.000 | 0.000 | 0.000 | 0.003 | 0.000 | 0.000 | 0.000 | 0.006 | 0.006 | |
| | Valley | mg/L | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| | River | mg/L | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| | Time | years | 30000 | 21000 | 9000 | 140 | 30000 | 30000 | 60000 | 300000 | 620 | |
| Se | Backfill | mg/L | 0.049 | 0.049 | 0.049 | 0.049 | 0.049 | 0.049 | 0.049 | 0.049 | 0.049 | |
| | Rock | mg/L | 0.000 | 0.000 | 0.000 | 0.025 | 0.000 | 0.000 | 0.000 | 0.042 | 0.043 | |
| | Slope | mg/L | 0.000 | 0.000 | 0.000 | 0.003 | 0.000 | 0.000 | 0.000 | 0.005 | 0.005 | |
| | Valley | mg/L | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| | River | mg/L | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| | Time | years | 82500 | 58500 | 48000 | 140 | 84000 | 84000 | 165000 | 450000 | 600 | |

Figure 1- Hydraulic Conductivity Distributions

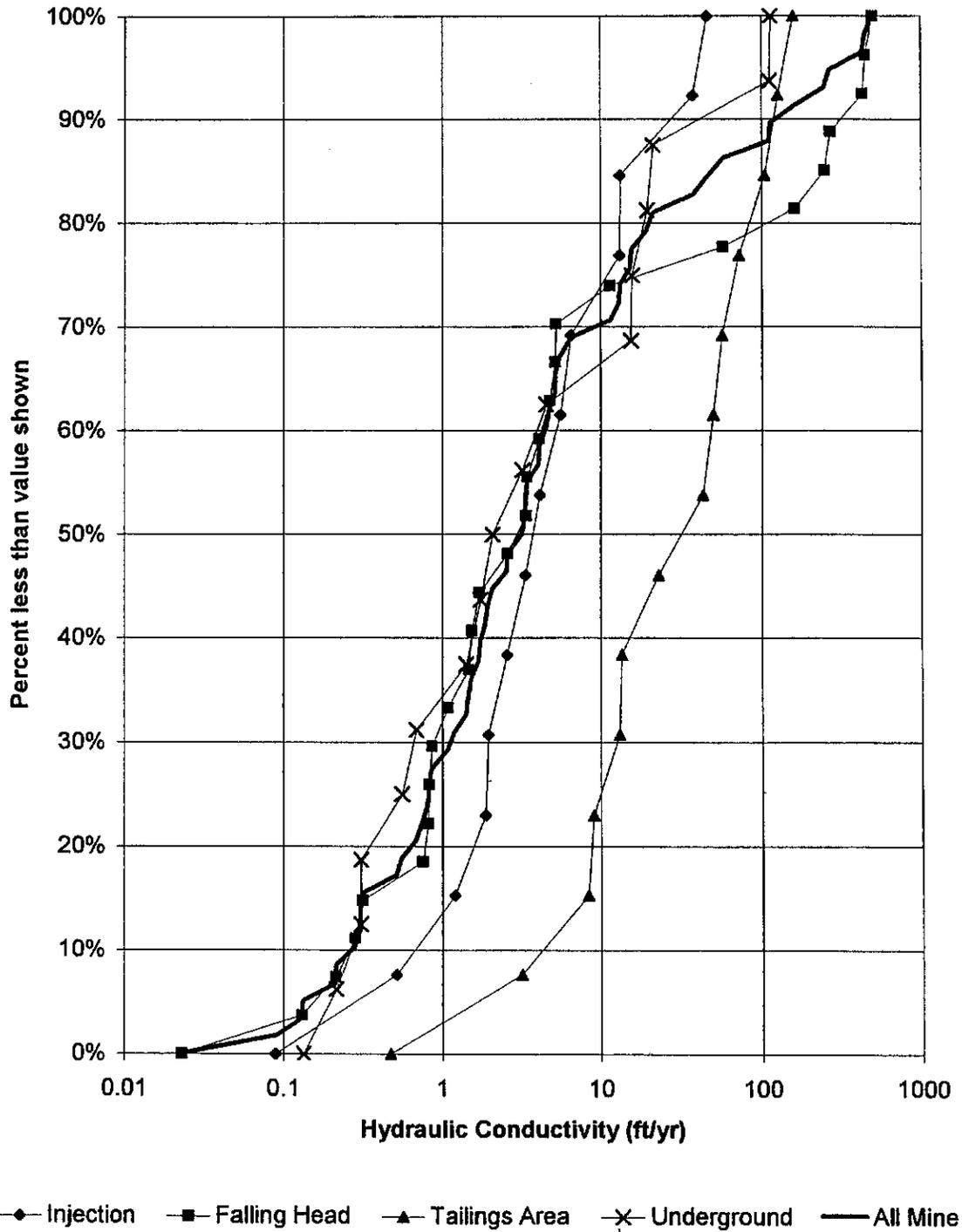


Figure 2 – Schematic of Mixing Cell Model

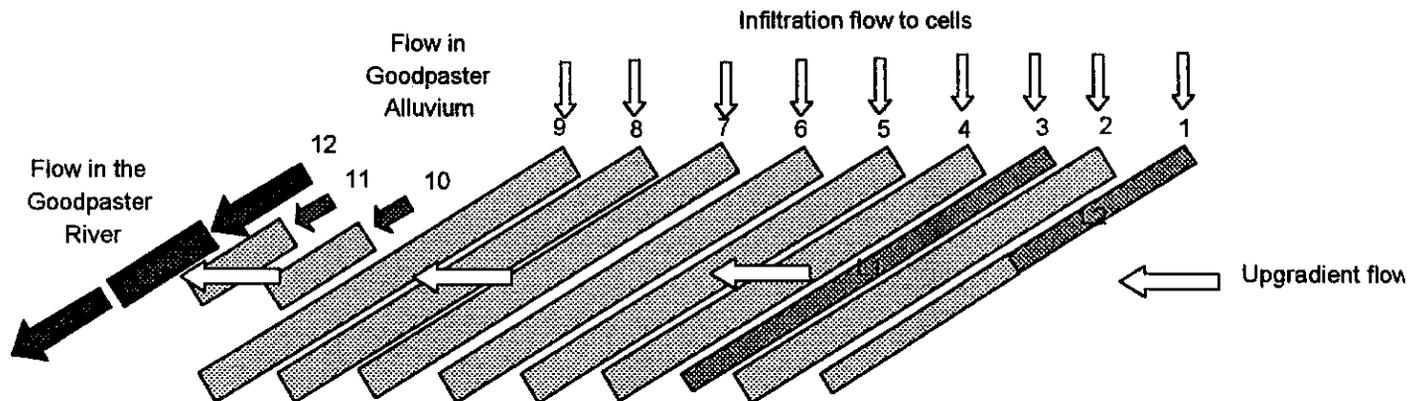


Figure 3 – Expected Case – TDS

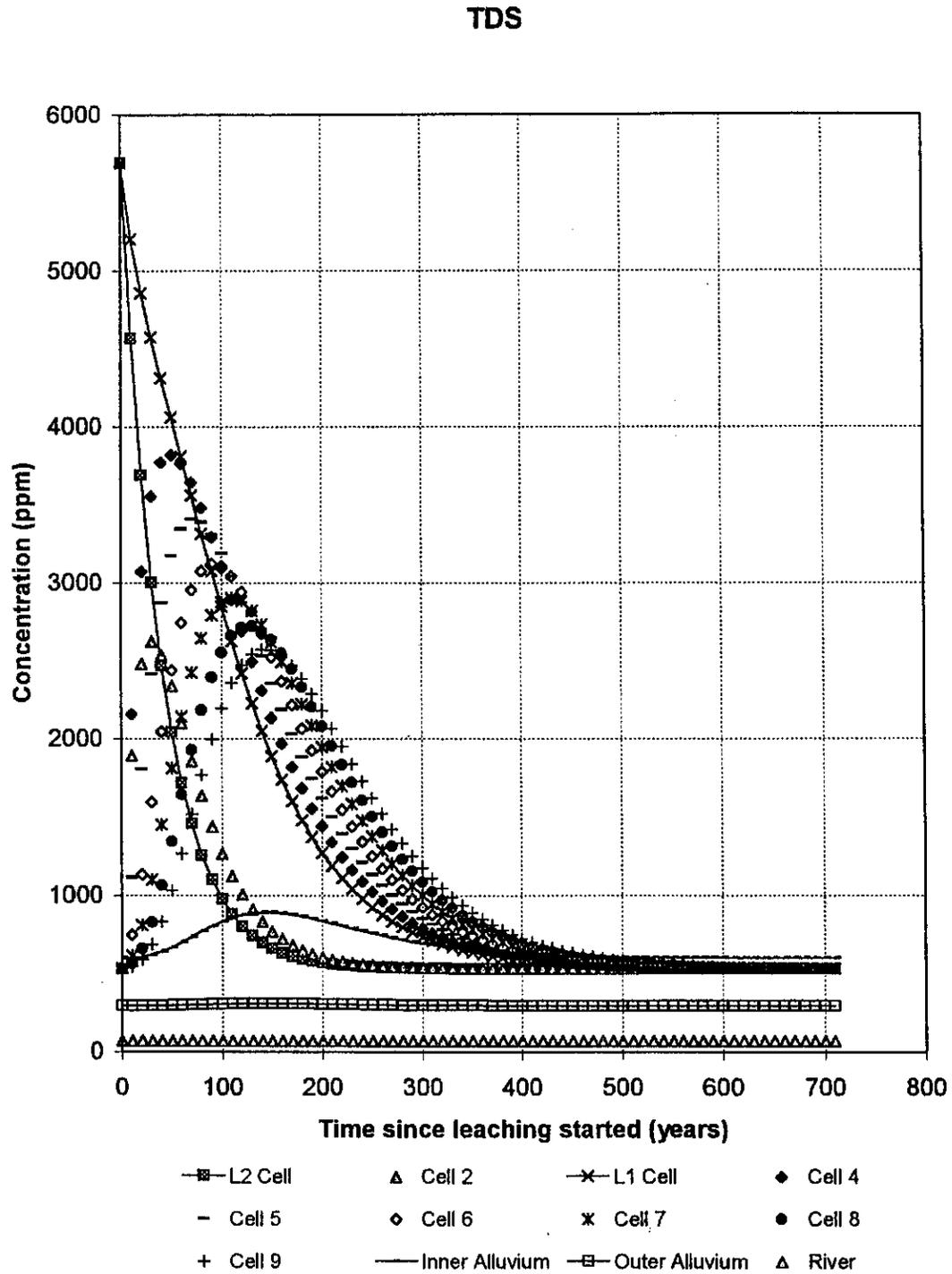


Figure 4 – Expected Case – Arsenic

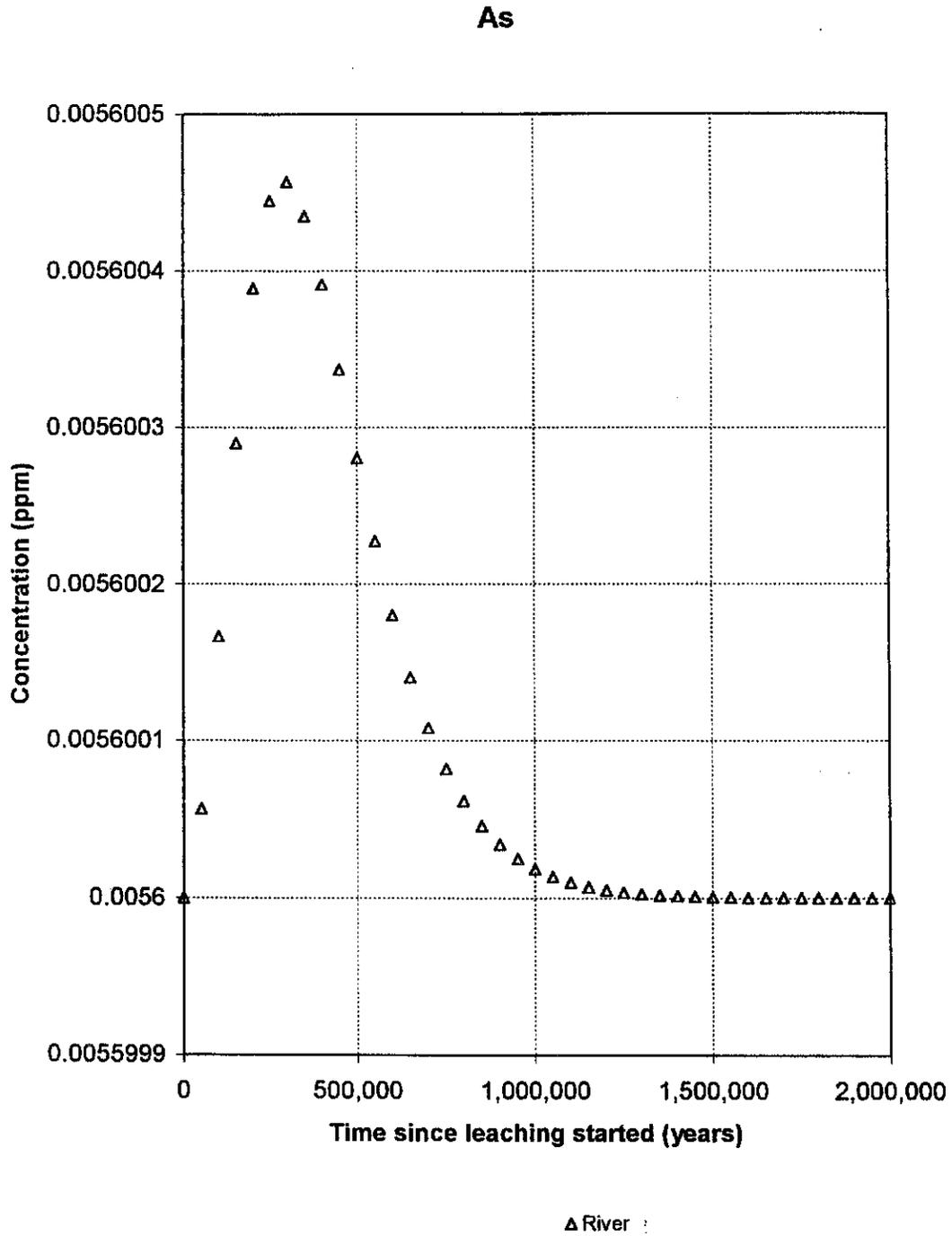


Figure 5 - Maximum Source - TDS

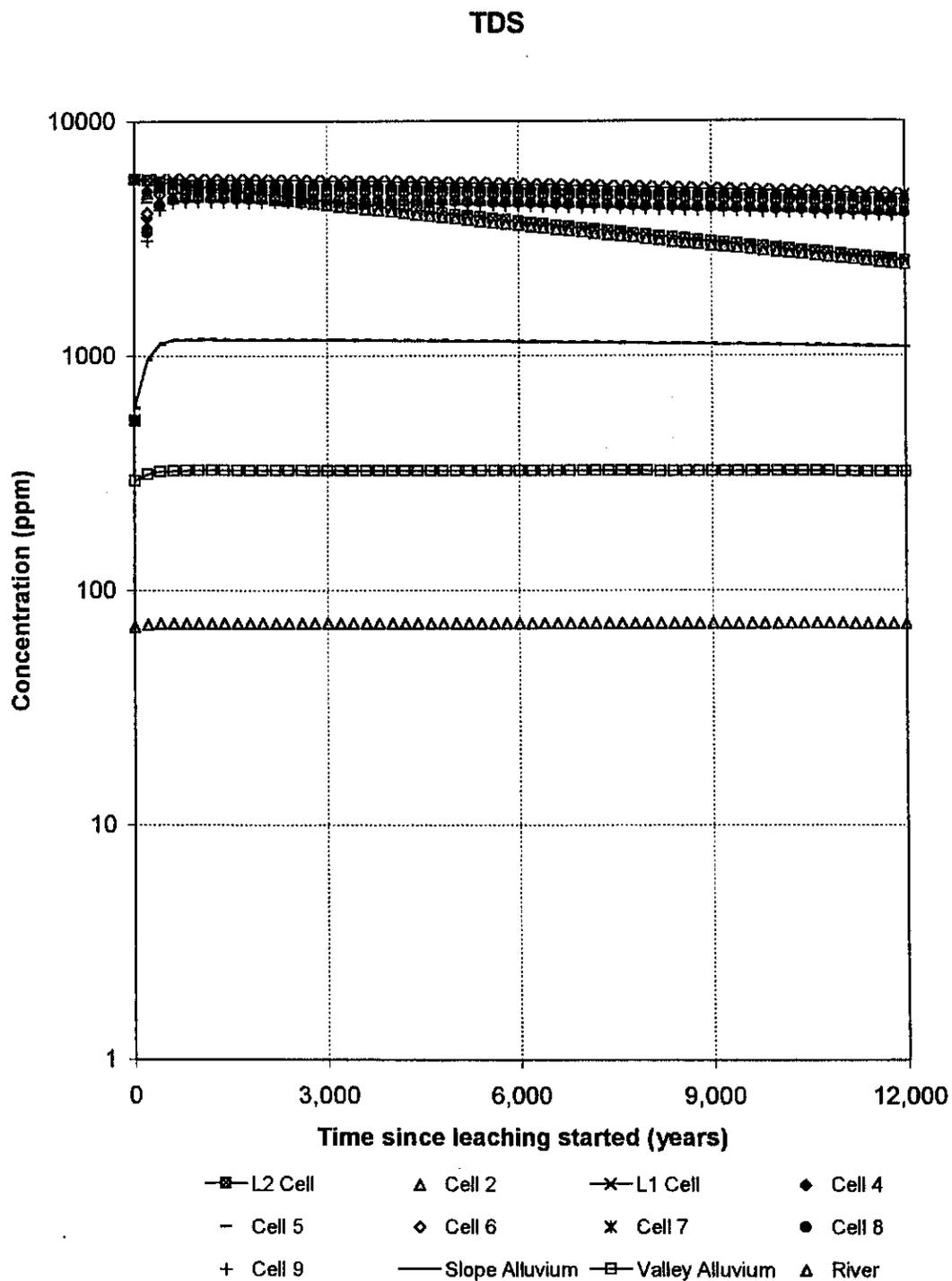
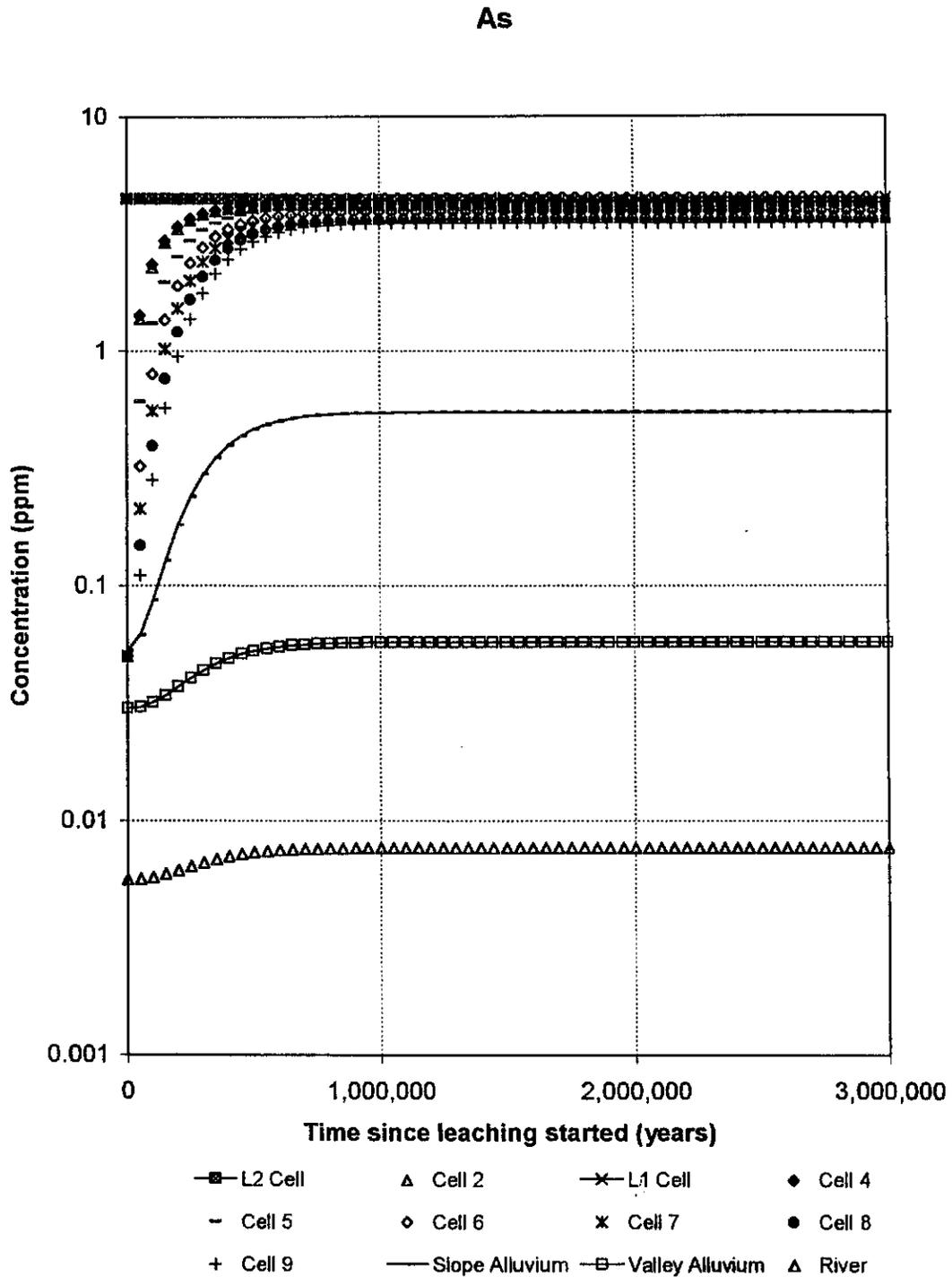
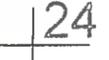
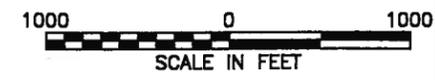
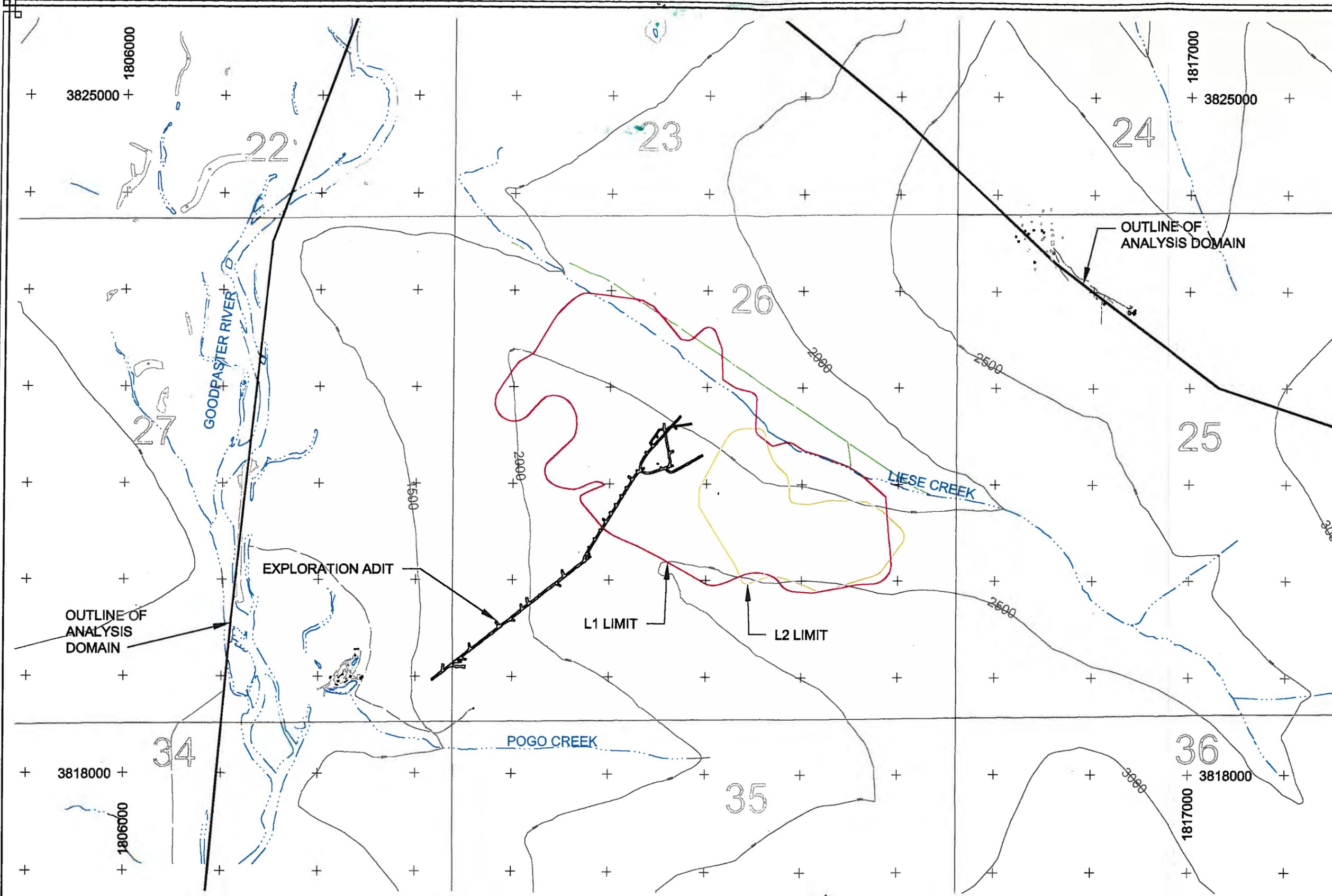


Figure 6 - Maximum Source - Arsenic



LEGEND

-  SECTION LINES AND NUMBERS
-  UTM COORDINATE GRID
-  STREAMS
-  SURFACE CONTOURS
-  L1 LIMIT
-  L2 LIMIT



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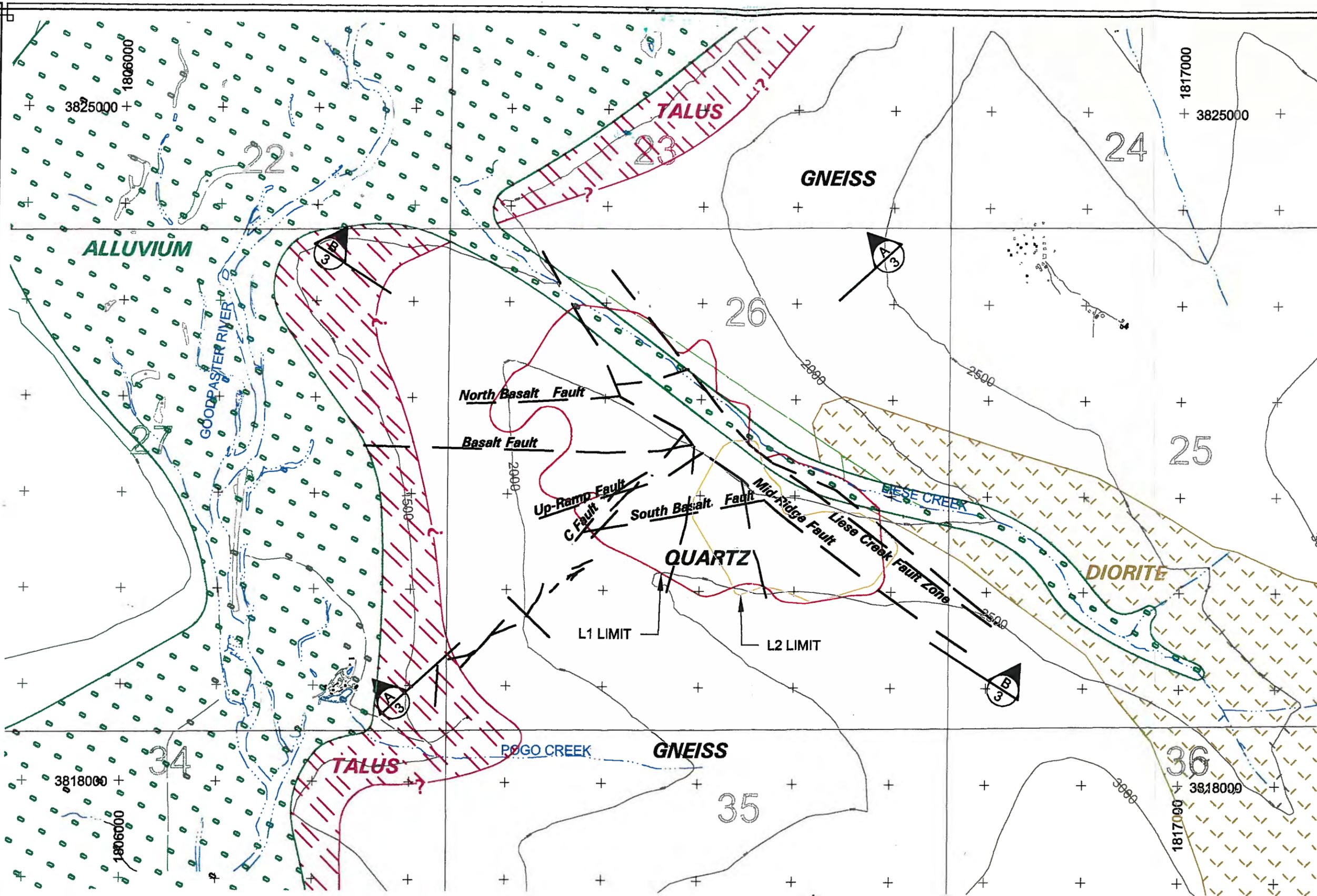


LOCATION PLAN

POGO GOLD PROJECT, ALASKA



| | | | |
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| DRAWN: D.B. | DATE: 12 JUNE 2001 | Date: 12 June 2001 14:00:00 | 1 |
| CHECKED: A.B. | DATE: 12 JUNE 2001 | | |



LEGEND

- SECTION LINES AND NUMBERS
- UTM COORDINATE GRID
- STREAMS
- SURFACE CONTOURS
- DIORITE BODY BOUNDARY
- L1 LIMIT
- L2 LIMIT
- FAULT LINES
- ALLUVIUM
- TALUS
- DIORITE
- GNEISS
- SUBSURFACE OREBODIES (QUARTZ)



TECK
CORPORATION

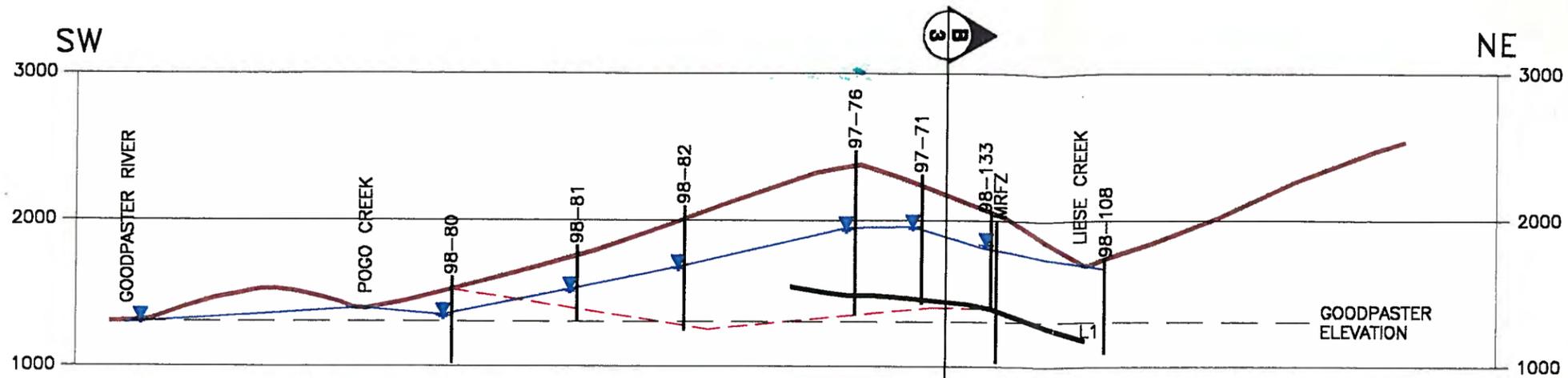


GEOLOGY AND STRUCTURE

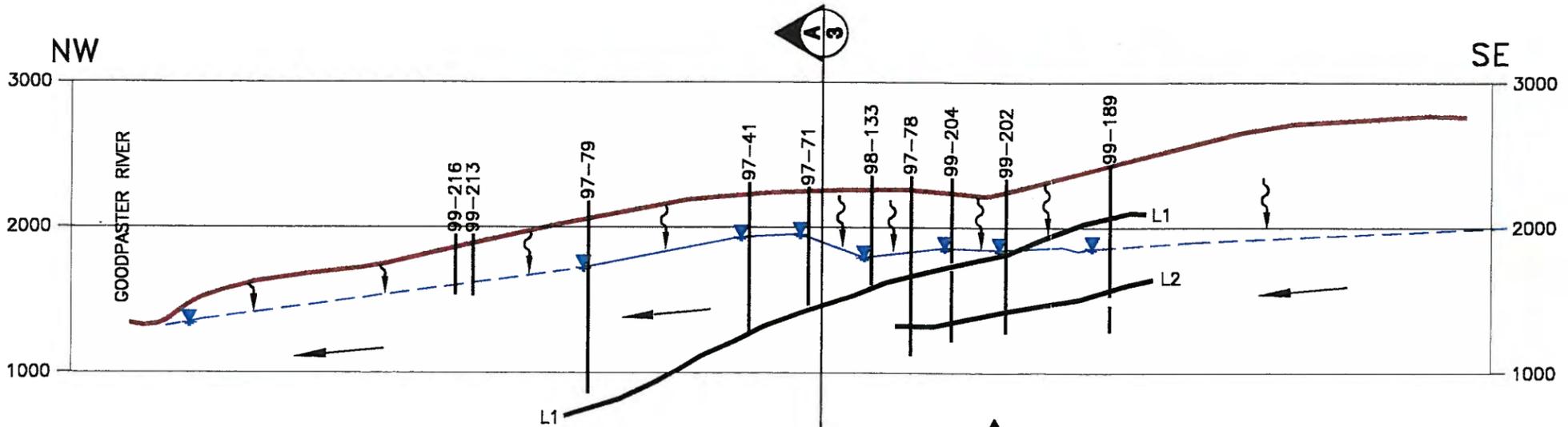
POGO GOLD PROJECT, ALASKA



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| CHECKED: A.B. | DATE 12 JUNE 2001 | Date: 12 June 2001 10:10:00 | |



CROSS SECTION
NO VERTICAL EXAGGERATION

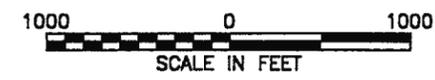


CROSS SECTION
NO VERTICAL EXAGGERATION



LEGEND

- GROUND SURFACE
- PIEZOMETRIC SURFACE (1999)
- DECLINE PROFILE
- OREBODY INTERSECTS
- INFILTRATION
- GROUNDWATER FLOW



TECK
CORPORATION



GEOLOGIC CROSS SECTIONS

**POGO GOLD
PROJECT, ALASKA**



| | | | |
|----------------|-----------------------|-----------------------------|--------------|
| DESIGNED: A.B. | DATE: 24 JANUARY 2001 | FILE: /1543a1 | PLATE NUMBER |
| DRAWN: D.B. | DATE: 24 JANUARY 2001 | 1543a-005.DWG; X-Sections | 3 |
| CHECKED: A.B. | DATE: 24 JANUARY 2001 | Date: 24 Jan. 2001 14:10:00 | |

AttachmentOne. Chemical Testing

Bench-Scale Testing of **Attenuation Capacity of** Pogo Mine Lithologies

Prepared for:

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October 30, 2000
Report 1543A.001030



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| | | |
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1. INTRODUCTION

1.1 Overview and Purpose

The Goodpaster River is beside and downgradient of the proposed Pogo Mine, located 90 miles southeast of Fairbanks, Alaska. Paste tails which are used to backfill the underground mine void will contact groundwater as it flows toward the river. Between the Goodpaster River and the proposed mine is a flow-path of approximately 4000 feet of local bedrock. This bedrock will interact with any chemical constituents dissolved in groundwater, primarily through chemical adsorption processes.

The purpose of the chemical attenuation test program presented here is to quantify the extent to which local bedrock will attenuate trace metal concentrations in groundwater. The approach used was to collect representative bedrock samples from the volume between the proposed mine void and the Goodpaster River, and to measure the distribution coefficient (K_d) of the rock using the standardized method.

1.2 Approach

When an aqueous solution contacts a solid, chemical constituents dissolved in the solution will, to varying extents, adsorb onto the solid. It is commonly observed that as the concentration of a species in solution increases, the amount of it adsorbed to contacting solid surfaces also increases. A graph of the amount of species adsorbed as a function of the solution concentration is called an isotherm. The distribution coefficient, K_d , is the simplest numerical description of an isotherm. It is defined by the following equation, with the adsorption reaction at equilibrium:

$$K_d = \frac{\text{concentration of the constituent in the solid phase (mg/kg)}}{\text{concentration of the constituent in the liquid phase (mg/L)}}$$

A range of factors, including solution pH and salinity, affects the magnitude of K_d . Its magnitude cannot easily be predicted and is best determined empirically, using materials and conditions that most closely mirror site circumstances.

The present evaluation of the K_d for trace metal interaction with Pogo lithologies considered an expected base case and a range of variations intended to provide a sensitivity evaluation, increasing the reliability of the base case measurements and constraining uncertainty. The specifics of the base case and each of the variations is presented below in a discussion of methods.

2. METHODS

2.1 Evaluation Approach

The present evaluation considered a best or most likely case for determination of K_d . Additionally, a range of variations on this base case was considered to provide a sensitivity check on the base case determination. The base case scenario for this evaluation considers paragneiss, the dominant rock type in

using paragneiss, and a test solution with a pH of 9. Individual experiments were conducted on each grainsize.

2.1.4 Ionic Strength

As the ionic strength (TDS) of the bulk solution increases, adsorption of trace metals onto mineral surfaces would be expected to decrease, as a result of increased interaction of ions in solution and the increased competition for adsorption sites on the mineral surfaces. A check on the effects of ionic strength was performed in the present evaluation by using paragneiss, a 50/50 grainsize mixture and a bulk solution pH of 9. A high TDS bulk solution was prepared to be consistent with the TDS anticipated for porewaters from paste tails. A second TDS solution was used that was consistent with porewater from paste tails diluted with local groundwater.

2.1.5 Rock Type

Different mineral surfaces have varying capacities for trace metal adsorption and, thus, K_d . At the Pogo site, paragneiss is the dominant rock type and, accordingly, forms the foundation for the base case. However, an orthogneiss and a granitic material are also present. The present evaluation performed tests using these materials in addition to the tests with paragneiss to characterize their contributions. Tests were performed using bulk solutions with a pH of 9 and a 50/50 grainsize mixture.

2.1.6 Leach Blank

An evaluation of metal uptake necessarily considers the potential release of metals from tested minerals due to the action of the bulk solutions. As described above, solutions with elevated pH conditions will react with silicate minerals in an acid-base reaction to decrease the pH, simultaneously dissolving the mineral. The present evaluation performed a check on the potential release of trace metals from the local lithologies. The test was performed using paragneiss, at a 50/50 grainsize mixture, and a distilled water solution adjusted to pH 9 with slaked lime ($\text{Ca}(\text{OH})_2$). The test was conducted in a procedurally identical manner to the metal attenuation tests.

2.2 Methods

2.2.1 Testing Procedure

The approach to testing used in this study involved contacting the site bedrock types with synthetically prepared metal-laden water, with pH and bulk solute concentrations established to be consistent with expected aqueous chemistry conditions at the Pogo site after mine closure. The specific details and procedure of the testing methodology are found in Attachment One to this report.

The testing procedure provided for the combination of a selected solid with a selected solution at a ratio of 100 grams of solid to 500 mL of solution. The mixtures were agitated and allowed to remain in contact for 24 hours. At the end of 24 hours, the experimental solutions were filtered through a 0.45-micron filter and samples were collected for laboratory analysis of dissolved metals. Metals selected for analysis

these standards were included in the testing program. Some elements (e.g. cadmium) did not exceed any identified standard, but were included as a result of expected environmental sensitivity. Using this process, the following trace metals were selected for testing:

- Silver
- Arsenic
- Cadmium
- Copper
- Antimony
- Selenium

Table 3a presents the formulations for the test solutions used in the present study. Table 3b presents the corresponding calculated concentrations. Table 4 (Experimental Results) reports the analytically determined trace metal concentrations in starting test solutions, as well as their concentrations following testing (discussed below).

2.3 Materials

Figure 1 is a generalized cross-section that incorporates all of the lithological data from the underground pilot holes and is a reasonable depiction of the relative abundance of the main rock types.

1. Paragneiss. As seen in Figure 1, the most abundant rock type is paragneiss, which includes variants of biotite-quartz-feldspar gneiss. This material accounts for approximately 85% of the rock mass between the proposed mine void and the river. Other rock types include sub-equal volumes of orthogneiss and non-foliated granitic dykes. The sample is from drillhole UP99-2, taken from a distance of 793 to 800.5 feet from the hole collar.
2. Orthogneiss. The orthogneiss is a heterogeneous rock type that includes augengneiss and textural varieties of meta-granite. This rock type accounts for approximately 10% of the rockmass between the proposed mine void and the river. The sample used in the present study is augengneiss and is from drillhole UP99-2, taken from a distance of 813 to 820 feet from the collar.
3. Granite. Granitic rocks occur in the rockmass as varieties of equigranular granite to coarse-grained pegmatite. These occur as dykes and sills that average 3 ft thick, but are up to 60 ft thick. They are widely distributed, and account for approximately 5% of the rockmass between the proposed mine void and the river. Frequently the equigranular granites exhibit pervasive phyllic alteration. The sample used in the present study is equigranular granite that exhibits weak phyllic alteration and comes from drillhole UP99-2, taken from a distance of 239.5 to 243 feet from the collar.

All three rock types were received as two-inch core. On receipt, they were separately milled at two distinct size fractions: less than 0.25-inch, and less than 0.1-inch. An intermediate size fraction was obtained by mixing equal parts of both of these fractions. Apart from crushing and sieving, the materials were not pre-treated prior to adsorption testing.

| Element | As | Cd | Ni | Sb | Se |
|----------------------|-----|-------|-------|-----|-----|
| Average K_d (mL/g) | 9.6 | >44.5 | ~16.7 | 0.9 | 3.6 |

The base case results for arsenic and selenium appear in Figure 2 and Figure 3 as diamond shaped points. For both elements, the mass adsorbed (mg/kg) increases with the concentration in solution (mg/L), as is expected from theoretical considerations. Note that the points plotted in these figures represent equilibrium conditions, so the solution concentration plotted is lower than the initial concentration. The mass adsorbed (mg/kg) represents the mass lost from the volume of the initial solution distributed over the mass of the solid used in the test. Given the absence of leachable quantities of these elements in the blank run (see Section 3.7 below), this calculus is validated.

As illustrate in Figure 4 for the case of arsenic, the specific form of the adsorption isotherm is not clearly defined. This figure illustrates the conventional difference between a site-specific adsorption mechanism (curved fit) where there is an upper limit to adsorption capacity and a multi-layer mechanism where adsorption capacity rises linearly with solution concentration. Because the present program conducted measurements with trace element concentrations that exceed the expected site concentrations, either mechanistic view is suitable for use in analysis, as there is no need to forecast chemical responses beyond the range of that tested.

For simplicity, and to avoid undue consideration of suitability of one isotherm fit over another, the present evaluation calculated the K_d at each individual measurement point and then averaged them all, for each element. The individual results and the calculated average are reported in Table 5.

3.3 pH Effects

The effect of changing pH on the value of K_d for arsenic and selenium is illustrated on Figure 5. The effect was more pronounced for arsenic than for selenium. For both elements, a decrease in pH of the initial solution resulted in an increase in K_d . Note that the regression lines shown in Figure 5 are for the purpose of highlighting the trends in the data and do not represent any meaningful chemical relationship.

A summary of results of the variation of K_d with pH for otherwise relatively constant conditions (paragneiss, medium grainsize, constant ionic strength) is presented below. Values which are indicated with a ">" sign are for analyses where the initial concentration of the constituent in the test was measurable, but the final concentration was below the MDL. Based on these results, it would appear that all test results are consistent with K_d values decreasing with increasing pH in the tested range (7 to 9). Further, the variation of arsenic and selenium with pH identified in Figure 5 is supported by these data.

| Grainsize | K_d (mL/g) | | | | |
|-------------------------------------|--------------|------|------|-----|-----|
| | As | Cd | Ni | Sb | Se |
| Small (<0.1 inch) | 10.2 | 42.6 | >2.5 | 0.7 | 3.9 |
| Medium (mix of <0.1 and <0.25 inch) | 9.7 | 44.5 | 11.2 | 0.9 | 3.6 |
| Large (<0.25 inch) | 6.3 | 16.1 | >2.5 | 0.7 | 2.7 |
| Estimated rockmass value | 5 | 15 | 5 | 0.5 | 2 |
| Factor: medium to rockmass value | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 |

3.5 Ionic Strength Effects

Ionic strength affected the measured value of K_d in the present evaluation. However, the effect was poorly constrained and somewhat variable. Ionic strength effects were most noticeable for arsenic than selenium (Figure 7).

The variation of K_d with ionic strength as measured by conductivity¹ is shown below for medium size paragneiss, for tests restricted to those with final pH within the range 7.9 to 8.1; the table includes an estimate of the standard deviation of the value of K_d for variation over the entire range of ionic strength²:

| Conductivity (uS/cm) | Estimated TDS ⁽¹⁾ (mg/L) | K_d (mL/g) | | | | |
|---|--|--------------|-----|-----|-----|-----|
| | | As | Cd | Ni | Sb | Se |
| 3800 | 2800 | 10 | 45 | 11 | 0.9 | 3.6 |
| 4400 | 3200 | 13 | 20 | >3 | 1.3 | 3.3 |
| 5200 | 3800 | 8 | 14 | >5 | 1.3 | 2.9 |
| Estimated standard error on mean K_d ⁽²⁾ | | 10% | 40% | 20% | 30% | 20% |

As can be seen, K_d generally decreases as TDS and ionic strength increases; this is expected, as competition for adsorptive sites increases as the ionic strength increases. However, the effect is in general not great; only cadmium shows any significant reduction, with K_d dropping from 45 to 14 as the TDS rises from 2,800 mg/L to 3,800 mg/L. Accordingly, the ionic strength dependence is treated as an uncertainty in the computation of effective K_d , using the estimated standard error.

3.6 Rock Type Effects

As reported in Table 5, the measured K_d values for orthogneiss and granite were lower than the values obtained for paragneiss. This relationship held for arsenic as well as selenium. Thus, the present evaluation indicates that the predominant rock type in downgradient from the proposed underground mine

¹ Conductivity is related to Total Dissolved Solids by the approximate relationship TDS (mg/L) = 0.73 Conductivity (uS/cm), which has been developed from 120 analyses of Pogo groundwaters.

² The estimated standard error is computed by assuming that the range of K_d values include 95% of the total range (that is approximately 4 standard deviations); the value shown is therefore approximately 1/4 of the total range expressed as a percentage of the mean value.

| Element | As | Cd | Ni | Sb | Se | All |
|--------------------------------|-----|-----|----|-----|-----|-----|
| Relative Percentage Difference | 22% | 21% | na | 44% | 13% | 20% |
| Estimated Standard Error | 11% | 10% | na | 22% | 7% | 10% |

Based on these results, the RPD of all analyses is relatively low. The RPD for Antimony is higher because the absolute value of the K_d (the numerator in the expression for RPD) is low.

4. CONCLUSIONS

The testing and evaluation presented above has demonstrated that the subsurface geologic material along the groundwater flow path from the proposed underground Pogo mine workings has an appreciable capacity to adsorb the trace metals which have been evaluated. Determinations of K_d for arsenic, cadmium, nickel, antimony, and selenium show a moderate sensitivity to fluid pH and ionic strength, and rockmass grainsize and rock type. These observed effects are consistent with theoretical expectations.

4.1 Rockmass Distribution Coefficients

The overall rockmass K_d values for the elements evaluated are computed as follows:

1. The values obtained for the three pH values of 7, 8, and 9 are used as the base for paragneiss of medium grainsize (Section 3.3).
2. To convert to the rockmass particle size, the K_d values are halved (Section 0).
3. To allow for the (less adsorptive) minor rock types in the orebody, the K_d values found for paragneiss are multiplied by a factor of 0.9 (Section 3.6).

Making these adjustments, the overall rockmass K_d values for each element for the range of pH values of relevance in the Pogo project are as follows:

| pH | Rockmass K_d (mL/g) | | | | |
|----|-----------------------|------|-----|-----|-----|
| | As | Cd | Ni | Sb | Se |
| 7 | 9.0 | 90.0 | 9.0 | 0.9 | 2.7 |
| 8 | 4.5 | 45.0 | 4.5 | 0.5 | 1.4 |
| 9 | 2.3 | 22.5 | 2.3 | 0.2 | 0.7 |

The uncertainty of these values can be estimated by consideration of the variability introduced by the following factors:

1. Testing. The testing standard error has been estimated as being approximately 10%, based on the replication of each test; actual values for each element are computed in Section 3.8.

Based on these considerations, the K_d values for backfill are as follows:

| pH | Backfill K_d (mL/g) | | | | |
|----|-----------------------|----|-----|-----|-----|
| | As | Cd | Ni | Sb | Se |
| 7 | 5.9 | 59 | 5.9 | 0.6 | 1.8 |
| 8 | 3.0 | 30 | 3.0 | 0.3 | 0.9 |
| 9 | 1.5 | 15 | 1.5 | 0.1 | 0.4 |

The variability of these values is the same as for the rockmass.

4.3 Alluvium

The alluvial materials of the Goodpaster River are made up of a mixture of transported granitic and volcanic particles, grading from boulders to fine sand. Accordingly, the distribution coefficients for the alluvium will also differ from the rockmass, as follows:

4. Size: The size will be equivalent to the medium grind, which is the base case (Section 3.4).
5. pH: The pH of the backfill will be in the order of 7 for the post-closure period; this is considered in Section 3.3.
6. Rock Type: The rock type of the alluvium is a mix of volcanic and granitic materials. This mixture will have a lower K_d than the base rock, paragneiss. The ratio between paragneiss and granite is 0.2 (Section 3.6), so assuming that the alluvium is 50% granite and 50% paragneiss, the K_d factor to convert paragneiss to backfill is computed to be 0.6.

Based on these considerations, the K_d values for backfill are as follows:

| pH | Alluvium K_d (mL/g) | | | | |
|----|-----------------------|-----|----|-----|-----|
| | As | Cd | Ni | Sb | Se |
| 7 | 12 | 120 | 12 | 1.2 | 3.6 |
| 8 | 6 | 60 | 6 | 0.6 | 1.8 |
| 9 | 3 | 30 | 3 | 0.3 | 0.9 |

The variability of these values is the same as for the rockmass.

TABLES

Table 1. Overview of testing conditions.

| Case | Rock | Grainsize | pH | | TDS | | Metal Concentrations | | Other |
|----------------------|-------------|-----------|-------|---|-----|---------|----------------------|-----|------------------------|
| | | | 0.25" | 9 | Raw | Diluted | High | Low | |
| BASE pH Check | Paragneiss | 50% | 50% | 9 | X | X | X | X | Mixture of grainsizes |
| | Paragneiss | 50% | 50% | 8 | X | X | X | X | Mixture of grainsizes |
| Grainsize Check | Paragneiss | 50% | 50% | 9 | X | X | X | X | Mixture of grainsizes |
| | Paragneiss | 100% | | 9 | X | X | X | X | |
| | Paragneiss | | 100% | 9 | X | X | X | X | |
| Ionic Strength Check | Paragneiss | 50% | 50% | 9 | X | X | X | X | Raw tailing porewater |
| | Paragneiss | 50% | 50% | 9 | X | X | X | X | Raw tailing porewater |
| Rock Type Check | Orthogneiss | 50% | 50% | 9 | X | X | X | X | Mixture of grainsizes |
| | Granite | 50% | 50% | 9 | X | X | X | X | Mixture of grainsizes |
| Leach Blank | Paragneiss | 50% | 50% | 9 | | | | | pH adjusted with lime. |

Table 2. Estimation of Paste Tails Porewater Chemistry.

| Parameter | Units | Water Chemistry | | | Water Standards | | | |
|--------------|------------|------------------|------------------------------|--------------------------------------|-----------------|---------------|----------------------------|------------------------------|
| | | Ground-water (1) | Cemented Tailings Liquor (2) | Diluted Cemented Tailings Liquor (2) | Primary MCL (5) | Secondary MCL | Fresh Water Acute LOEL (4) | Fresh Water Chronic LOEL (4) |
| Conductivity | µS/cm | 1,416 | 7080.67 | | | | | |
| pH | pH units | 7.44 | 9.30 | 8.372 | | 6.5-8.5 | | 6.5-9.0 |
| TDS | mg/L | 987 | | | | 500 | | |
| TSS | mg/L | 20 | | | | | | |
| Turbidity | NTU | 24 | | | | 0.5-1.0 | | |
| Bicarbonate | mg/L | 338 | | | | | | |
| Alkalinity | mg/L CaCO3 | 338 | 63 | 200.393 | | | | 20 |
| Acidity | mg/L CaCO3 | | 0 | 0.000 | | | | |
| Hardness | mg/L | 709 | | | | | | |
| Anions | meq/L | 15.55 | | | | | | |
| Cations | meq/L | 15.66 | | | | | | |
| Error | % | -1% | | | | | | |
| Ca | ppm | 117 | 1545 | 831.102 | | | | |
| Fe | ppm | 1.14 | 1.00 | 1.071 | | 0.30 | | 1 |
| K | ppm | 3 | 69 | 36.166 | | | | |
| Mg | ppm | 99 | 16 | 57.483 | | | | |
| Na | ppm | 41 | 230 | 135.622 | | | | |
| P | ppm | 0.54 | 0.3 | 0.420 | | | | |
| Cl | ppm | | 29 | 14.307 | | 250 | | |
| NH3 | ppm | 0.06 | | | | | 0.02 | 0.00 |
| NO3 | ppm | 0.11 | | | 10 | | | |
| TKN | ppm | 0.17 | | | | | | |
| SO4 | ppm | 431 | 3714 | 2072.517 | 500 | 250 | | |
| CN | ppm | | | | 0 | | | |
| Si | ppm | | 13 | 6.263 | | | | |
| F | ppm | 0.57 | | | 4 | 2 | | |
| Ag | ppb | 0.0 | 181 | 90.298 | | 100 | 4.1 | 0.12 |
| Al | ppb | 6.4 | 1,584 | 795.124 | L | 50-200 | | |
| As | ppb | 1,645 | 4,482 | 3063.750 | 50 | | 360 | 190 |
| Ba | ppb | 17 | 109 | 63.143 | 2,000 | | | |
| Be | ppb | | -0.21 | -0.107 | 4 | | | |
| B | ppb | 11 | 167 | 89.158 | L | | | |
| Bi | ppb | 0.6 | -0.24 | 0.162 | | | | |
| Cd | ppb | 0.0 | -0.21 | -0.090 | 5 | | 3.9 | 1.1 |
| Co | ppb | 1.0 | 31 | 15.894 | | | | |
| Cr | ppb | 4.1 | 29 | 16.354 | 100 | | | |
| Cu | ppb | 1.3 | 63 | 32.339 | 1,300 | 1,000 | 18 | 12 |
| Fe | ppb | 1,108 | 1,279 | 1193.664 | | 300 | | 1,000 |
| Ga | ppb | | 11 | 5.730 | | | | |
| Hg | ppb | 0.0 | -0.43 | -0.203 | 2 | | 2.4 | 0.012 |
| La | ppb | | -0.04 | -0.021 | | | | |
| Mn | ppb | 57 | 4.74 | 30.840 | L | 50 | | |
| Mo | ppb | 6.3 | 783 | 394.667 | L | | | |
| Ni | ppb | 6.4 | 363 | 184.593 | 100 | | 1,400 | 160 |
| Pb | ppb | 0.1 | -9 | -4.260 | 15 | | 82 | 3.2 |
| Sb | ppb | 2.4 | 53 | 27.687 | 6 | | 9,000 | 1,600 |
| Sc | ppb | | 4.42 | 2.210 | | | | |
| Se | ppb | 1.2 | 50 | 25.406 | 50 | | 260 | 35 |
| Sn | ppb | 0.1 | 6 | 2.891 | | | | |
| Sr | ppb | 4,980 | 2,070 | 3524.607 | L | | | |
| Ti | ppb | | -43 | -21.461 | | | | |
| Tl | ppb | 0.0 | 0.11 | 0.069 | 2 | | 1,400 | 40 |
| U | ppb | 20 | 0.41 | 10.301 | 20 | | | |
| V | ppb | 0.9 | 23 | 11.916 | T | | | |
| W | ppb | | 74 | 36.841 | | | | |
| Zn | ppb | 8.1 | 18 | 13.148 | L | 5 | 120 | 110 |

NOTES:

- (1) Groundwater samples are taken from flow from underground drill holes
- (2) Humidity Cell Test Liquors are computed concentrations from leachate, reconcentrated to original moisture content
- (3) Tailings solid phase taken from Tests 37, 38, and 39 of the Humidity Cell Test sequence
- (4) "LOEL" means "lowest observed effect level"
- (5) "T" indicates "Tentative (not officially proposed)"; "L" = listed for regulation
- (6) Negative sign means less than (for averages means that at least one value was below detection and set equal to detection)

Table 3a. Formulation of synthetic test solutions.

| Sample ID | Distilled Water (L) | Sulfuric Acid (18 M) (ml) | CaO (g) | NaOH (g) | HCl (ml) | HCl Normality | Ag (ml) | As (ml) | Cd (ml) | Cu (ml) | Ni (ml) | Sb (ml) | Se (ml) | pH | cond (ms) | Analyte Conc | TDS |
|-----------|---------------------|---------------------------|---------|----------|----------|---------------|---------|---------|---------|---------|---------|---------|---------|------|-----------|--------------|-----|
| | | | | | | | | | | | | | | | | | |
| Pogo 101 | 8 | 9.6 | 9.6 | 3.45 | 14 | 0.05 | 4.0 | 36.0 | 4.0 | 4.0 | 4.0 | 0.8 | 0.8 | 9.36 | 4.03 | Hi | Lo |
| Pogo 102 | 3 | 3.6 | 3.6 | 1.01 | 1.75 | 0.50 | 0.4 | 8.0 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 8.86 | 3.69 | Lo | Lo |
| Pogo 103 | 1 | 1.2 | 1.2 | 1.10 | 18.25 | 0.05 | 0.5 | 4.5 | 0.5 | 0.5 | 0.5 | 0.1 | 0.1 | 7.79 | 5.09 | Hi | Lo |
| Pogo 104 | 1 | 1.2 | 1.2 | 0.85 | 14.2 | 0.05 | 0.5 | 4.5 | 0.5 | 0.5 | 0.5 | 0.1 | 0.1 | 6.73 | 5.04 | Hi | Lo |
| Pogo 105 | 2 | 4.8 | 4.8 | 2.20 | 28.9 | 0.50 | 1.0 | 9.0 | 1.0 | 1.0 | 1.0 | 0.2 | 0.2 | 8.89 | 5.20 | Hi | Hi |
| Pogo 106 | 2 | 4.8 | 4.8 | 1.10 | 11.4 | 0.50 | 0.1 | 2.0 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 8.72 | 4.39 | Lo | Hi |

Table 3b. Calculated chemical concentrations of synthetic test solutions.

| Sample ID | SO4 | Ca | Na | Cl | Ag | As | Cd | Cu | Ni | Sb | Se |
|-----------|------|------|-----|-----|-------|------|---------|-------|-------|-------|-------|
| Pogo 101 | 2074 | 857 | 248 | 1 | 0.5 | 4.5 | 0.5 | 0.5 | 0.5 | 0.1 | 0.1 |
| Pogo 102 | 2074 | 857 | 194 | 5 | 0.13 | 2.67 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| Pogo 103 | 2074 | 857 | 633 | 16 | 0.5 | 4.5 | 0.5 | 0.5 | 0.5 | 0.1 | 0.1 |
| Pogo 104 | 2074 | 857 | 489 | 12 | 0.5 | 4.5 | 0.5 | 0.5 | 0.5 | 0.1 | 0.1 |
| Pogo 105 | 4147 | 1714 | 633 | 123 | 0.5 | 4.5 | 0.5 | 0.5 | 0.5 | 0.1 | 0.1 |
| Pogo 106 | 4147 | 1714 | 316 | 48 | 0.05 | 1.0 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| Low TDS | 2073 | 831 | 135 | 14 | 0.090 | 3.1 | 0.0009 | 0.032 | 0.184 | 0.028 | 0.025 |
| High TDS | 3714 | 1545 | 230 | 29 | 0.181 | 4.4 | 0.00021 | 0.063 | 0.363 | 0.053 | 0.050 |

Table 4. Experimental results.

| Test Sample ID | Fine (g) | Coarse (g) | Initial Volume (ml) | pH initial | pH final | cond initial (ms) | pH final | cond final (ms) | Ag | | As | | Cd | | Cu | | Ni | | Sb | | Se | |
|--|----------|------------|---------------------|------------|----------|-------------------|----------|-----------------|------|------|------|-------|-------|-------|------|------|------|------|-------|-------|-------|-------|
| | | | | | | | | | init | fin | init | fin | init | fin | init | fin | init | fin | init | fin | init | fin |
| Base Case- Paragneiss (50/50 mix of grainsizes), pH=9, Hi and Lo analytes | | | | | | | | | | | | | | | | | | | | | | |
| 201 | 50 | 50 | 101 | 500 | 9.36 | 4.02 | 7.97 | 4.15 | 0.01 | 0.01 | 3.6 | 1.35 | 0.074 | 0.006 | 0.02 | 0.02 | 0.03 | 0.02 | 0.08 | 0.07 | 0.105 | 0.061 |
| 202 | 50 | 50.1 | 101 | 500 | 9.36 | 4.05 | 8.26 | 4.15 | 0.01 | 0.01 | 3.6 | 1.62 | 0.074 | 0.006 | 0.02 | 0.02 | 0.03 | 0.02 | 0.08 | 0.07 | 0.105 | 0.067 |
| 203 | 50.2 | 50.1 | 102 | 500 | 8.86 | 3.69 | 7.91 | 3.76 | 0.02 | 0.01 | 1.83 | 0.57 | 0.045 | 0.006 | 0.02 | 0.02 | 0.1 | 0.02 | 0.11 | 0.09 | 0.134 | 0.077 |
| 204 | 50.1 | 50.2 | 102 | 500 | 8.86 | 3.69 | 7.82 | 3.75 | 0.02 | 0.01 | 1.83 | 0.51 | 0.045 | 0.006 | 0.02 | 0.02 | 0.1 | 0.03 | 0.11 | 0.09 | 0.134 | 0.072 |
| pH effects- Paragneiss (50/50 mix of grainsizes), pH= 8, 7 | | | | | | | | | | | | | | | | | | | | | | |
| 205 | 25.2 | 26.2 | 103 | 250 | 7.79 | 5.09 | 7.69 | 5.11 | 0.01 | 0.01 | 3.1 | 0.61 | 0.273 | 0.006 | 0.02 | 0.02 | 0.2 | 0.04 | 0.08 | 0.06 | 0.104 | 0.054 |
| 206 | 25 | 25.3 | 103 | 250 | 7.79 | 5.09 | 7.57 | 5.1 | 0.01 | 0.01 | 3.1 | 0.74 | 0.273 | 0.007 | 0.02 | 0.02 | 0.2 | 0.04 | 0.08 | 0.061 | 0.104 | 0.06 |
| 207 | 25 | 25 | 104 | 250 | 6.73 | 5.04 | 7.61 | 5.11 | 0.01 | 0.01 | 3.1 | 0.82 | 0.424 | 0.017 | 0.04 | 0.02 | 0.41 | 0.1 | 0.08 | 0.07 | 0.112 | 0.06 |
| 208 | 24.9 | 25.3 | 104 | 250 | 6.73 | 5.04 | 7.33 | 4.86 | 0.01 | 0.01 | 3.1 | 0.62 | 0.424 | 0.021 | 0.04 | 0.02 | 0.41 | 0.11 | 0.08 | 0.062 | 0.112 | 0.052 |
| Grainsize effects- pH =9, Hi analytes, Paragneiss- small and large | | | | | | | | | | | | | | | | | | | | | | |
| 209 | 100.3 | 0 | 101 | 500 | 9.36 | 4.02 | 8.04 | 4.13 | 0.01 | 0.01 | 3.6 | 1.18 | 0.074 | 0.006 | 0.02 | 0.02 | 0.03 | 0.02 | 0.08 | 0.07 | 0.105 | 0.059 |
| 210 | 99.6 | 0 | 101 | 500 | 9.36 | 4.02 | 8.01 | 4.03 | 0.01 | 0.01 | 3.6 | 1.19 | 0.074 | 0.011 | 0.02 | 0.02 | 0.03 | 0.02 | 0.08 | 0.08 | 0.105 | 0.059 |
| 211 | 0 | 100 | 101 | 500 | 9.36 | 4.02 | 8.21 | 3.97 | 0.01 | 0.01 | 3.6 | 1.8 | 0.074 | 0.018 | 0.02 | 0.02 | 0.03 | 0.02 | 0.08 | 0.07 | 0.105 | 0.07 |
| 212 | 0 | 100.6 | 101 | 500 | 9.36 | 4.02 | 8.01 | 4.17 | 0.01 | 0.01 | 3.6 | 1.42 | 0.074 | 0.017 | 0.02 | 0.02 | 0.03 | 0.03 | 0.08 | 0.08 | 0.105 | 0.066 |
| Ionic strength effects- Paragneiss (50/50 mix of grainsizes), pH=9, Hi and Lo TDS | | | | | | | | | | | | | | | | | | | | | | |
| 213 | 49.9 | 50.1 | 105 | 500 | 8.89 | 5.2 | 8.11 | 5.26 | 0.03 | 0.01 | 2.6 | 1.07 | 0.023 | 0.006 | 0.02 | 0.02 | 0.04 | 0.02 | 0.09 | 0.073 | 0.101 | 0.064 |
| 214 | 50.9 | 49.7 | 105 | 500 | 8.89 | 5.2 | 8.06 | 5.23 | 0.03 | 0.01 | 2.6 | 0.99 | 0.023 | 0.006 | 0.02 | 0.02 | 0.04 | 0.02 | 0.09 | 0.07 | 0.101 | 0.064 |
| 215 | 50.1 | 49.9 | 106 | 500 | 8.72 | 4.39 | 7.95 | 4.06 | 0.01 | 0.01 | 0.74 | 0.23 | 0.03 | 0.006 | 0.02 | 0.02 | 0.03 | 0.02 | 0.047 | 0.037 | 0.053 | 0.033 |
| 216 | 50.3 | 49.3 | 106 | 500 | 8.72 | 4.39 | 7.86 | 4.16 | 0.01 | 0.01 | 0.74 | 0.18 | 0.03 | 0.006 | 0.02 | 0.02 | 0.03 | 0.02 | 0.047 | 0.038 | 0.053 | 0.031 |
| Blank- Paragneiss (50/50 mix of grainsizes), Distilled water at pH =9 | | | | | | | | | | | | | | | | | | | | | | |
| 217 | 50 | 49.8 | Distilled | 500 | 9.09 | 6 | 8.79 | 90.9 | 0 | 0.01 | 0 | 0.007 | 0 | 0.006 | 0 | 0.02 | 0 | 0.02 | 0 | 0.003 | 0 | 0.001 |
| Rock Type Effects- pH=9, Hi analytes, Ortho gneiss (1) and granite (2)(50/50 size mix) | | | | | | | | | | | | | | | | | | | | | | |
| 218 (1) | 50 | 50.2 | 101 | 500 | 9.36 | 4.02 | 8.47 | 4.1 | 0.01 | 0.01 | 3.6 | 2.3 | 0.074 | 0.022 | 0.02 | 0.02 | 0.03 | 0.02 | 0.08 | 0.08 | 0.105 | 0.082 |
| 218 (1) | 50.1 | 49.8 | 101 | 500 | 9.36 | 4.02 | 8.42 | 4.05 | 0.01 | 0.01 | 3.6 | 2.1 | 0.074 | 0.018 | 0.02 | 0.02 | 0.03 | 0.02 | 0.08 | 0.08 | 0.105 | 0.08 |
| 220 (2) | 50.3 | 50.6 | 101 | 500 | 9.36 | 4.02 | 8.66 | 4.13 | 0.01 | 0.01 | 3.6 | 2.6 | 0.074 | 0.027 | 0.02 | 0.02 | 0.03 | 0.02 | 0.08 | 0.07 | 0.105 | 0.088 |
| 220 (2) | 50.5 | 49.6 | 101 | 500 | 9.36 | 4.02 | 8.6 | 4.14 | 0.01 | 0.01 | 3.6 | 2.6 | 0.074 | 0.042 | 0.02 | 0.02 | 0.03 | 0.02 | 0.08 | 0.08 | 0.105 | 0.088 |

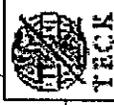
Table 5. Calculated values of Kd

| | | Ag | As | Cd | Cu | Ni | Sb | Se |
|--|---------|-----|------|-------|----|------|-----|-----|
| Base Case- Paragneiss (50/50 mix of grainsizes), pH=9, Hi and Lo analytes | | | | | | | | |
| | 201 | Con | 8.3 | 56.7 | | 2.5 | 0.7 | 3.6 |
| | 202 | Con | 6.1 | 56.6 | | 2.5 | 0.7 | 2.8 |
| | 203 | Dil | 11.0 | 32.4 | | 19.9 | 1.1 | 3.7 |
| | 204 | Dil | 12.9 | 32.4 | | 11.6 | 1.1 | 4.3 |
| | Average | | 9.6 | 44.5 | | 9.1 | 0.9 | 3.6 |
| pH effects- Paragneiss (50/50 mix of grainsizes), pH= 8, 7 | | | | | | | | |
| | 205 | 8 | 19.9 | 216.4 | | 19.5 | 1.6 | 4.5 |
| | 206 | 8 | 15.9 | 188.9 | | 19.9 | 1.5 | 3.6 |
| | 207 | 7 | 13.9 | 119.7 | | 15.5 | 0.7 | 4.3 |
| | 208 | 7 | 19.9 | 95.6 | | 13.6 | 1.4 | 5.7 |
| | Average | | | | | | | |
| Grainsize effects- pH =9, Hi analytes, Paragneiss- small and large | | | | | | | | |
| | 209 | Sm | 10.2 | 56.5 | | 2.5 | 0.7 | 3.9 |
| | 210 | Sm | 10.2 | 28.8 | | 2.5 | 0.0 | 3.9 |
| | 211 | Lg | 5.0 | 15.6 | | 2.5 | 0.7 | 2.5 |
| | 212 | Lg | 7.6 | 16.7 | | 0.0 | 0.0 | 2.9 |
| | Average | | | | | | | |
| Ionic strength effects- Paragneiss (50/50 mix of grainsizes), pH=9, Hi and Lo TDS | | | | | | | | |
| | 213 | Hi | 7.1 | 14.2 | | 5.0 | 1.2 | 2.9 |
| | 214 | Hi | 8.1 | 14.1 | | 5.0 | 1.4 | 2.9 |
| | 215 | Lo | 11.1 | 20.0 | | 2.5 | 1.4 | 3.0 |
| | 216 | Lo | 15.6 | 20.1 | | 2.5 | 1.2 | 3.6 |
| | Average | | | | | | | |
| Rock Type Effects- pH=9, Hi analytes, Ortho gneiss (1) and granite (2)(50/50 size mix) | | | | | | | | |
| | 218 (1) | | 2.8 | 11.8 | | 2.5 | 0.0 | 1.4 |
| | 218 (1) | | 3.6 | 15.6 | | 2.5 | 0.0 | 1.6 |
| | 220 (2) | | 1.9 | 8.6 | | 2.5 | 0.7 | 1.0 |
| | 220 (2) | | 1.9 | 3.8 | | 2.5 | 0.0 | 1.0 |
| | Average | | | | | | | |

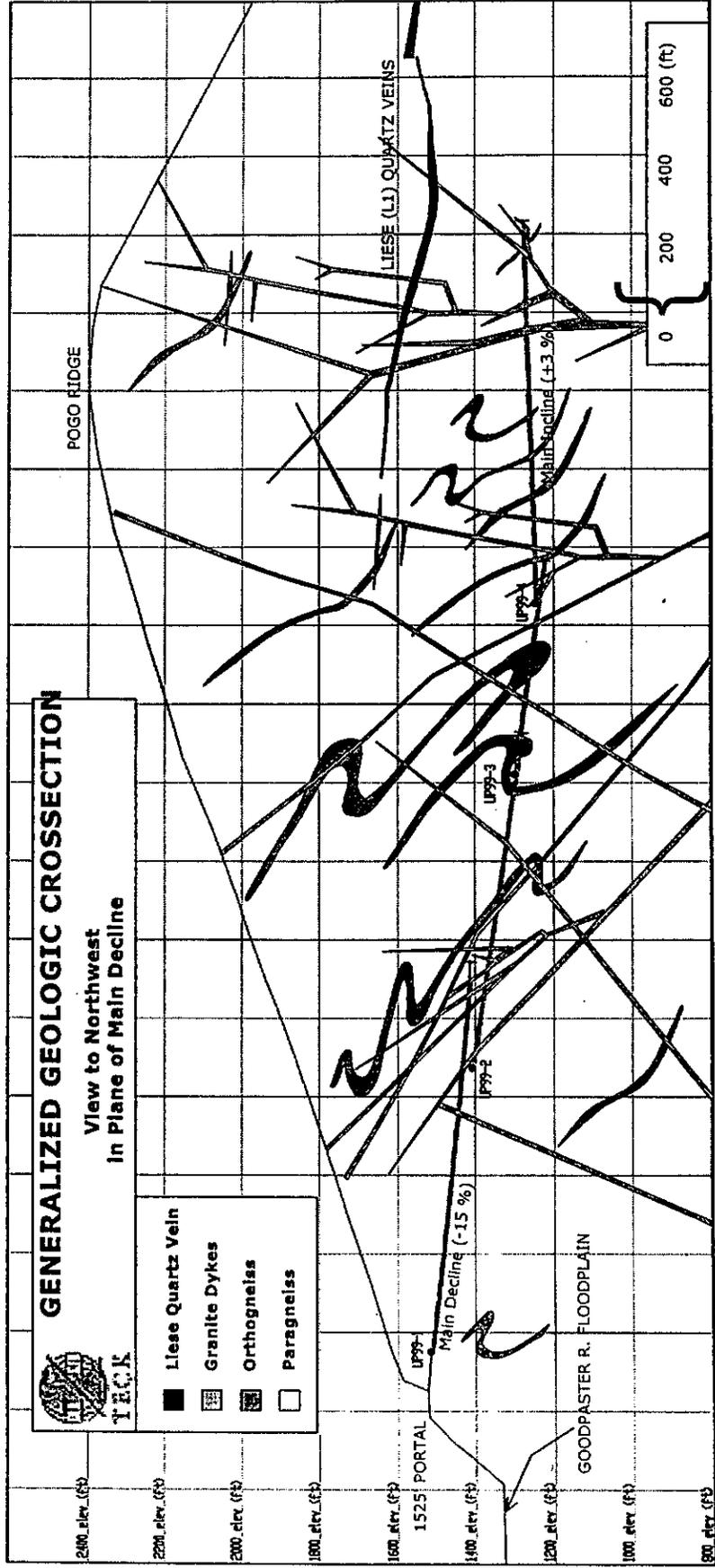
FIGURES

GENERALIZED GEOLOGIC CROSSSECTION

View to Northwest
In Plane of Main Decline



- Liese Quartz Vein
- Granite Dykes
- Orthogneiss
- Paragneiss



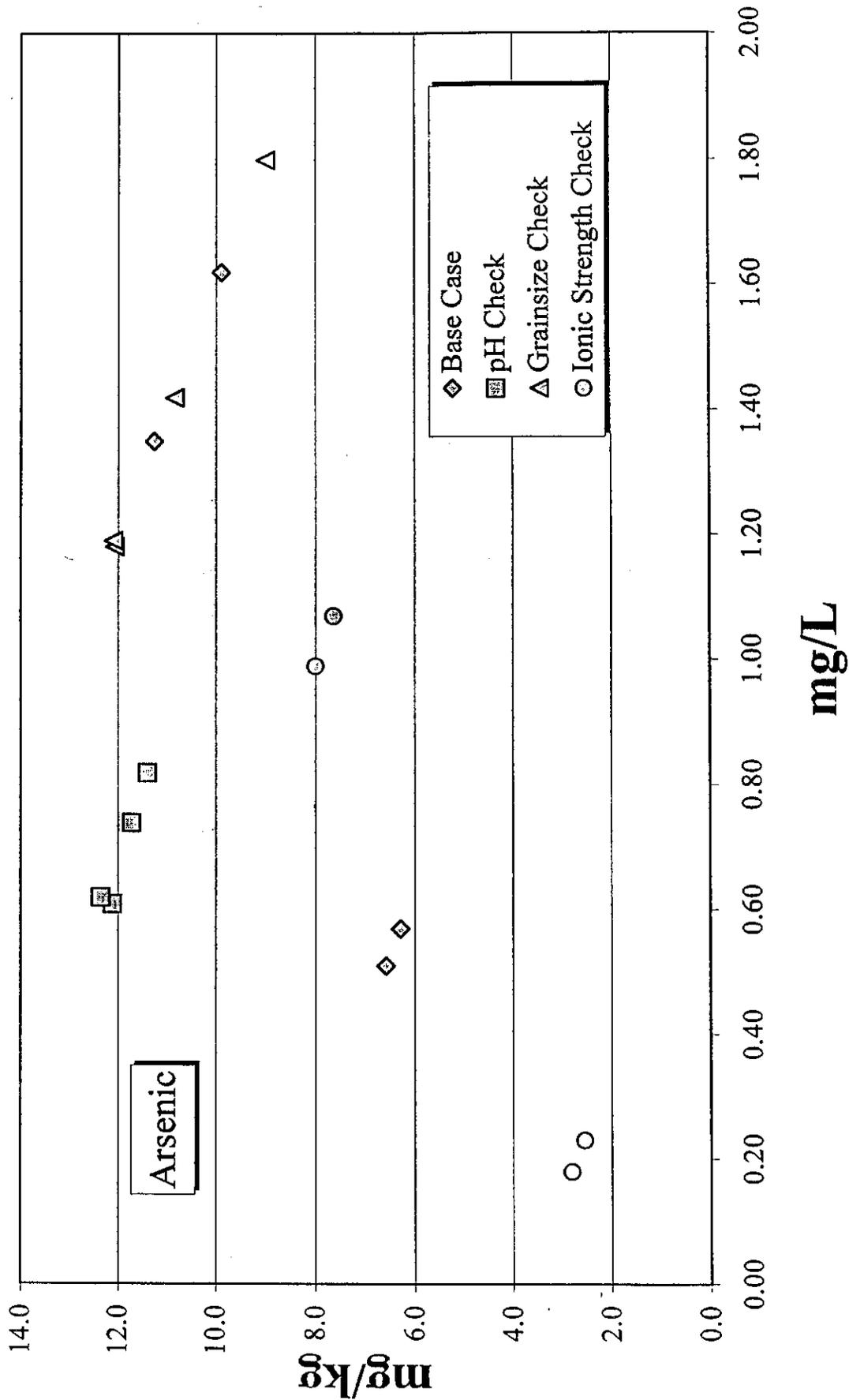


Figure 2. Experimental results for arsenic.

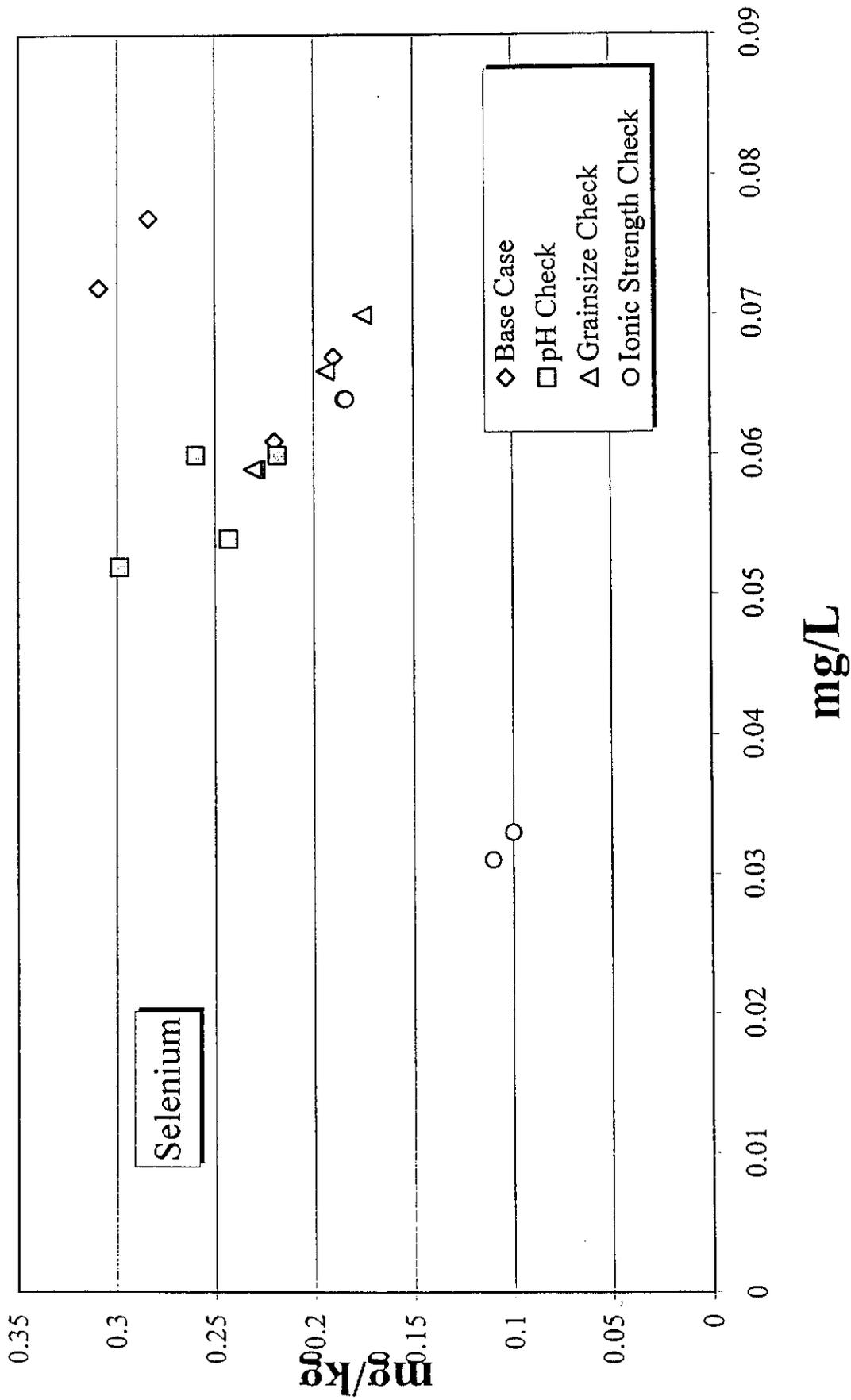


Figure 3. Experimental results for selenium.

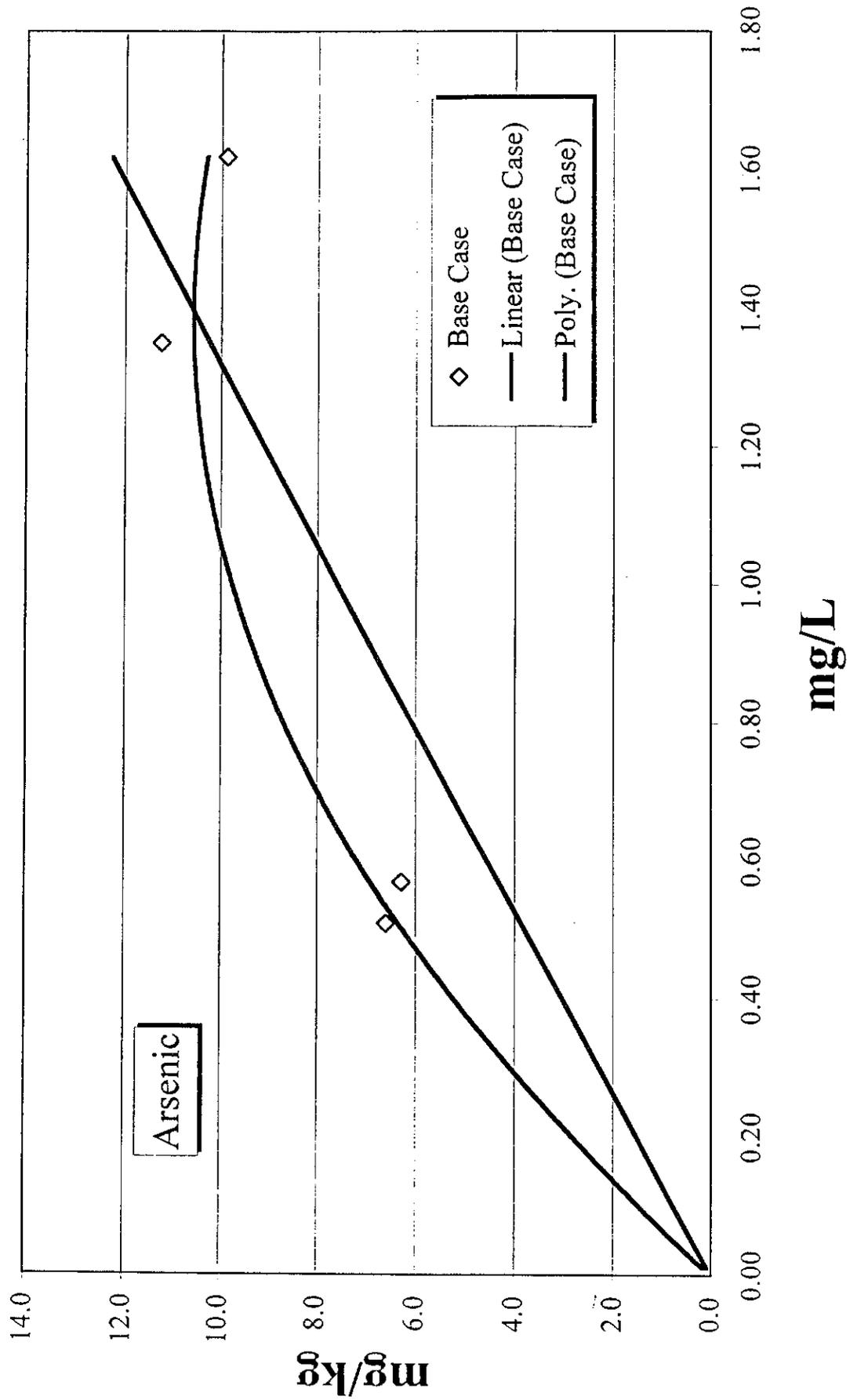


Figure 4. Base case arsenic performance.

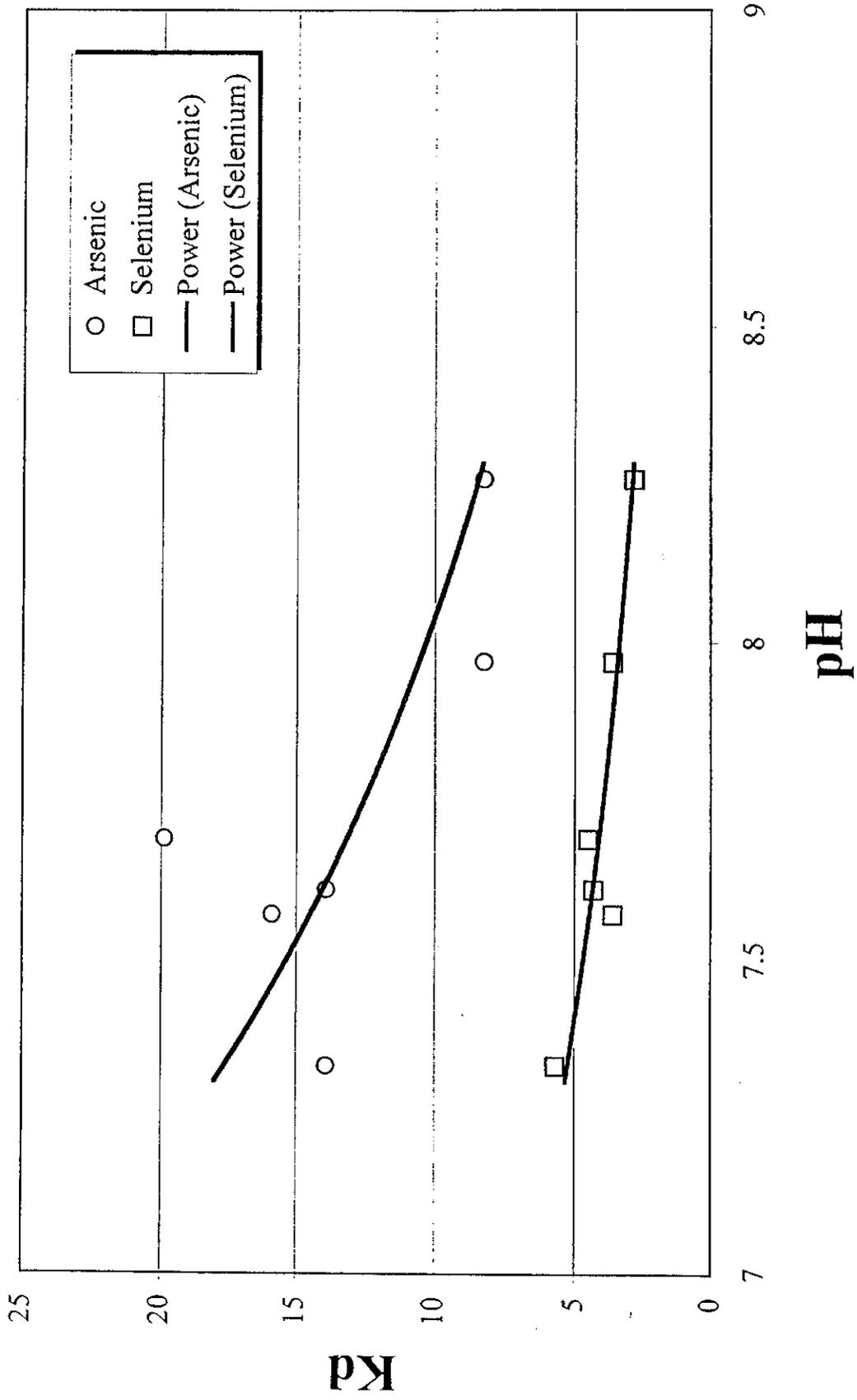


Figure 5. Variation of K_d with pH.

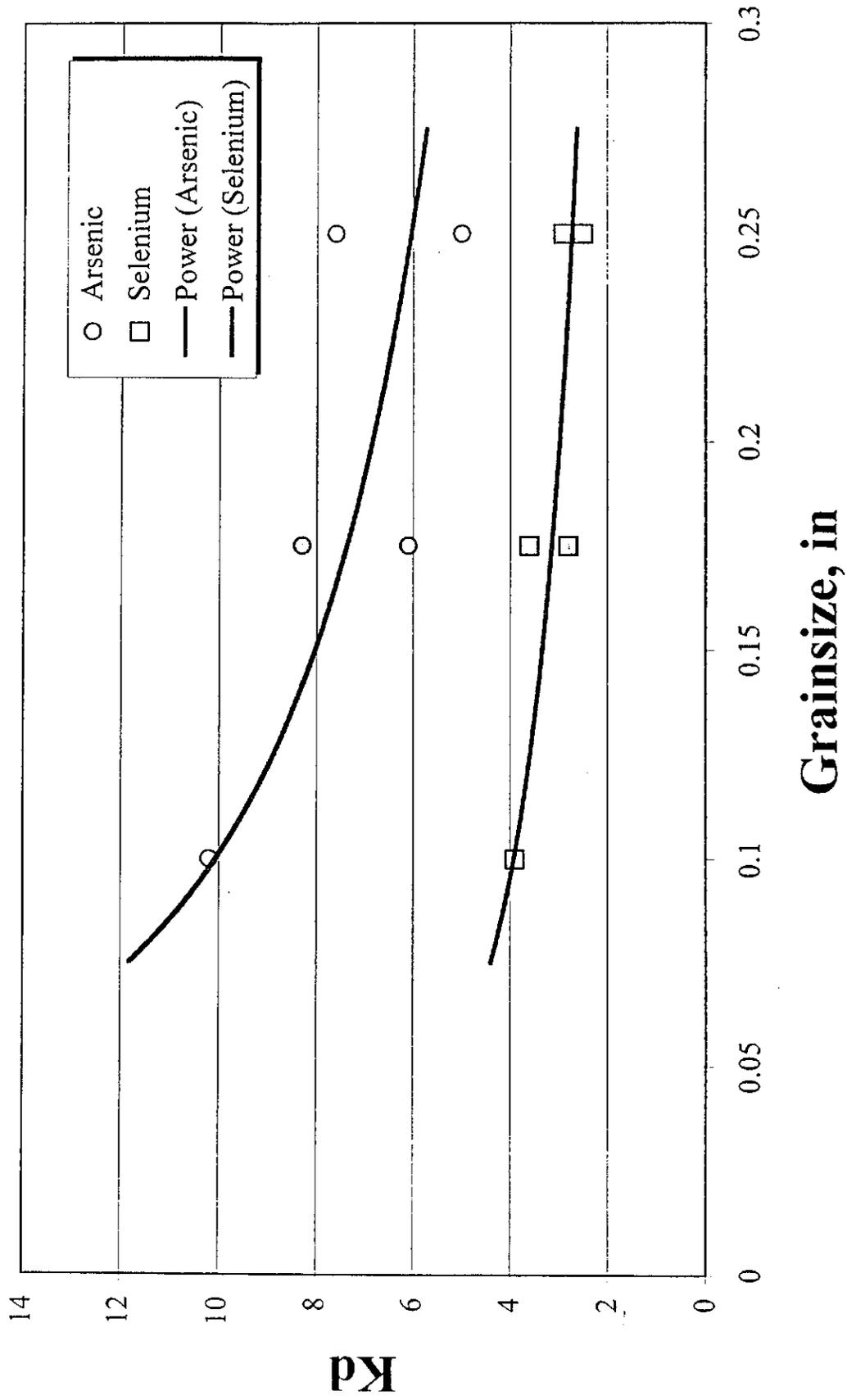


Figure 6. Variation of K_d with grainsize.

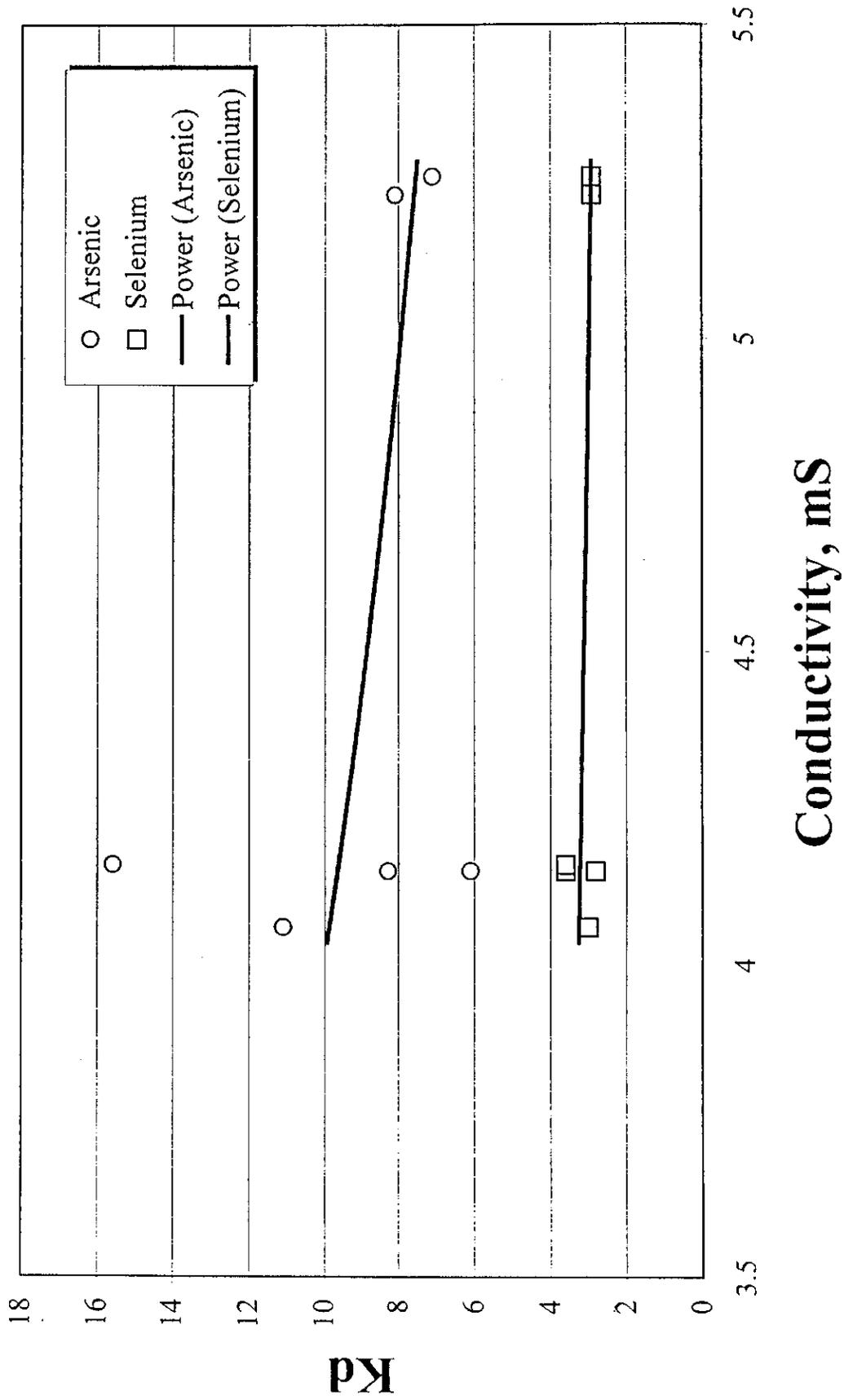


Figure 7. Variation of Kd with total dissolved solids.

ATTACHMENT ONE

STANDARD OPERATING
PROCEDURE
for

**Partition Coefficient
Determination**

Prepared for:

General Procedures
For All Clients and Projects

June 16, 1998
SOP-TST056



AdrianBrown

*Groundwater Hydrology, Geochemistry, Remediation
Innovative Environmental Solutions*

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Denver, Colorado 80226-1801
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1. PURPOSE

This document defines the Standard Operating Procedure (SOP) for laboratory determination of the partition coefficient, or K_d . The partition coefficient is used to determine the extent to which dissolved solutes may adsorb onto the surfaces of solid phases that the solution contacts. It is, a linear adsorption isotherm and allows for infinite adsorption.

This procedure is designed to provide a determination of K_d using study site solid materials and, when available, solutions collected at the site. Because the valid value of K_d is dependant upon specific solid phase characteristics and solution bulk composition, the use of site-specific materials extends the defensibility of K_d values obtained using this procedure.

This procedure is not suitable for combining low pH solutions with acid neutralizing materials like limestone, or other forms of calcium carbonate. Attenuation of metals or other solution solutes under these neutralization conditions is governed more by solubility concerns than simple adsorption.

2. MATERIALS REQUIRED

2.1 Apparatus

- 1 L polyethylene bottles that have been acid rinsed with a nitric acid solution (~10% will suffice)
- A scale or balance capable of measuring 100 ± 0.5 g
- A 500 mL graduated cylinder
- Solution filtration equipment ($0.45\mu\text{m}$)

2.2 Reagents

- Solids collected from the study site
- Ground or surface water collected at the study site. If waters are not available from the site, a synthetic stock solution must be prepared
- 1000 ± 1 mg/L metal standard solutions for the solutes of interest

3. SAMPLE MATERIAL

3.1 Field Sampling

Solids for laboratory analysis may be obtained from surface or subsurface locations, depending on whether ground or surface water fate and transport of particular interest. Solids should be collected from locations that are as representative of the solid as possible. For site wide modeling efforts, composite samples of various lithologies are appropriate to develop representative K_d 's.

5. DATA ANALYSIS

The K_d for solids tested is calculated simply as determining the mass of an element of concern that is removed from solution and dividing that mass by the weight of the solid used in the testing. This ratio is subsequently graphed against the final concentration of the solution used in the test. The data point of 0 mg/kg and 0 mg/L is valid (indicating no adsorption when concentration is zero) and is made part of the graph. The resulting data are linearly regressed and the slope of the fit is the value of the partition coefficient, K_d . Otherwise, under certain circumstances, a simple average of the K_d values measured for each point may be averaged. The specifics of this procedure are presented below.

1. Calculate the difference in concentration between the initial and final solution (C_L), with the units of mg/L
2. Multiply this difference by the volume of the solution used in the experiment (0.5 L) to produce a value for the mass of the specific element removed from solution (mg).
3. Divide the value mg by the mass of the solid used in the test (kg) to yield a concentration of the element adsorbed onto the solid (mg/kg = C_S)
4. Prepare a graph of C_S against the corresponding C_L , being certain to include the point 0,0.
5. Produce a linear least squares regression of the graphed data and determine the slope.
6. Report the K_d for the solid toward the specific element considered as the slope of the best fit.

ATTACHMENT TWO

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 333 W. Bayaud Ave.
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 Mark Williamson

Lab Sample ID: L28695-05
 Client Sample ID: Pogo 105
 Client Project ID: 1543A-Pogo Mine
 ACZ Report ID: RG127153

Date Sampled: 08/23/2000 4:30:00 PM
 Date Received: 08/25/2000
 Date Reported: 08/28/2000

Sample Matrix: Ground Water

Metals Analysis

| Parameter | EPA Method | Result | Qual | Units | MDL | PQL | Date | Analyst |
|---------------------|--------------------------|--------|------|-------|-------|------|-----------|---------|
| Antimony, dissolved | M204.2 GFAA | 0.09 | | mg/L | 0.01 | 0.05 | 8/26/2000 | jl |
| Arsenic, dissolved | M206.2 GFAA | 2.6 | | mg/L | 0.1 | 0.5 | 8/26/2000 | jl |
| Cadmium, dissolved | M200.7 ICP | 0.023 | B | mg/L | 0.006 | 0.03 | 8/28/2000 | kr |
| Copper, dissolved | M200.7 ICP | | U | mg/L | 0.02 | 0.1 | 8/28/2000 | kr |
| Nickel, dissolved | M200.7 ICP | 0.04 | B | mg/L | 0.02 | 0.1 | 8/28/2000 | kr |
| Selenium, dissolved | SM 3500-Se C, AA-Hydride | 0.101 | | mg/L | 0.005 | 0.03 | 8/25/2000 | sjs |
| Silver, dissolved | M200.7 ICP | 0.03 | B | mg/L | 0.01 | 0.05 | 8/28/2000 | kr |

Inorganic Qualifiers (based on EPA CLP 3/90)

U = Analyte was analyzed for but not detected at the indicated MDL
 B = Analyte concentration detected at a value between MDL and PQL
 PQL = Practical Quantitation Limit



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 Mark Williamson

Lab Sample ID: L28695-03
 Client Sample ID: Pogo 103
 Client Project ID: 1543A-Pogo Mine
 ACZ Report ID: RG127151

Date Sampled: 08/24/2000 2:05:00 PM
 Date Received: 08/25/2000
 Date Reported: 08/28/2000

Sample Matrix: Ground Water

Metals Analysis

| Parameter | EPA Method | Result | Qual | Units | MDL | PQL | Date | Analyst |
|---------------------|--------------------------|--------|------|-------|-------|------|-----------|---------|
| Antimony, dissolved | M204.2 GFAA | 0.08 | | mg/L | 0.01 | 0.05 | 8/26/2000 | jl |
| Arsenic, dissolved | M206.2 GFAA | 3.1 | | mg/L | 0.1 | 0.5 | 8/26/2000 | jl |
| Cadmium, dissolved | M200.7 ICP | 0.273 | | mg/L | 0.006 | 0.03 | 8/28/2000 | kr |
| Copper, dissolved | M200.7 ICP | | U | mg/L | 0.02 | 0.1 | 8/28/2000 | kr |
| Nickel, dissolved | M200.7 ICP | 0.20 | | mg/L | 0.02 | 0.1 | 8/28/2000 | kr |
| Selenium, dissolved | SM 3500-Se C, AA-Hydride | 0.104 | | mg/L | 0.005 | 0.03 | 8/25/2000 | sjs |
| Silver, dissolved | M200.7 ICP | 0.01 | B | mg/L | 0.01 | 0.05 | 8/28/2000 | kr |

Inorganic Qualifiers (based on EPA CLP 3/90)

U = Analyte was analyzed for but not detected at the indicated MDL
 B = Analyte concentration detected at a value between MDL and PQL
 PQL = Practical Quantitation Limit



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Lab Sample ID: L28695-01
 Client Sample ID: Pogo 101
 Client Project ID: 1543A-Pogo Mine
 ACZ Report ID: RG127149

Adrian Brown Consultants, Inc.
 333 W. Bayaud Ave.
 Denver, CO 80223
 Mark Williamson

Date Sampled: 08/24/2000 2:10:00 PM
 Date Received: 08/25/2000
 Date Reported: 08/28/2000

Sample Matrix: Ground Water

Metals Analysis

| Parameter | EPA Method | Result | Qual | Units | MDL | PQL | Date | Analyst |
|---------------------|-------------------------|--------|------|-------|-------|------|-----------|---------|
| Antimony, dissolved | M204.2 GFAA | 0.08 | | mg/L | 0.01 | 0.05 | 8/26/2000 | jl |
| Arsenic, dissolved | M206.2 GFAA | 3.6 | | mg/L | 0.1 | 0.5 | 8/26/2000 | jl |
| Cadmium, dissolved | M200.7 ICP | 0.074 | | mg/L | 0.006 | 0.03 | 8/28/2000 | kr |
| Copper, dissolved | M200.7 ICP | | U | mg/L | 0.02 | 0.1 | 8/28/2000 | kr |
| Nickel, dissolved | M200.7 ICP | 0.03 | B | mg/L | 0.02 | 0.1 | 8/28/2000 | kr |
| Selenium, dissolved | SM 3500-Se C, AA-Hydrde | 0.105 | | mg/L | 0.005 | 0.03 | 8/25/2000 | sjjs |
| Silver, dissolved | M200.7 ICP | 0.01 | B | mg/L | 0.01 | 0.05 | 8/28/2000 | kr |

Inorganic Qualifiers (based on EPA CLP 3/90)
 U = Analyte was analyzed for but not detected at the indicated MDL
 B = Analyte concentration detected at a value between MDL and PQL
 PQL = Practical Quantitation Limit



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Lab Sample ID: **L28695-07**
 Client Sample ID: **Pogo 201**
 Client Project ID: **1543A-Pogo Mine**
 ACZ Report ID: **RG127155**

Adrian Brown Consultants, Inc.
 333 W. Bayaud Ave.
 Denver, CO 80223
 Mark Williamson

Date Sampled: **08/24/2000 3:05:00 PM**
 Date Received: **08/25/2000**
 Date Reported: **08/28/2000**

Sample Matrix: **Ground Water**

Metals Analysis

| Parameter | EPA Method | Result | Qual | Units | MDL | PQL | * Date | Analyst |
|---------------------|--------------------------|--------|------|-------|-------|------|-----------|---------|
| Antimony, dissolved | M204.2 GFAA | 0.07 | | mg/L | 0.01 | 0.05 | 8/26/2000 | jl |
| Arsenic, dissolved | M206.2 GFAA | 1.35 | | mg/L | 0.05 | 0.3 | 8/26/2000 | jl |
| Cadmium, dissolved | M200.7 ICP | | U | mg/L | 0.006 | 0.03 | 8/28/2000 | kr |
| Copper, dissolved | M200.7 ICP | | U | mg/L | 0.02 | 0.1 | 8/28/2000 | kr |
| Nickel, dissolved | M200.7 ICP | 0.02 | B | mg/L | 0.02 | 0.1 | 8/28/2000 | kr |
| Selenium, dissolved | SM 3500-Se C, AA-Hydride | 0.061 | | mg/L | 0.005 | 0.03 | 8/25/2000 | sjs |
| Silver, dissolved | M200.7 ICP | | U | mg/L | 0.01 | 0.05 | 8/28/2000 | kr |

Inorganic Qualifiers (based on EPA CLP 3/90)
 U = Analyte was analyzed for but not detected at the indicated MDL
 B = Analyte concentration detected at a value between MDL and PQL
 PQL = Practical Quantitation Limit



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Lab Sample ID: L28695-09
 Client Sample ID: Pogo 203
 Client Project ID: 1543A-Pogo Mine
 ACZ Report ID: RG127157

Adrian Brown Consultants, Inc.
 333 W. Bayaud Ave.
 Denver, CO 80223
 Mark Williamson

Date Sampled: 08/24/2000 3:10:00 PM
 Date Received: 08/25/2000
 Date Reported: 08/28/2000

Sample Matrix: Ground Water

Metals Analysis

| Parameter | EPA Method | Result | Qual | Units | MDL | PQL | Date | Analyst |
|---------------------|--------------------------|--------|------|-------|-------|------|-----------|---------|
| Antimony, dissolved | M204.2 GFAA | 0.09 | | mg/L | 0.01 | 0.05 | 8/26/2000 | jl |
| Arsenic, dissolved | M206.2 GFAA | 0.57 | | mg/L | 0.03 | 0.1 | 8/26/2000 | jl |
| Cadmium, dissolved | M200.7 ICP | | U | mg/L | 0.006 | 0.03 | 8/28/2000 | kr |
| Copper, dissolved | M200.7 ICP | | U | mg/L | 0.02 | 0.1 | 8/28/2000 | kr |
| Nickel, dissolved | M200.7 ICP | 0.02 | B | mg/L | 0.02 | 0.1 | 8/28/2000 | kr |
| Selenium, dissolved | SM 3500-Se C, AA-Hydride | 0.077 | | mg/L | 0.005 | 0.03 | 8/25/2000 | sj |
| Silver, dissolved | M200.7 ICP | | U | mg/L | 0.01 | 0.05 | 8/28/2000 | kr |

Inorganic Qualifiers (based on EPA CLP 3/90)
 U = Analyte was analyzed for but not detected at the indicated MDL
 B = Analyte concentration detected at a value between MDL and PQL
 PQL = Practical Quantitation Limit



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 Mark Williamson

Lab Sample ID: **L28695-11**
 Client Sample ID: **Pogo 205**
 Client Project ID: **1543A-Pogo Mine**
 ACZ Report ID: **RG127159**

Date Sampled: **08/24/2000 3:20:00 PM**
 Date Received: **08/25/2000**
 Date Reported: **08/28/2000**

Sample Matrix: **Ground Water**

Metals Analysis

| Parameter | EPA Method | Result | Qual | Units | MDL | PQL | Date | Analyst |
|---------------------|--------------------------|--------|------|-------|-------|------|-----------|---------|
| Antimony, dissolved | M204.2 GFAA | 0.060 | | mg/L | 0.004 | 0.02 | 8/26/2000 | jl |
| Arsenic, dissolved | M206.2 GFAA | 0.61 | | mg/L | 0.03 | 0.1 | 8/26/2000 | jl |
| Cadmium, dissolved | M200.7 ICP | | U | mg/L | 0.006 | 0.03 | 8/28/2000 | kr |
| Copper, dissolved | M200.7 ICP | | U | mg/L | 0.02 | 0.1 | 8/28/2000 | kr |
| Nickel, dissolved | M200.7 ICP | 0.04 | B | mg/L | 0.02 | 0.1 | 8/28/2000 | kr |
| Selenium, dissolved | SM 3500-Se C, AA-Hydride | 0.054 | | mg/L | 0.005 | 0.03 | 8/25/2000 | sjs |
| Silver, dissolved | M200.7 ICP | | U | mg/L | 0.01 | 0.05 | 8/28/2000 | kr |

Inorganic Qualifiers (based on EPA CLP 3/90)

U = Analyte was analyzed for but not detected at the indicated MDL
 B = Analyte concentration detected at a value between MDL and PQL
 PQL = Practical Quantitation Limit



Ralph Poulsen (VP) / Scott Habermehl (PM)

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Lab Sample ID: L28695-13
 Client Sample ID: Pogo 207
 Client Project ID: 1543A-Pogo Mine
 ACZ Report ID: RG127161

Adrian Brown Consultants, Inc.
 333 W. Bayaud Ave.
 Denver, CO 80223
 Mark Williamson

Date Sampled: 08/24/2000 3:27:00 PM
 Date Received: 08/25/2000
 Date Reported: 08/28/2000

Sample Matrix: Ground Water

Metals Analysis

| Parameter | EPA Method | Result | Qual | Units | MDL | PQL | Date | Analyst |
|---------------------|--------------------------|--------|------|-------|-------|------|-----------|---------|
| Antimony, dissolved | M204.2 GFAA | 0.07 | | mg/L | 0.01 | 0.05 | 8/26/2000 | jl |
| Arsenic, dissolved | M206.2 GFAA | 0.82 | | mg/L | 0.03 | 0.1 | 8/26/2000 | jl |
| Cadmium, dissolved | M200.7 ICP | 0.017 | B | mg/L | 0.006 | 0.03 | 8/28/2000 | kr |
| Copper, dissolved | M200.7 ICP | | U | mg/L | 0.02 | 0.1 | 8/28/2000 | kr |
| Nickel, dissolved | M200.7 ICP | 0.10 | B | mg/L | 0.02 | 0.1 | 8/28/2000 | kr |
| Selenium, dissolved | SM 3500-Se C, AA-Hydride | 0.060 | | mg/L | 0.005 | 0.03 | 8/25/2000 | sjs |
| Silver, dissolved | M200.7 ICP | | U | mg/L | 0.01 | 0.05 | 8/28/2000 | kr |

Inorganic Qualifiers (Based on EPA CLP 3/90)

U = Analyte was analyzed for but not detected at the indicated MDL
 B = Analyte concentration detected at a value between MDL and PQL
 PQL = Practical Quantitation Limit


 Ralph Poulsen (VP) / Scott Habermehl (PM)

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Lab Sample ID: **L28695-15**
 Client Sample ID: **Pogo 209**
 Client Project ID: **1543A-Pogo Mine**
 ACZ Report ID: **RG127163**

Adrian Brown Consultants, Inc.
 333 W. Bayaud Ave.
 Denver, CO 80223
 Mark Williamson

Date Sampled: **08/24/2000 3:40:00 PM**
 Date Received: **08/25/2000**
 Date Reported: **08/28/2000**

Sample Matrix: **Ground Water**

Metals Analysis

| Parameter | EPA Method | Result | Qual | Units | MDL | PQL | Date | Analyst |
|---------------------|--------------------------|--------|------|-------|-------|------|-----------|---------|
| Antimony, dissolved | M204.2 GFAA | 0.07 | | mg/L | 0.01 | 0.05 | 8/26/2000 | jl |
| Arsenic, dissolved | M206.2 GFAA | 1.18 | | mg/L | 0.03 | 0.1 | 8/26/2000 | jl |
| Cadmium, dissolved | M200.7 ICP | 0.006 | B | mg/L | 0.006 | 0.03 | 8/28/2000 | kr |
| Copper, dissolved | M200.7 ICP | | U | mg/L | 0.02 | 0.1 | 8/28/2000 | kr |
| Nickel, dissolved | M200.7 ICP | | U | mg/L | 0.02 | 0.1 | 8/28/2000 | kr |
| Selenium, dissolved | SM 3500-Se C, AA-Hydride | 0.059 | | mg/L | 0.005 | 0.03 | 8/25/2000 | sjs |
| Silver, dissolved | M200.7 ICP | | U | mg/L | 0.01 | 0.05 | 8/28/2000 | kr |

Inorganic Qualifiers (based on EPA CLP 3/91)
 U = Analyte was analyzed for but not detected at the indicated MDL
 B = Analyte concentration detected at a value between MDL and PQL
 PQL = Practical Quantitation Limit



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Lab Sample ID: L28695-17
 Client Sample ID: Pogo 211
 Client Project ID: 1543A-Pogo Mine
 ACZ Report ID: RG127165

Adrian Brown Consultants, Inc.
 333 W. Bayaud Ave.
 Denver, CO 80223
 Mark Williamson

Date Sampled: 08/24/2000 3:47:00 PM
 Date Received: 08/25/2000
 Date Reported: 08/28/2000

Sample Matrix: Ground Water

Metals Analysis

| Parameter | EPA Method | Result | Qual | Units | MDL | PQL | Date | Analyst |
|---------------------|--------------------------|--------|------|-------|-------|------|-----------|---------|
| Antimony, dissolved | M204.2 GFAA | 0.07 | | mg/L | 0.01 | 0.05 | 8/26/2000 | jl |
| Arsenic, dissolved | M206.2 GFAA | 1.8 | | mg/L | 0.1 | 0.5 | 8/26/2000 | jl |
| Cadmium, dissolved | M200.7 ICP | 0.018 | B | mg/L | 0.006 | 0.03 | 8/28/2000 | kr |
| Copper, dissolved | M200.7 ICP | | U | mg/L | 0.02 | 0.1 | 8/28/2000 | kr |
| Nickel, dissolved | M200.7 ICP | 0.02 | B | mg/L | 0.02 | 0.1 | 8/28/2000 | kr |
| Selenium, dissolved | SM 3500-Se C, AA-Hydride | 0.070 | | mg/L | 0.005 | 0.03 | 8/25/2000 | sjs |
| Silver, dissolved | M200.7 ICP | | U | mg/L | 0.01 | 0.05 | 8/28/2000 | kr |

Inorganic Qualifiers (based on EPA CLP 3/90)
 U = Analyte was analyzed for but not detected at the indicated MDL
 B = Analyte concentration detected at a value between MDL and PQL
 PQL = Practical Quantitation Limit



Ralph Poulsen (VP) / Scott Habermehl (PM)

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Lab Sample ID: L28695-19
 Client Sample ID: Pogo 213
 Client Project ID: 1543A-Pogo Mine
 ACZ Report ID: RG127167

Adrian Brown Consultants, Inc.
 333 W. Bayaud Ave.
 Denver, CO 80223
 Mark Williamson

Date Sampled: 08/24/2000 4:30:00 PM
 Date Received: 08/25/2000
 Date Reported: 08/28/2000

Sample Matrix: Ground Water

Metals Analysis

| Parameter | EPA Method | Result | Qual | Units | MDL | PQL | Date | Analyst |
|---------------------|--------------------------|--------|------|-------|-------|------|-----------|---------|
| Antimony, dissolved | M204.2 GFAA | 0.073 | | mg/L | 0.008 | 0.04 | 8/26/2000 | jl |
| Arsenic, dissolved | M206.2 GFAA | 1.07 | | mg/L | 0.03 | 0.1 | 8/26/2000 | jl |
| Cadmium, dissolved | M200.7 ICP | | U | mg/L | 0.006 | 0.03 | 8/28/2000 | kr |
| Copper, dissolved | M200.7 ICP | | U | mg/L | 0.02 | 0.1 | 8/28/2000 | kr |
| Nickel, dissolved | M200.7 ICP | | U | mg/L | 0.02 | 0.1 | 8/28/2000 | kr |
| Selenium, dissolved | SM 3500-Se C, AA-Hydride | 0.064 | | mg/L | 0.005 | 0.03 | 8/25/2000 | sjs |
| Silver, dissolved | M200.7 ICP | | U | mg/L | 0.01 | 0.05 | 8/28/2000 | kr |

Inorganic Qualifiers (based on EPA CLP 3/90)

U = Analyte was analyzed for but not detected at the indicated MDL
 B = Analyte concentration detected at a value between MDL and PQL
 PQL = Practical Quantitation Limit



Ralph Poulsen (VP) / Scott Habermehl (PM)

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Lab Sample ID: L28695-21
 Client Sample ID: Pogo 215
 Client Project ID: 1543A-Pogo Mine
 ACZ Report ID: RG127169

Adrian Brown Consultants, Inc.
 333 W. Bayaud Ave.
 Denver, CO 80223
 Mark Williamson

Date Sampled: 08/24/2000 4:37:00 PM
 Date Received: 08/25/2000
 Date Reported: 08/28/2000

Sample Matrix: Ground Water

Metals Analysis

| Parameter | EPA Method | Result | Qual | Units | MDL | PQL | Date | Analyst |
|---------------------|--------------------------|--------|------|-------|-------|-------|-----------|---------|
| Antimony, dissolved | M204.2 GFAA | 0.037 | | mg/L | 0.002 | 0.01 | 8/26/2000 | jl |
| Arsenic, dissolved | M206.2 GFAA | 0.23 | | mg/L | 0.01 | 0.05 | 8/26/2000 | jl |
| Cadmium, dissolved | M200.7 ICP | | U | mg/L | 0.006 | 0.03 | 8/28/2000 | kr |
| Copper, dissolved | M200.7 ICP | | U | mg/L | 0.02 | 0.1 | 8/28/2000 | kr |
| Nickel, dissolved | M200.7 ICP | | U | mg/L | 0.02 | 0.1 | 8/28/2000 | kr |
| Selenium, dissolved | SM 3500-Se C, AA-Hydride | 0.033 | | mg/L | 0.001 | 0.005 | 8/25/2000 | sjs |
| Silver, dissolved | M200.7 ICP | | U | mg/L | 0.01 | 0.05 | 8/28/2000 | kr |

Inorganic Qualifiers (based on EPA CLP 3/90)

U = Analyte was analyzed for but not detected at the indicated MDL
 B = Analyte concentration detected at a value between MDL and PQL
 PQL = Practical Quantitation Limit



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Lab Sample ID: **L28695-23**
 Client Sample ID: **Pogo 217**
 Client Project ID: **1543A-Pogo Mine**
 ACZ Report ID: **RG127171**

Date Sampled: **08/24/2000 4:45:00 PM**
 Date Received: **08/25/2000**
 Date Reported: **08/28/2000**

Sample Matrix: **Ground Water**

Metals Analysis

| Parameter | EPA Method | Result | Qual | Units | MDL | PQL | Date | Analyst |
|---------------------|--------------------------|--------|------|-------|-------|-------|-----------|---------|
| Antimony, dissolved | M204.2 GFAA | 0.003 | B | mg/L | 0.002 | 0.01 | 8/26/2000 | jl |
| Arsenic, dissolved | M206.2 GFAA | 0.007 | | mg/L | 0.001 | 0.005 | 8/27/2000 | jl |
| Cadmium, dissolved | M200.7 ICP | | U | mg/L | 0.006 | 0.03 | 8/28/2000 | kr |
| Copper, dissolved | M200.7 ICP | | U | mg/L | 0.02 | 0.1 | 8/28/2000 | kr |
| Nickel, dissolved | M200.7 ICP | | U | mg/L | 0.02 | 0.1 | 8/28/2000 | kr |
| Selenium, dissolved | SM 3500-Se C, AA-Hydride | | U | mg/L | 0.001 | 0.005 | 8/25/2000 | sjs |
| Silver, dissolved | M200.7 ICP | | U | mg/L | 0.01 | 0.05 | 8/28/2000 | kr |

Inorganic Qualifiers (based on EPA CLP 3/90)

U = Analyte was analyzed for but not detected at the indicated MDL
 B = Analyte concentration detected at a value between MDL and PQL
 PQL = Practical Quantitation Limit



Ralph Poulsen (VP) / Scott Habermehl (PM)

ACZ Laboratories, Inc.
 2773 Downhill Drive
 Steamboat Springs, CO 80487
 (800) 334-5493

Lab Sample ID: **L28695-25**
 Client Sample ID: **Pogo 219**
 Client Project ID: **1543A-Pogo Mine**
 ACZ Report ID: **RG127173**

Adrian Brown Consultants, Inc.
 333 W. Bayaud Ave.
 Denver, CO 80223
 Mark Williamson

Date Sampled: **08/24/2000 4:58:00 PM**
 Date Received: **08/25/2000**
 Date Reported: **08/28/2000**

Sample Matrix: **Ground Water**

Metals Analysis

| Parameter | EPA Method | Result | Qual | Units | MDL | PQL | Date | Analyst |
|---------------------|--------------------------|--------|------|-------|-------|------|-----------|---------|
| Antimony, dissolved | M204.2 GFAA | 0.08 | | mg/L | 0.01 | 0.05 | 8/26/2000 | jl |
| Arsenic, dissolved | M206.2 GFAA | 2.1 | | mg/L | 0.1 | 0.5 | 8/26/2000 | jl |
| Cadmium, dissolved | M200.7 ICP | 0.018 | B | mg/L | 0.006 | 0.03 | 8/28/2000 | kr |
| Copper, dissolved | M200.7 ICP | | U | mg/L | 0.02 | 0.1 | 8/28/2000 | kr |
| Nickel, dissolved | M200.7 ICP | 0.02 | B | mg/L | 0.02 | 0.1 | 8/28/2000 | kr |
| Selenium, dissolved | SM 3500-Se C, AA-Hydride | 0.080 | | mg/L | 0.005 | 0.03 | 8/25/2000 | sjs |
| Silver, dissolved | M200.7 ICP | | U | mg/L | 0.01 | 0.05 | 8/28/2000 | kr |

Inorganic Qualifiers (based on EPA CLP 3/90)
 U = Analyte was analyzed for but not detected at the indicated MDL
 B = Analyte concentration detected at a value between MDL and PQL
 PQL = Practical Quantitation Limit



Ralph Poulsen (VP) / Scott Habermehl (PM)

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 333 W. Bayaud Ave.
 Denver, CO 80223
 Mark Williamson

Lab Sample ID: **L28695-27**
 Client Sample ID: **Pogo 221**
 Client Project ID: **1543A-Pogo Mine**
 ACZ Report ID: **RG127175**

Date Sampled: **08/24/2000 5:10:00 PM**
 Date Received: **08/25/2000**
 Date Reported: **08/28/2000**

Sample Matrix: **Ground Water**

Metals Analysis

| Parameter | EPA Method | Result | Qual | Units | MDL | PQL | Date | Analyst |
|---------------------|--------------------------|--------|------|-------|-------|------|-----------|---------|
| Antimony, dissolved | M204.2 GFAA | 0.08 | | mg/L | 0.01 | 0.05 | 8/26/2000 | jl |
| Arsenic, dissolved | M206.2 GFAA | 2.6 | | mg/L | 0.1 | 0.5 | 8/26/2000 | jl |
| Cadmium, dissolved | M200.7 ICP | 0.042 | | mg/L | 0.006 | 0.03 | 8/28/2000 | kr |
| Copper, dissolved | M200.7 ICP | | U | mg/L | 0.02 | 0.1 | 8/28/2000 | kr |
| Nickel, dissolved | M200.7 ICP | | U | mg/L | 0.02 | 0.1 | 8/28/2000 | kr |
| Selenium, dissolved | SM 3500-Se C, AA-Hydride | 0.088 | | mg/L | 0.005 | 0.03 | 8/25/2000 | sjs |
| Silver, dissolved | M200.7 ICP | | U | mg/L | 0.01 | 0.05 | 8/28/2000 | kr |

Inorganic Qualifiers (based on EPA CLP 3/90)

U = Analyte was analyzed for but not detected at the indicated MDL
 B = Analyte concentration detected at a value between MDL and PQL
 PQL = Practical Quantitation Limit



Ralph Poulsen (VP) / Scott Habermehl (PM)

Attachment**Two** – Transport Model

| Material | Analyte | Units | TDS | CN | As | Cd | Ni | Sb | Se |
|-------------------------|---------------------------------|--|------|-----|--------|----------|---------|---------|---------|
| | Analysis timestep | year | 10 | 10 | 10000 | 20000 | 10000 | 1500 | 1500 |
| Rock | Concentration of infiltration | mg/L | 533 | 0 | 0.05 | 0.00011 | 0.015 | 0.00076 | 0.0012 |
| | Concentration in side flow | mg/L | 533 | 0 | 0.05 | 0.00011 | 0.015 | 0.00076 | 0.0012 |
| | Initial Concentration in water | mg/L | 533 | 0 | 0.05 | 0.00011 | 0.015 | 0.00076 | 0.0012 |
| | Distribution coefficient (pH=8) | ml/g | 0 | 0 | 4.5 | 45 | 4.5 | 0.5 | 1.4 |
| Backfill | Concentration of infiltration | mg/L | 533 | 0 | 0.05 | 0.00011 | 0.015 | 0.00076 | 0.0012 |
| | Concentration in side flow | mg/L | 533 | 0 | 0.05 | 0.00011 | 0.015 | 0.00076 | 0.0012 |
| | Concentration in water | mg/L | 5691 | 0.4 | 4.482 | 0.000215 | 0.363 | 0.053 | 0.05 |
| | Distribution coefficient (pH=8) | ml/g | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Alluvium-Slope | Concentration of infiltration | mg/L | 601 | 0 | 0.053 | 0.00007 | 0.0017 | 0.00012 | 0.0015 |
| | Concentration in side flow | mg/L | 601 | 0 | 0.053 | 0.00007 | 0.0017 | 0.00012 | 0.0015 |
| | Concentration in water | mg/L | 601 | 0 | 0.053 | 0.00007 | 0.0017 | 0.00012 | 0.0015 |
| | Distribution coefficient (pH=8) | ml/g | 0 | 0 | 6 | 60 | 6 | 0.6 | 1.8 |
| Alluvium-Valley | Concentration of infiltration | mg/L | 294 | 0 | 0.03 | 0.00007 | 0.00245 | 0.00014 | 0.00108 |
| | Concentration in side flow | mg/L | 294 | 0 | 0.03 | 0.00007 | 0.00245 | 0.00014 | 0.00108 |
| | Concentration in water | mg/L | 294 | 0 | 0.03 | 0.00007 | 0.00245 | 0.00014 | 0.00108 |
| | Distribution coefficient (pH=8) | ml/g | 0 | 0 | 6 | 60 | 6 | 0.6 | 1.8 |
| River | Concentration of infiltration | mg/L | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | Concentration in side flow | mg/L | 70 | 0 | 0.0056 | 0.00004 | 0.00082 | 0.0001 | 0.001 |
| | Concentration in water | mg/L | 70 | 0 | 0.0056 | 0.00004 | 0.00082 | 0.0001 | 0.001 |
| | Distribution coefficient (pH=8) | ml/g | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| <i>Notes (italics):</i> | | 1. Selenium in river not measured; estimated based on groundwater beside river (MW98-05) | | | | | | | |

| Parameter | Type | Unit | Backfill | Rock | Alluvium-Slope | Alluvium-Valley | River |
|------------------------|---------|-------|----------|-------|----------------|-----------------|----------|
| Effective Porosity | current | % | 0.3 | 0.003 | 0.3 | 0.3 | 1 |
| | base | % | 0.3 | 0.003 | 0.3 | 0.3 | 1 |
| | lower | % | 0.2 | 0.001 | 0.25 | 0.25 | 1 |
| | upper | % | 0.5 | 0.005 | 0.4 | 0.4 | 1 |
| Hydraulic Conductivity | current | ft/yr | n/a | 0.5 | 2,000 | 40,000 | infinity |
| | base | ft/yr | n/a | 0.5 | 2,000 | 40,000 | infinity |
| | lower | ft/yr | n/a | 0.2 | 1,000 | 5000 | infinity |
| | upper | ft/yr | n/a | 0.75 | 10,000 | 72000 | infinity |
| Infiltration | current | in/yr | 0.5 | 0.5 | 2 | 2 | 0 |
| | base | in/yr | 0.5 | 0.5 | 2 | 2 | 0 |
| | lower | in/yr | 0.18 | 0.18 | 1 | 1 | 0 |
| | upper | in/yr | 0.75 | 0.75 | 4 | 4 | 0 |
| Kd(TDS) | current | mL/g | 0 | 0 | 0 | 0 | 0 |
| | base | mL/g | 0 | 0 | 0 | 0 | 0 |
| | lower | mL/g | 0 | 0 | 0 | 0 | 0 |
| | upper | mL/g | 0 | 0 | 0 | 0 | 0 |
| Kd(CN) | current | mL/g | 0 | 0 | 0 | 0 | 0 |
| | base | mL/g | 0 | 0 | 0 | 0 | 0 |
| | lower | mL/g | 0 | 0 | 0 | 0 | 0 |
| | upper | mL/g | 0 | 0 | 0 | 0 | 0 |
| Kd (As) | current | mL/g | 0 | 4.5 | 6.0 | 6.0 | 0 |
| | base | mL/g | 0 | 4.5 | 6.0 | 6.0 | 0 |
| | lower | mL/g | 0 | 3.2 | 4.3 | 4.3 | 0 |
| | upper | mL/g | 3 | 5.8 | 7.7 | 7.7 | 0 |
| Kd (Cd) | current | mL/g | 0 | 45.0 | 60.0 | 60.0 | 0 |
| | base | mL/g | 0 | 45.0 | 60.0 | 60.0 | 0 |
| | lower | mL/g | 0.0 | 8.6 | 11.4 | 11.4 | 0 |
| | upper | mL/g | 30 | 81.5 | 108.6 | 108.6 | 0 |
| Kd (Ni) | current | mL/g | 0 | 4.5 | 6.0 | 6.0 | 0 |
| | base | mL/g | 0 | 4.5 | 6.0 | 6.0 | 0 |
| | lower | mL/g | 0.0 | 2.5 | 3.4 | 3.4 | 0 |
| | upper | mL/g | 3 | 6.5 | 8.6 | 8.6 | 0 |
| Kd (Sb) | current | mL/g | 0 | 0.5 | 0.6 | 0.6 | 0 |
| | base | mL/g | 0 | 0.5 | 0.6 | 0.6 | 0 |
| | lower | mL/g | 0.0 | 0.1 | 0.2 | 0.2 | 0 |
| | upper | mL/g | 0.3 | 0.9 | 1.0 | 1.0 | 0 |
| Kd (Se) | current | mL/g | 0 | 1.4 | 1.8 | 1.8 | 0 |
| | base | mL/g | 0 | 1.4 | 1.8 | 1.8 | 0 |
| | lower | mL/g | 0.0 | 0.8 | 1.0 | 1.0 | 0 |
| | upper | mL/g | 1 | 2.0 | 2.6 | 2.6 | 0 |

| As | Unk | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
|---|----------|----------|---------|-----------|---------|---------|---------|---------|---------|---------|----------------|-----------------|------------|
| Material in cell | | Backfill | Rock | Backfill | Rock | Rock | Rock | Rock | Rock | Rock | Alluvium-Slope | Alluvium-Valley | River |
| Constants | | | | | | | | | | | | | |
| Solid unit mass | ton/cuft | 0.083 | 0.083 | 0.083 | 0.083 | 0.083 | 0.083 | 0.083 | 0.083 | 0.083 | 0.083 | 0.083 | 0.083 |
| Liquid unit mass | ton/cuft | 0.031 | 0.031 | 0.031 | 0.031 | 0.031 | 0.031 | 0.031 | 0.031 | 0.031 | 0.031 | 0.031 | 0.031 |
| Moisture content (by volume) | % | 30% | 0% | 30% | 0% | 0% | 0% | 0% | 0% | 0% | 30% | 30% | 100% |
| Solid mass per unit volume | ton/cuft | 0.058 | 0.083 | 0.058 | 0.083 | 0.083 | 0.083 | 0.083 | 0.083 | 0.083 | 0.058 | 0.058 | 0.000 |
| Water mass per unit volume | ton/cuft | 0.00936 | 0.00009 | 0.00936 | 0.00009 | 0.00009 | 0.00009 | 0.00009 | 0.00009 | 0.00009 | 0.00936 | 0.00936 | 0.03120 |
| Dimensions | | | | | | | | | | | | | |
| Height of individual cell | ft | 4000 | 4000 | 4000 | 4000 | 4000 | 4000 | 4000 | 4000 | 4000 | 100 | 100 | 100 |
| Width of analysis zone | ft | 2000 | 2000 | 2000 | 2000 | 2000 | 2000 | 2000 | 2000 | 2000 | 2000 | 2000 | 2000 |
| Thickness of cell | ft | 7.5 | 400 | 15 | 400 | 400 | 400 | 400 | 400 | 400 | 100 | 100 | 100 |
| Volume | cuft | 80000000 | 3.2E+08 | 120000000 | 3.2E+08 | 3.2E+08 | 3.2E+08 | 3.2E+08 | 3.2E+08 | 3.2E+08 | 20000000 | 20000000 | 20000000 |
| Dip of slices from the horizontal | deg | 36 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 90 | 90 | 90 |
| Area of cell normal to flow | sqft | 4000000 | 4000000 | 4000000 | 4000000 | 4000000 | 4000000 | 4000000 | 4000000 | 4000000 | 200000 | 200000 | 200000 |
| Area for infiltration to cell | sqft | 30000 | 1600000 | 60000 | 1600000 | 1600000 | 1600000 | 1600000 | 1600000 | 1600000 | 200000 | 200000 | 200000 |
| Infiltration | | | | | | | | | | | | | |
| Infiltration rate to cell surface | ft/yr | 0.015 | 0.015 | 0.015 | 0.015 | 0.015 | 0.015 | 0.015 | 0.015 | 0.015 | 0.0833333 | 0.0833333 | 0 |
| Infiltration mass rate to cell | ton/yr | 14 | 749 | 28 | 749 | 749 | 749 | 749 | 749 | 749 | 520 | 520 | 0 |
| Concentration in infiltration | mg/L | 0.0500 | 0.0500 | 0.0500 | 0.0500 | 0.0500 | 0.0500 | 0.0500 | 0.0500 | 0.0500 | 0.0530 | 0.0300 | 0.0000 |
| Chemical in infiltrating flow | ton/yr | 7.0E-07 | 3.7E-05 | 1.4E-06 | 3.7E-05 | 3.7E-05 | 3.7E-05 | 3.7E-05 | 3.7E-05 | 3.7E-05 | 2.8E-05 | 1.6E-05 | 0.0E+00 |
| Side Flow | | | | | | | | | | | | | |
| Side flow rate to cell | ton/yr | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 1.2E+05 | 2.5E+06 | 3.3E+07 |
| Concentration of side flow | mg/L | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0535 | 0.0287 | 0.0036 |
| Chemical in side flow | ton/yr | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 6.7E-03 | 7.2E-02 | 1.2E-01 |
| Liquid Phase in Cell | | | | | | | | | | | | | |
| Liquid mass in cells | ton/cell | 5.6E+05 | 3.0E+05 | 1.1E+06 | 3.0E+05 | 3.0E+05 | 3.0E+05 | 3.0E+05 | 3.0E+05 | 3.0E+05 | 1.9E+05 | 1.9E+05 | 6.2E+05 |
| Initial water concentration | mg/L | 4.48200 | 0.05000 | 4.48200 | 0.05000 | 0.05000 | 0.05000 | 0.05000 | 0.05000 | 0.05000 | 0.05300 | 0.03000 | 0.00560 |
| Solid: Liquid Relationship | | | | | | | | | | | | | |
| pH & Distribution Coefficient | ml/g | 0 | 4.500 | 0 | 4.500 | 4.500 | 4.500 | 4.500 | 4.500 | 4.500 | 6.000 | 6.000 | 0.000 |
| Rockmass pH assumed | s.u. | 9.0 | 8.5 | 9.0 | 8.5 | 8.0 | 7.5 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| pH Distribution Coefficient Factor | | 2.000 | 1.500 | 2.000 | 1.500 | 1.000 | 0.750 | 0.500 | 0.500 | 0.500 | 0.500 | 0.500 | 0.500 |
| Distribution coefficient | ml/g | 0 | 6.750 | 0 | 6.750 | 4.500 | 3.375 | 2.250 | 2.250 | 2.250 | 3.000 | 3.000 | 0.000 |
| Solid Phase in Cell | | | | | | | | | | | | | |
| Solid Mass in cells | ton/cell | 3.5E+06 | 2.7E+06 | 7.0E+06 | 2.7E+06 | 2.7E+06 | 2.7E+06 | 2.7E+06 | 2.7E+06 | 2.7E+06 | 1.2E+06 | 1.2E+06 | 0.0E+00 |
| Initial solid concentration | mg/kg | 0 | 0.338 | 0 | 0.338 | 0.225 | 0.169 | 0.113 | 0.113 | 0.113 | 0.159 | 0.080 | 0.000 |
| Initial chemical mass in solid | ton | 0.0E+00 | 8.0E+01 | 0.0E+00 | 8.0E+01 | 6.0E+01 | 4.5E+01 | 3.0E+01 | 3.0E+01 | 3.0E+01 | 1.9E-01 | 1.0E-01 | 0.0E+00 |
| INITIAL CONCENTRATION | | | | | | | | | | | | | |
| Note that this is computed by evaluating the concentration that would occur by mixing infiltration, side, and cell above inputs at ss | | | | | | | | | | | | | |
| Initial flows | | | | | | | | | | | | | |
| Infiltration to cell | ton/yr | 1.4E+01 | 7.5E+02 | 2.8E+01 | 7.5E+02 | 7.5E+02 | 7.5E+02 | 7.5E+02 | 7.5E+02 | 7.5E+02 | 5.2E+02 | 5.2E+02 | 0 |
| Flow from cell above | ton/yr | 1.6E+04 | 1.6E+04 | 1.6E+04 | 1.6E+04 | 1.7E+04 | 1.8E+04 | 1.9E+04 | 1.9E+04 | 1.9E+04 | 2.0E+04 | 2.1E+04 | 1.5E+05 |
| Side flow to cell | ton/yr | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 1.2E+05 | 2.5E+06 | 32,754,803 |
| Total flow to cell | ton/yr | 1.6E+04 | 1.6E+04 | 1.6E+04 | 1.7E+04 | 1.8E+04 | 1.9E+04 | 1.9E+04 | 1.9E+04 | 2.0E+04 | 2.1E+04 | 1.5E+05 | 35,397,527 |
| Flow out of cell (all downgradient) | ton/yr | 1.6E+04 | 1.6E+04 | 1.6E+04 | 1.7E+04 | 1.8E+04 | 1.9E+04 | 1.9E+04 | 1.9E+04 | 2.0E+04 | 2.1E+04 | 1.5E+05 | 35,397,527 |
| Side Flow Concentration (computed to avoid an initial jump in concentration at the alluvium and the stream) | | | | | | | | | | | | | |
| Concentration of Infiltration | mg/L | 0.050 | 0.050 | 0.050 | 0.050 | 0.050 | 0.050 | 0.050 | 0.050 | 0.050 | 0.053 | 0.030 | 0.0000 |
| Concentration from cell above | mg/L | 0.050 | 0.050 | 0.050 | 0.050 | 0.050 | 0.050 | 0.050 | 0.050 | 0.050 | 0.050 | 0.053 | 0.030 |
| Final concentration in cell | mg/L | 0.050 | 0.050 | 0.050 | 0.050 | 0.050 | 0.050 | 0.050 | 0.050 | 0.050 | 0.053 | 0.030 | 0.0056 |
| Computed side flow conc in | mg/L | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.054 | 0.029 | 0.004 |

| Time year | Initial solids ton | Initial chemical in solid ton | Initial water ton | Incoming water from cell above ton | Incoming chemical from cell above ton | Incoming water from side ton | Incoming chemical from side ton | Incoming water from bottom ton | Incoming chemical from bottom ton | Total water in cell ton | Total chemical in cell ton | Mass on solids ton | Mass in leach ton | Concentration in solids mg/kg | Concentration in liquid mg/L | Outgoing liquid to next cell ton | Outgoing chemical to next cell ton | Final solid in cell tons | Final chemical on solid tons | Final chemical in liquid tons | Final chemical in cell tons | | | |
|-----------|--------------------|-------------------------------|-------------------|------------------------------------|---------------------------------------|------------------------------|---------------------------------|--------------------------------|-----------------------------------|-------------------------|----------------------------|--------------------|-------------------|-------------------------------|------------------------------|----------------------------------|------------------------------------|--------------------------|------------------------------|-------------------------------|-----------------------------|----------|----------|----------|
| 0 | | | | | | | | | | | | | | | | | | | | | | | | |
| 10000 | 2.66E+06 | 89.69847 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 7486000 | 0.3744 | 163277920 | 100.3749 | 91.97096 | 8.404045 | 0.34636 | 0.051267 | 163626400 | 8.38889 | 2.66E+06 | 299520 | 89.69847 | 0.014978 | 15614040 |
| 20000 | 2.66E+06 | 91.97096 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 7486000 | 0.3744 | 163277920 | 100.1755 | 91.78901 | 8.397436 | 0.345366 | 0.051165 | 163626400 | 8.372111 | 2.66E+06 | 299520 | 91.78901 | 0.014978 | 15614040 |
| 30000 | 2.66E+06 | 91.78901 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 7486000 | 0.3744 | 163277920 | 99.98566 | 91.61439 | 8.371472 | 0.344709 | 0.051068 | 163626400 | 8.356777 | 2.66E+06 | 299520 | 91.61439 | 0.014978 | 15614040 |
| 40000 | 2.66E+06 | 91.45426 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 7486000 | 0.3744 | 163277920 | 99.80111 | 91.45426 | 8.356777 | 0.344007 | 0.050979 | 163626400 | 8.341572 | 2.66E+06 | 299520 | 91.45426 | 0.014978 | 15614040 |
| 50000 | 2.66E+06 | 91.45426 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 7486000 | 0.3744 | 163277920 | 99.62596 | 91.30763 | 8.343432 | 0.343254 | 0.050897 | 163626400 | 8.326917 | 2.66E+06 | 299520 | 91.30763 | 0.014978 | 15614040 |
| 60000 | 2.66E+06 | 91.30763 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 7486000 | 0.3744 | 163277920 | 99.46049 | 91.17934 | 8.331143 | 0.342498 | 0.050822 | 163626400 | 8.312491 | 2.66E+06 | 299520 | 91.17934 | 0.014978 | 15614040 |
| 70000 | 2.66E+06 | 91.17934 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 7486000 | 0.3744 | 163277920 | 99.30499 | 91.04988 | 8.319822 | 0.341742 | 0.050747 | 163626400 | 8.298134 | 2.66E+06 | 299520 | 91.04988 | 0.014978 | 15614040 |
| 80000 | 2.66E+06 | 91.04988 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 7486000 | 0.3744 | 163277920 | 99.15442 | 90.93666 | 8.309562 | 0.341016 | 0.050668 | 163626400 | 8.284039 | 2.66E+06 | 299520 | 90.93666 | 0.014978 | 15614040 |
| 90000 | 2.66E+06 | 90.93666 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 7486000 | 0.3744 | 163277920 | 99.13547 | 90.83336 | 8.302104 | 0.340317 | 0.050593 | 163626400 | 8.269438 | 2.66E+06 | 299520 | 90.83336 | 0.014978 | 15614040 |
| 100000 | 2.66E+06 | 90.83336 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 7486000 | 0.3744 | 163277920 | 99.03696 | 90.73651 | 8.291437 | 0.339641 | 0.050521 | 163626400 | 8.255277 | 2.66E+06 | 299520 | 90.73651 | 0.014978 | 15614040 |
| 110000 | 2.66E+06 | 90.73651 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 7486000 | 0.3744 | 163277920 | 98.95028 | 90.65159 | 8.283454 | 0.338986 | 0.050452 | 163626400 | 8.241519 | 2.66E+06 | 299520 | 90.65159 | 0.014978 | 15614040 |
| 120000 | 2.66E+06 | 90.65159 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 7486000 | 0.3744 | 163277920 | 98.88141 | 90.57193 | 8.276721 | 0.338357 | 0.050387 | 163626400 | 8.228193 | 2.66E+06 | 299520 | 90.57193 | 0.014978 | 15614040 |
| 130000 | 2.66E+06 | 90.57193 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 7486000 | 0.3744 | 163277920 | 98.82647 | 90.49827 | 8.269844 | 0.337742 | 0.050326 | 163626400 | 8.215246 | 2.66E+06 | 299520 | 90.49827 | 0.014978 | 15614040 |
| 140000 | 2.66E+06 | 90.49827 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 7486000 | 0.3744 | 163277920 | 98.78454 | 90.43222 | 8.263311 | 0.337146 | 0.050268 | 163626400 | 8.203133 | 2.66E+06 | 299520 | 90.43222 | 0.014978 | 15614040 |
| 150000 | 2.66E+06 | 90.43222 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 7486000 | 0.3744 | 163277920 | 98.75464 | 90.37071 | 8.257129 | 0.336567 | 0.050213 | 163626400 | 8.191724 | 2.66E+06 | 299520 | 90.37071 | 0.014978 | 15614040 |
| 160000 | 2.66E+06 | 90.37071 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 7486000 | 0.3744 | 163277920 | 98.73672 | 90.31453 | 8.251294 | 0.336003 | 0.050161 | 163626400 | 8.181043 | 2.66E+06 | 299520 | 90.31453 | 0.014978 | 15614040 |
| 170000 | 2.66E+06 | 90.31453 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 7486000 | 0.3744 | 163277920 | 98.72903 | 90.26303 | 8.245789 | 0.335454 | 0.050112 | 163626400 | 8.171106 | 2.66E+06 | 299520 | 90.26303 | 0.014978 | 15614040 |
| 180000 | 2.66E+06 | 90.26303 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 7486000 | 0.3744 | 163277920 | 98.73159 | 90.21585 | 8.240632 | 0.334921 | 0.050066 | 163626400 | 8.161921 | 2.66E+06 | 299520 | 90.21585 | 0.014978 | 15614040 |
| 190000 | 2.66E+06 | 90.21585 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 7486000 | 0.3744 | 163277920 | 98.73543 | 90.17287 | 8.235766 | 0.334404 | 0.050023 | 163626400 | 8.153497 | 2.66E+06 | 299520 | 90.17287 | 0.014978 | 15614040 |
| 200000 | 2.66E+06 | 90.17287 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 7486000 | 0.3744 | 163277920 | 98.74087 | 90.13361 | 8.231216 | 0.333904 | 0.050000 | 163626400 | 8.145824 | 2.66E+06 | 299520 | 90.13361 | 0.014978 | 15614040 |
| 210000 | 2.66E+06 | 90.13361 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 7486000 | 0.3744 | 163277920 | 98.74844 | 90.09866 | 8.227268 | 0.333422 | 0.050000 | 163626400 | 8.138904 | 2.66E+06 | 299520 | 90.09866 | 0.014978 | 15614040 |
| 220000 | 2.66E+06 | 90.09866 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 7486000 | 0.3744 | 163277920 | 98.75872 | 90.06833 | 8.223746 | 0.332957 | 0.050000 | 163626400 | 8.132744 | 2.66E+06 | 299520 | 90.06833 | 0.014978 | 15614040 |
| 230000 | 2.66E+06 | 90.06833 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 7486000 | 0.3744 | 163277920 | 98.77026 | 90.04263 | 8.220698 | 0.332508 | 0.050000 | 163626400 | 8.127344 | 2.66E+06 | 299520 | 90.04263 | 0.014978 | 15614040 |
| 240000 | 2.66E+06 | 90.04263 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 7486000 | 0.3744 | 163277920 | 98.78354 | 90.02044 | 8.218044 | 0.332074 | 0.050000 | 163626400 | 8.122704 | 2.66E+06 | 299520 | 90.02044 | 0.014978 | 15614040 |
| 250000 | 2.66E+06 | 90.02044 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 7486000 | 0.3744 | 163277920 | 98.79817 | 90.00193 | 8.215719 | 0.331654 | 0.050000 | 163626400 | 8.118824 | 2.66E+06 | 299520 | 90.00193 | 0.014978 | 15614040 |
| 260000 | 2.66E+06 | 90.00193 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 7486000 | 0.3744 | 163277920 | 98.81467 | 89.98693 | 8.213719 | 0.331254 | 0.050000 | 163626400 | 8.115604 | 2.66E+06 | 299520 | 89.98693 | 0.014978 | 15614040 |
| 270000 | 2.66E+06 | 89.98693 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 7486000 | 0.3744 | 163277920 | 98.83257 | 89.97446 | 8.211952 | 0.330872 | 0.050000 | 163626400 | 8.112944 | 2.66E+06 | 299520 | 89.97446 | 0.014978 | 15614040 |
| 280000 | 2.66E+06 | 89.97446 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 7486000 | 0.3744 | 163277920 | 98.85147 | 89.96431 | 8.210416 | 0.330508 | 0.050000 | 163626400 | 8.110844 | 2.66E+06 | 299520 | 89.96431 | 0.014978 | 15614040 |
| 290000 | 2.66E+06 | 89.96431 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 7486000 | 0.3744 | 163277920 | 98.87187 | 89.95623 | 8.209089 | 0.330161 | 0.050000 | 163626400 | 8.109204 | 2.66E+06 | 299520 | 89.95623 | 0.014978 | 15614040 |
| 300000 | 2.66E+06 | 89.95623 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 7486000 | 0.3744 | 163277920 | 98.89427 | 89.95014 | 8.207952 | 0.329829 | 0.050000 | 163626400 | 8.108024 | 2.66E+06 | 299520 | 89.95014 | 0.014978 | 15614040 |
| 310000 | 2.66E+06 | 89.95014 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 7486000 | 0.3744 | 163277920 | 98.91867 | 89.94586 | 8.206984 | 0.329511 | 0.050000 | 163626400 | 8.107244 | 2.66E+06 | 299520 | 89.94586 | 0.014978 | 15614040 |
| 320000 | 2.66E+06 | 89.94586 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 7486000 | 0.3744 | 163277920 | 98.94567 | 89.94346 | 8.206166 | 0.329207 | 0.050000 | 163626400 | 8.106864 | 2.66E+06 | 299520 | 89.94346 | 0.014978 | 15614040 |
| 330000 | 2.66E+06 | 89.94346 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 7486000 | 0.3744 | 163277920 | 98.97467 | 89.94286 | 8.205466 | 0.328917 | 0.050000 | 163626400 | 8.106884 | 2.66E+06 | 299520 | 89.94286 | 0.014978 | 15614040 |
| 340000 | 2.66E+06 | 89.94286 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 7486000 | 0.3744 | 163277920 | 98.99627 | 89.94386 | 8.204886 | 0.328641 | 0.050000 | 163626400 | 8.107244 | 2.66E+06 | 299520 | 89.94386 | 0.014978 | 15614040 |
| 350000 | 2.66E+06 | 89.94386 | 299520 | 0.014978 | 15614040 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | | | | | | | | | | | | | | | |

| Time year | Initial solids ton | Initial chemical in add ton | Initial water ton | Initial chemical in water ton | Incoming water from cell above ton | Incoming chemical from cell above ton | Incoming water from side ton | Incoming chemical from side ton | Incoming water from infiltration ton | Incoming chemical from infiltration ton | Total water in cell ton | Total chemical in cell ton | Mass on solids ton | Mass in liquids ton | Concentration in solids mg/kg | Concentration in liquids mg/L | Outgoing liquid to next cell tons | Outgoing chemical to next cell tons | Final solid in cell tons | Final chemical on solid tons | Final chemical in liquid tons | Final chemical in cell tons | |
|-----------|--------------------|-----------------------------|-------------------|-------------------------------|------------------------------------|---------------------------------------|------------------------------|---------------------------------|--------------------------------------|---|-------------------------|----------------------------|--------------------|---------------------|-------------------------------|-------------------------------|-----------------------------------|-------------------------------------|--------------------------|------------------------------|-------------------------------|-----------------------------|----------|
| 0 | | | | | | | 0 | | 0 | 748900 | 0.3744 | | 4.6 | | 0.226 | 0.05 | | | | | | | |
| 10000 | 2.65E+08 | 99.78994 | 299520 | 0.014978 | 0.3975 | 0.05 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.014978 | 59.81392 | 59.81392 |
| 20000 | 2.65E+08 | 99.84267 | 299520 | 0.014989 | 0 | 0.0767 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.014989 | 59.86361 | 59.86361 |
| 30000 | 2.65E+08 | 99.85337 | 299520 | 0.014999 | 0 | 0.100028 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.014999 | 59.91330 | 59.91330 |
| 40000 | 2.65E+08 | 99.87462 | 299520 | 0.015008 | 0 | 0.12112 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015008 | 59.96300 | 59.96300 |
| 50000 | 2.65E+08 | 99.91017 | 299520 | 0.015017 | 0 | 0.14116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015017 | 60.01270 | 60.01270 |
| 60000 | 2.65E+08 | 99.95022 | 299520 | 0.015026 | 0 | 0.16116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015026 | 60.06240 | 60.06240 |
| 70000 | 2.65E+08 | 99.99486 | 299520 | 0.015035 | 0 | 0.18116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015035 | 60.11210 | 60.11210 |
| 80000 | 2.65E+08 | 100.04416 | 299520 | 0.015044 | 0 | 0.20116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015044 | 60.16180 | 60.16180 |
| 90000 | 2.65E+08 | 100.09746 | 299520 | 0.015053 | 0 | 0.22116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015053 | 60.21150 | 60.21150 |
| 100000 | 2.65E+08 | 100.15476 | 299520 | 0.015062 | 0 | 0.24116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015062 | 60.26120 | 60.26120 |
| 110000 | 2.65E+08 | 100.21606 | 299520 | 0.015071 | 0 | 0.26116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015071 | 60.31090 | 60.31090 |
| 120000 | 2.65E+08 | 100.28136 | 299520 | 0.015080 | 0 | 0.28116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015080 | 60.36060 | 60.36060 |
| 130000 | 2.65E+08 | 100.35066 | 299520 | 0.015089 | 0 | 0.30116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015089 | 60.41030 | 60.41030 |
| 140000 | 2.65E+08 | 100.42396 | 299520 | 0.015098 | 0 | 0.32116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015098 | 60.46000 | 60.46000 |
| 150000 | 2.65E+08 | 100.50126 | 299520 | 0.015107 | 0 | 0.34116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015107 | 60.50970 | 60.50970 |
| 160000 | 2.65E+08 | 100.58256 | 299520 | 0.015116 | 0 | 0.36116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015116 | 60.55940 | 60.55940 |
| 170000 | 2.65E+08 | 100.66786 | 299520 | 0.015125 | 0 | 0.38116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015125 | 60.60910 | 60.60910 |
| 180000 | 2.65E+08 | 100.75716 | 299520 | 0.015134 | 0 | 0.40116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015134 | 60.65880 | 60.65880 |
| 190000 | 2.65E+08 | 100.85046 | 299520 | 0.015143 | 0 | 0.42116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015143 | 60.70850 | 60.70850 |
| 200000 | 2.65E+08 | 100.94776 | 299520 | 0.015152 | 0 | 0.44116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015152 | 60.75820 | 60.75820 |
| 210000 | 2.65E+08 | 101.04906 | 299520 | 0.015161 | 0 | 0.46116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015161 | 60.80790 | 60.80790 |
| 220000 | 2.65E+08 | 101.15436 | 299520 | 0.015170 | 0 | 0.48116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015170 | 60.85760 | 60.85760 |
| 230000 | 2.65E+08 | 101.26366 | 299520 | 0.015179 | 0 | 0.50116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015179 | 60.90730 | 60.90730 |
| 240000 | 2.65E+08 | 101.37696 | 299520 | 0.015188 | 0 | 0.52116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015188 | 60.95700 | 60.95700 |
| 250000 | 2.65E+08 | 101.49426 | 299520 | 0.015197 | 0 | 0.54116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015197 | 61.00670 | 61.00670 |
| 260000 | 2.65E+08 | 101.61556 | 299520 | 0.015206 | 0 | 0.56116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015206 | 61.05640 | 61.05640 |
| 270000 | 2.65E+08 | 101.74086 | 299520 | 0.015215 | 0 | 0.58116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015215 | 61.10610 | 61.10610 |
| 280000 | 2.65E+08 | 101.87016 | 299520 | 0.015224 | 0 | 0.60116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015224 | 61.15580 | 61.15580 |
| 290000 | 2.65E+08 | 102.00346 | 299520 | 0.015233 | 0 | 0.62116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015233 | 61.20550 | 61.20550 |
| 300000 | 2.65E+08 | 102.14176 | 299520 | 0.015242 | 0 | 0.64116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015242 | 61.25520 | 61.25520 |
| 310000 | 2.65E+08 | 102.28506 | 299520 | 0.015251 | 0 | 0.66116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015251 | 61.30490 | 61.30490 |
| 320000 | 2.65E+08 | 102.43336 | 299520 | 0.015260 | 0 | 0.68116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015260 | 61.35460 | 61.35460 |
| 330000 | 2.65E+08 | 102.58666 | 299520 | 0.015269 | 0 | 0.70116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015269 | 61.40430 | 61.40430 |
| 340000 | 2.65E+08 | 102.74496 | 299520 | 0.015278 | 0 | 0.72116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015278 | 61.45400 | 61.45400 |
| 350000 | 2.65E+08 | 102.90826 | 299520 | 0.015287 | 0 | 0.74116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015287 | 61.50370 | 61.50370 |
| 360000 | 2.65E+08 | 103.07656 | 299520 | 0.015296 | 0 | 0.76116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015296 | 61.55340 | 61.55340 |
| 370000 | 2.65E+08 | 103.24986 | 299520 | 0.015305 | 0 | 0.78116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015305 | 61.60310 | 61.60310 |
| 380000 | 2.65E+08 | 103.42816 | 299520 | 0.015314 | 0 | 0.80116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015314 | 61.65280 | 61.65280 |
| 390000 | 2.65E+08 | 103.61146 | 299520 | 0.015323 | 0 | 0.82116 | 0 | | 0 | 748900 | 0.3744 | 778750 | 80.23832 | 89.84852 | 0.266688 | 0.226187 | 748900.3 | 0.374711 | 2.65E+08 | 299520 | 0.015323 | 61.70250 | 61.70250 |
| 400000 | 2.65E+08 | 103.79976 | 299520 | 0.015332 | 0 | 0.84116 | 0 | | 0 | | | | | | | | | | | | | | |

| Time year | Initial solids ton | Initial chemical in solid ton | Initial water ton | Initial chemical in water ton | Incoming water from cell above ton | Incoming chemical from cell above ton | Incoming water from cell above ton | Incoming chemical from cell above ton | Incoming water from cell above ton | Incoming chemical from cell above ton | Total water in cell ton | Total chemical in cell ton | Mass on solids ton | Mass in liquids ton | Concentration in solids mg/kg | Concentration in liquids mg/l | Outgoing liquid to next cell ton | Outgoing chemical to next cell ton | Final solid in cell ton | Final liquid in cell ton | Final chemical in solid in cell ton | Final chemical in liquid in cell ton | Final chemical in cell ton |
|-----------|--------------------|-------------------------------|-------------------|-------------------------------|------------------------------------|---------------------------------------|------------------------------------|---------------------------------------|------------------------------------|---------------------------------------|-------------------------|----------------------------|--------------------|---------------------|-------------------------------|-------------------------------|----------------------------------|------------------------------------|-------------------------|--------------------------|-------------------------------------|--------------------------------------|----------------------------|
| 0 | | | | | | | | | | | | | | | | | | | | | | | |
| 10000 | 2.66E+08 | 44.84921 | 299520 | 0.014978 | 7480000 | 0.374711 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 45.61329 | 44.84921 | 0.763781 | 0.188751 | 0.06 | 14978000 | 5.748006 | 2.66E+08 | 299520 | 44.84921 | 0.014978 | 44.86418 |
| 20000 | 2.66E+08 | 44.84921 | 299520 | 0.014978 | 7480000 | 0.374711 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 45.61329 | 44.84921 | 0.763781 | 0.188751 | 0.06 | 14978000 | 5.748006 | 2.66E+08 | 299520 | 44.84921 | 0.014978 | 44.86418 |
| 30000 | 2.66E+08 | 345.2434 | 299520 | 0.116619 | 7480000 | 626.77 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 976.6046 | 345.2434 | 1.633544 | 3.606891 | 1.065320 | 14978000 | 16.01426 | 2.66E+08 | 299520 | 345.2434 | 0.116619 | 349.3601 |
| 40000 | 2.66E+08 | 959.17 | 299520 | 0.320285 | 7480000 | 939.9401 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 1898.705 | 959.17 | 4.281958 | 2.002417 | 1.497800 | 14978000 | 31.16277 | 2.66E+08 | 299520 | 959.17 | 0.320285 | 959.4902 |
| 50000 | 2.66E+08 | 1697.895 | 299520 | 0.623725 | 7480000 | 1291.962 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 3020.869 | 1697.895 | 7.522570 | 3.114893 | 2.121016 | 14978000 | 51.23914 | 2.66E+08 | 299520 | 1697.895 | 0.623725 | 1699.518 |
| 60000 | 2.66E+08 | 3266.597 | 299520 | 1.024663 | 7480000 | 1952.113 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 4632.14 | 3266.597 | 17.56382 | 4.173708 | 3.077866 | 14978000 | 76.04284 | 2.66E+08 | 299520 | 3266.597 | 1.024663 | 3269.622 |
| 70000 | 2.66E+08 | 4834.576 | 299520 | 1.528589 | 7480000 | 2870.364 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 6426.968 | 4834.576 | 23.77666 | 5.044986 | 3.819597 | 14978000 | 105.9259 | 2.66E+08 | 299520 | 4834.576 | 1.528589 | 4836.105 |
| 80000 | 2.66E+08 | 6319.2 | 299520 | 2.110117 | 7480000 | 3915.728 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 8426.482 | 6319.2 | 31.48085 | 6.319597 | 4.193111 | 14978000 | 139.5141 | 2.66E+08 | 299520 | 6319.2 | 2.110117 | 6321.36 |
| 90000 | 2.66E+08 | 8354.159 | 299520 | 2.793278 | 7480000 | 5201.157 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 10943.48 | 8354.159 | 40.56596 | 8.010546 | 5.193111 | 14978000 | 177.9612 | 2.66E+08 | 299520 | 8354.159 | 2.793278 | 8356.948 |
| 100000 | 2.66E+08 | 10629.95 | 299520 | 3.558228 | 7480000 | 6763.681 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 13446.58 | 10629.95 | 52.26181 | 10.474704 | 6.73506 | 14978000 | 220.7442 | 2.66E+08 | 299520 | 10629.95 | 3.558228 | 10632.54 |
| 110000 | 2.66E+08 | 13221.42 | 299520 | 4.414884 | 7480000 | 8944.344 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 16310.56 | 13221.42 | 63.34261 | 12.87929 | 8.07929 | 14978000 | 273.1053 | 2.66E+08 | 299520 | 13221.42 | 4.414884 | 13223.84 |
| 120000 | 2.66E+08 | 16037.34 | 299520 | 5.352526 | 7480000 | 11633.127 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 19426.3 | 16037.34 | 75.18692 | 15.2547 | 9.52547 | 14978000 | 318.9056 | 2.66E+08 | 299520 | 16037.34 | 5.352526 | 16039.68 |
| 130000 | 2.66E+08 | 19101.01 | 299520 | 6.379189 | 7480000 | 15680.06 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 22787.61 | 19101.01 | 86.15752 | 17.83692 | 10.93692 | 14978000 | 374.0834 | 2.66E+08 | 299520 | 19101.01 | 6.379189 | 19103.38 |
| 140000 | 2.66E+08 | 22406.24 | 299520 | 7.481868 | 7480000 | 20475.127 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 26395.22 | 22406.24 | 96.8796 | 19.52669 | 12.2731 | 14978000 | 433.2156 | 2.66E+08 | 299520 | 22406.24 | 7.481868 | 22408.62 |
| 150000 | 2.66E+08 | 26847.34 | 299520 | 8.664309 | 7480000 | 26283.39 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 30274.75 | 26847.34 | 106.5046 | 21.13174 | 13.13174 | 14978000 | 496.1033 | 2.66E+08 | 299520 | 26847.34 | 8.664309 | 26849.97 |
| 160000 | 2.66E+08 | 31918.65 | 299520 | 9.923619 | 7480000 | 33297.06 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 34426.73 | 31918.65 | 115.1647 | 22.06669 | 13.66669 | 14978000 | 562.9989 | 2.66E+08 | 299520 | 31918.65 | 9.923619 | 31920.83 |
| 170000 | 2.66E+08 | 37714.57 | 299520 | 11.25794 | 7480000 | 40433.361 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 38975.8 | 37714.57 | 123.6457 | 23.17146 | 14.25716 | 14978000 | 632.2716 | 2.66E+08 | 299520 | 37714.57 | 11.25794 | 37716.67 |
| 180000 | 2.66E+08 | 44299.69 | 299520 | 12.66643 | 7480000 | 48717.194 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 43930.63 | 44299.69 | 132.3602 | 23.9786 | 14.72309 | 14978000 | 707.2159 | 2.66E+08 | 299520 | 44299.69 | 12.66643 | 44299.89 |
| 190000 | 2.66E+08 | 51769.53 | 299520 | 14.14432 | 7480000 | 58233.207 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 49386.93 | 51769.53 | 141.0196 | 24.83026 | 15.23026 | 14978000 | 784.6415 | 2.66E+08 | 299520 | 51769.53 | 14.14432 | 51770.67 |
| 200000 | 2.66E+08 | 59959.85 | 299520 | 15.69384 | 7480000 | 69170.44 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 55316.86 | 59959.85 | 150.0111 | 25.73594 | 15.73594 | 14978000 | 865.4622 | 2.66E+08 | 299520 | 59959.85 | 15.69384 | 59960.97 |
| 210000 | 2.66E+08 | 68916.86 | 299520 | 17.33374 | 7480000 | 81669.805 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 61764.28 | 68916.86 | 159.2699 | 26.64065 | 16.24065 | 14978000 | 949.6311 | 2.66E+08 | 299520 | 68916.86 | 17.33374 | 68918.97 |
| 220000 | 2.66E+08 | 78697.57 | 299520 | 19.05196 | 7480000 | 95710.614 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 68676.65 | 78697.57 | 168.8195 | 27.54537 | 16.74537 | 14978000 | 1038.651 | 2.66E+08 | 299520 | 78697.57 | 19.05196 | 78699.67 |
| 230000 | 2.66E+08 | 89327.96 | 299520 | 20.85302 | 7480000 | 111409.577 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 76082.04 | 89327.96 | 178.9264 | 28.44008 | 17.24008 | 14978000 | 1132.456 | 2.66E+08 | 299520 | 89327.96 | 20.85302 | 89329.77 |
| 240000 | 2.66E+08 | 100926.64 | 299520 | 22.73069 | 7480000 | 128635.604 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 84037.57 | 100926.64 | 189.3359 | 29.33444 | 17.73444 | 14978000 | 1231.033 | 2.66E+08 | 299520 | 100926.64 | 22.73069 | 100928.36 |
| 250000 | 2.66E+08 | 113523.93 | 299520 | 24.68477 | 7480000 | 148027.003 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 92583.03 | 113523.93 | 200.3431 | 30.22915 | 18.22915 | 14978000 | 1335.579 | 2.66E+08 | 299520 | 113523.93 | 24.68477 | 113525.62 |
| 260000 | 2.66E+08 | 127191.01 | 299520 | 26.71548 | 7480000 | 169319.095 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 101763.57 | 127191.01 | 211.8359 | 31.12344 | 18.72344 | 14978000 | 1445.984 | 2.66E+08 | 299520 | 127191.01 | 26.71548 | 127192.70 |
| 270000 | 2.66E+08 | 141931.63 | 299520 | 28.82388 | 7480000 | 192811.181 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 111443.03 | 141931.63 | 223.6473 | 32.01815 | 19.21815 | 14978000 | 1562.059 | 2.66E+08 | 299520 | 141931.63 | 28.82388 | 141933.31 |
| 280000 | 2.66E+08 | 157877.3 | 299520 | 30.99966 | 7480000 | 218074.674 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 121633.54 | 157877.3 | 236.0068 | 32.91244 | 19.71244 | 14978000 | 1684.815 | 2.66E+08 | 299520 | 157877.3 | 30.99966 | 157879.00 |
| 290000 | 2.66E+08 | 175039.5 | 299520 | 33.24602 | 7480000 | 245627.296 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 132344.03 | 175039.5 | 248.9259 | 33.80673 | 20.20673 | 14978000 | 1814.241 | 2.66E+08 | 299520 | 175039.5 | 33.24602 | 175041.28 |
| 300000 | 2.66E+08 | 193446.5 | 299520 | 35.56352 | 7480000 | 275433.326 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 143685.52 | 193446.5 | 262.3116 | 34.69102 | 20.69102 | 14978000 | 1947.547 | 2.66E+08 | 299520 | 193446.5 | 35.56352 | 193448.53 |
| 310000 | 2.66E+08 | 213136.5 | 299520 | 37.95712 | 7480000 | 307617.704 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 155368.01 | 213136.5 | 276.1418 | 35.57531 | 21.17531 | 14978000 | 2084.826 | 2.66E+08 | 299520 | 213136.5 | 37.95712 | 213138.74 |
| 320000 | 2.66E+08 | 234111.5 | 299520 | 40.42921 | 7480000 | 342092.492 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 167430.5 | 234111.5 | 290.3297 | 36.45960 | 21.65960 | 14978000 | 2227.081 | 2.66E+08 | 299520 | 234111.5 | 40.42921 | 234113.71 |
| 330000 | 2.66E+08 | 256296.6 | 299520 | 42.98484 | 7480000 | 379889.807 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 180003.99 | 256296.6 | 304.8697 | 37.34389 | 22.13389 | 14978000 | 2374.319 | 2.66E+08 | 299520 | 256296.6 | 42.98484 | 256298.78 |
| 340000 | 2.66E+08 | 280684.8 | 299520 | 45.61925 | 7480000 | 420918.613 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 193007.48 | 280684.8 | 319.8195 | 38.22818 | 22.60818 | 14978000 | 2525.538 | 2.66E+08 | 299520 | 280684.8 | 45.61925 | 280686.77 |
| 350000 | 2.66E+08 | 307379.8 | 299520 | 48.32747 | 7480000 | 475413.814 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 206451.97 | 307379.8 | 335.2293 | 39.10247 | 23.08247 | 14978000 | 2680.747 | 2.66E+08 | 299520 | 307379.8 | 48.32747 | 307381.76 |
| 360000 | 2.66E+08 | 336437.6 | 299520 | 51.11484 | 7480000 | 534413.814 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 220456.46 | 336437.6 | 351.1391 | 39.96676 | 23.55676 | 14978000 | 2839.956 | 2.66E+08 | 299520 | 336437.6 | 51.11484 | 336439.55 |
| 370000 | 2.66E+08 | 367917.6 | 299520 | 53.98529 | 7480000 | 598018.16 | 0 | 0 | 7480000 | 0.3744 | 15275520 | 235000.95 | 367917.6 | 367.5489 | 40.82105 | 24.03105 | 14978000 | 2993.165 | 2.66E+08 | 299520 | 367917.6 | 53.98529 | 367919.54 |
| 380000 | | | | | | | | | | | | | | | | | | | | | | | |

| Time year | Initial acide ton | Initial chemical in acid ton | Initial water ton | Initial chemical in water ton | Incoming water from cell above ton | Incoming chemical from cell above ton | Incoming water from side ton | Incoming chemical from side ton | Incoming water from infiltration ton | Incoming chemical from infiltration ton | Total water in cell ton | Total chemical in cell ton | Mass on solids ton | Mass in leach ton | Concentration in solids mg/kg | Concentration in liquids mg/L | Outgoing liquid to next cell tons | Outgoing chemical to next cell tons | Final solid in cell tons | Final head in cell tons | Final chemical on solid tons | Final chemical in liquid tons | Final chemical in cell tons | Final chemical in cell tons | |
|-----------|-------------------|------------------------------|-------------------|-------------------------------|------------------------------------|---------------------------------------|------------------------------|---------------------------------|--------------------------------------|---|-------------------------|----------------------------|--------------------|-------------------|-------------------------------|-------------------------------|-----------------------------------|-------------------------------------|--------------------------|-------------------------|------------------------------|-------------------------------|-----------------------------|-----------------------------|----------|
| 10000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 0 | 0 | 0.1125 | 0.05 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 20000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 31.03785 | 29.89847 | 1.136176 | 0.1125 | 0.05 | 2246400 | 1.1232 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 30000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 36.11989 | 34.79526 | 1.274543 | 0.13034 | 0.05 | 2246400 | 1.307115 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 40000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 41.20184 | 49.32374 | 1.577588 | 0.148686 | 0.05 | 2246400 | 1.440230 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 50000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 46.28379 | 57.45569 | 1.881083 | 0.167001 | 0.05 | 2246400 | 1.573345 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 60000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 51.26574 | 65.58759 | 2.184578 | 0.185316 | 0.05 | 2246400 | 1.706460 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 70000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 56.24769 | 73.71949 | 2.488073 | 0.203631 | 0.05 | 2246400 | 1.839575 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 80000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 61.22964 | 81.85139 | 2.791568 | 0.221946 | 0.05 | 2246400 | 1.972690 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 90000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 66.21159 | 89.98329 | 3.095063 | 0.240261 | 0.05 | 2246400 | 2.105805 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 100000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 71.19354 | 98.11519 | 3.398558 | 0.258576 | 0.05 | 2246400 | 2.238920 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 110000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 76.17549 | 106.24709 | 3.702053 | 0.276891 | 0.05 | 2246400 | 2.372035 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 120000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 81.15744 | 114.37899 | 4.005548 | 0.295206 | 0.05 | 2246400 | 2.505150 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 130000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 86.13939 | 122.51089 | 4.309043 | 0.313521 | 0.05 | 2246400 | 2.638265 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 140000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 91.12134 | 130.64279 | 4.612538 | 0.331836 | 0.05 | 2246400 | 2.771380 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 150000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 96.10329 | 138.77469 | 4.916033 | 0.350151 | 0.05 | 2246400 | 2.904495 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 160000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 101.08524 | 146.90659 | 5.219528 | 0.368466 | 0.05 | 2246400 | 3.037610 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 170000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 106.06719 | 155.03849 | 5.523023 | 0.386781 | 0.05 | 2246400 | 3.170725 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 180000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 111.04914 | 163.17039 | 5.826518 | 0.405096 | 0.05 | 2246400 | 3.303840 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 190000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 116.03109 | 171.30229 | 6.130013 | 0.423411 | 0.05 | 2246400 | 3.436955 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 200000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 121.01304 | 179.43419 | 6.433508 | 0.441726 | 0.05 | 2246400 | 3.570070 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 210000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 126.00000 | 187.56609 | 6.737003 | 0.460041 | 0.05 | 2246400 | 3.703185 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 220000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 131.00000 | 195.69800 | 7.040496 | 0.478356 | 0.05 | 2246400 | 3.836300 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 230000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 136.00000 | 203.83000 | 7.343901 | 0.496671 | 0.05 | 2246400 | 3.969415 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 240000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 141.00000 | 211.96200 | 7.647306 | 0.514986 | 0.05 | 2246400 | 4.102530 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 250000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 146.00000 | 220.09400 | 7.950711 | 0.533301 | 0.05 | 2246400 | 4.235645 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 260000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 151.00000 | 228.22600 | 8.254116 | 0.551616 | 0.05 | 2246400 | 4.368760 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 270000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 156.00000 | 236.35800 | 8.557521 | 0.569931 | 0.05 | 2246400 | 4.501875 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 280000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 161.00000 | 244.49000 | 8.860926 | 0.588246 | 0.05 | 2246400 | 4.634990 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 290000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 166.00000 | 252.62200 | 9.164331 | 0.606561 | 0.05 | 2246400 | 4.768105 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 300000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 171.00000 | 260.75400 | 9.467736 | 0.624876 | 0.05 | 2246400 | 4.901220 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 310000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 176.00000 | 268.88600 | 9.771141 | 0.643191 | 0.05 | 2246400 | 5.034335 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 320000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 181.00000 | 277.01800 | 10.074546 | 0.661506 | 0.05 | 2246400 | 5.167450 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 330000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 186.00000 | 285.15000 | 10.377951 | 0.679821 | 0.05 | 2246400 | 5.300565 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 340000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 191.00000 | 293.28200 | 10.681356 | 0.698136 | 0.05 | 2246400 | 5.433680 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 350000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 196.00000 | 301.41400 | 10.984761 | 0.716451 | 0.05 | 2246400 | 5.566795 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 360000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 201.00000 | 309.54600 | 11.288166 | 0.734766 | 0.05 | 2246400 | 5.700000 | 2.68E+08 | 29.89847 | 0.014978 | 29.91445 | 29.91445 |
| 370000 | 29.89847 | 29.89847 | 29.89847 | 0.014978 | 1497900 | 0.748950 | 0 | 0 | 0 | 0 | 748000 | 0.3744 | 2276320 | 206.00000 | | | | | | | | | | | |

| Time year | Initial solids ton | Initial chemical in cell ton | Initial water ton | Initial chemical in water ton | Incoming water from cell above ton | Incoming chemical from above ton | Incoming water from cell below ton | Incoming chemical from below ton | Incoming water from cell above ton | Incoming chemical from above ton | Total water in cell ton | Total chemical in cell ton | Mass on solids ton | Mass in liquids ton | Concentration in solids mg/kg | Concentration in liquids mg/kg | Outgoing liquid to next cell ton | Outgoing chemical to next cell ton | Final solid in cell ton | Final chemical on solid ton | Final chemical in liquid ton | Final chemical in cell ton |
|-----------|--------------------|------------------------------|-------------------|-------------------------------|------------------------------------|----------------------------------|------------------------------------|----------------------------------|------------------------------------|----------------------------------|-------------------------|----------------------------|--------------------|---------------------|-------------------------------|--------------------------------|----------------------------------|------------------------------------|-------------------------|-----------------------------|------------------------------|----------------------------|
| 0 | | | | | | | | | 748000 | 0.3744 | 2.26 | | | | | | 2.68E+08 | | 298947 | 0.014976 | 29.91445 | |
| 10000 | 2.68E+06 | 29.8947 | 29920 | 0.014976 | 22484000 | 1.1222 | 0 | 0 | 748000 | 0.3744 | 30251520 | 31.41205 | 29.8947 | 1.512576 | 0.1125 | 0.05 | 2992000 | 1.4976 | 2.68E+08 | 29.8947 | 0.014976 | 29.91445 |
| 20000 | 2.68E+06 | 29.8947 | 29920 | 0.014976 | 22484000 | 1.307115 | 0 | 0 | 748000 | 0.3744 | 30251520 | 31.89996 | 30.07453 | 1.521433 | 0.113159 | 0.050293 | 2992000 | 1.506369 | 2.68E+08 | 29.8947 | 0.015064 | 30.09958 |
| 30000 | 2.68E+06 | 30.07453 | 29920 | 0.0160364 | 22484000 | 1.65289 | 0 | 0 | 748000 | 0.3744 | 30251520 | 32.31668 | 30.76074 | 1.556146 | 0.116741 | 0.051444 | 2992000 | 1.540739 | 2.68E+08 | 29.8947 | 0.0160364 | 30.77615 |
| 40000 | 2.68E+06 | 30.76074 | 29920 | 0.015407 | 22484000 | 2.927364 | 0 | 0 | 748000 | 0.3744 | 30251520 | 36.09651 | 32.43754 | 1.604973 | 0.12208 | 0.054244 | 2992000 | 1.624726 | 2.68E+08 | 29.8947 | 0.016247 | 32.45378 |
| 50000 | 2.68E+06 | 32.43754 | 29920 | 0.016247 | 22484000 | 4.699996 | 0 | 0 | 748000 | 0.3744 | 30251520 | 39.51778 | 35.11112 | 1.639994 | 0.134967 | 0.059719 | 2992000 | 1.708987 | 2.68E+08 | 29.8947 | 0.017087 | 35.72900 |
| 60000 | 2.68E+06 | 35.11112 | 29920 | 0.017691 | 22484000 | 7.285302 | 0 | 0 | 748000 | 0.3744 | 30251520 | 43.98678 | 41.2996 | 1.659584 | 0.146884 | 0.068634 | 2992000 | 1.808603 | 2.68E+08 | 29.8947 | 0.020286 | 41.32018 |
| 70000 | 2.68E+06 | 41.2996 | 29920 | 0.020686 | 22484000 | 10.85259 | 0 | 0 | 748000 | 0.3744 | 30251520 | 52.54767 | 50.01956 | 1.653074 | 0.160198 | 0.080643 | 2992000 | 2.005271 | 2.68E+08 | 29.8947 | 0.025053 | 50.0436 |
| 80000 | 2.68E+06 | 50.01956 | 29920 | 0.029093 | 22484000 | 15.52285 | 0 | 0 | 748000 | 0.3744 | 30251520 | 65.89995 | 62.75485 | 1.619584 | 0.236189 | 0.104959 | 2992000 | 2.143747 | 2.68E+08 | 29.8947 | 0.031437 | 62.7961 |
| 90000 | 2.68E+06 | 62.75485 | 29920 | 0.031437 | 22484000 | 21.41477 | 0 | 0 | 748000 | 0.3744 | 30251520 | 84.95226 | 80.61226 | 1.402301 | 0.300936 | 0.134639 | 2992000 | 2.332699 | 2.68E+08 | 29.8947 | 0.040237 | 80.65569 |
| 100000 | 2.68E+06 | 80.61226 | 29920 | 0.040237 | 22484000 | 28.64472 | 0 | 0 | 748000 | 0.3744 | 30251520 | 104.2927 | 104.2927 | 1.278033 | 0.389417 | 0.174406 | 2992000 | 2.523796 | 2.68E+08 | 29.8947 | 0.052236 | 104.3449 |
| 110000 | 2.68E+06 | 104.2927 | 29920 | 0.052236 | 22484000 | 37.30566 | 0 | 0 | 748000 | 0.3744 | 30251520 | 142.0279 | 135.1668 | 1.056663 | 0.506663 | 0.226272 | 2992000 | 2.771316 | 2.68E+08 | 29.8947 | 0.067713 | 135.2669 |
| 120000 | 2.68E+06 | 135.1668 | 29920 | 0.067713 | 22484000 | 47.51277 | 0 | 0 | 748000 | 0.3744 | 30251520 | 189.1437 | 174.3249 | 0.810872 | 0.656916 | 0.291518 | 2992000 | 3.091588 | 2.68E+08 | 29.8947 | 0.090731 | 174.4122 |
| 130000 | 2.68E+06 | 174.3249 | 29920 | 0.090731 | 22484000 | 59.34472 | 0 | 0 | 748000 | 0.3744 | 30251520 | 254.1913 | 221.8572 | 0.617406 | 0.838524 | 0.372579 | 2992000 | 3.511624 | 2.68E+08 | 29.8947 | 0.11624 | 222.9689 |
| 140000 | 2.68E+06 | 222.8572 | 29920 | 0.11624 | 22484000 | 72.86602 | 0 | 0 | 748000 | 0.3744 | 30251520 | 336.2315 | 281.9669 | 0.462635 | 1.060931 | 0.471525 | 2992000 | 4.041232 | 2.68E+08 | 29.8947 | 0.145231 | 282.1067 |
| 150000 | 2.68E+06 | 281.9669 | 29920 | 0.145231 | 22484000 | 88.71963 | 0 | 0 | 748000 | 0.3744 | 30251520 | 437.024 | 352.8521 | 0.352821 | 1.377644 | 0.600084 | 2992000 | 4.69326 | 2.68E+08 | 29.8947 | 0.1876736 | 353.0280 |
| 160000 | 2.68E+06 | 352.8521 | 29920 | 0.176736 | 22484000 | 105.4111 | 0 | 0 | 748000 | 0.3744 | 30251520 | 569.8143 | 436.7212 | 0.270936 | 1.843211 | 0.730316 | 2992000 | 5.487442 | 2.68E+08 | 29.8947 | 0.2416744 | 436.9099 |
| 170000 | 2.68E+06 | 436.7212 | 29920 | 0.216944 | 22484000 | 124.5271 | 0 | 0 | 748000 | 0.3744 | 30251520 | 735.8143 | 534.7872 | 0.201293 | 2.505421 | 0.894309 | 2992000 | 6.457633 | 2.68E+08 | 29.8947 | 0.3167633 | 535.0525 |
| 180000 | 2.68E+06 | 534.7872 | 29920 | 0.257493 | 22484000 | 145.6271 | 0 | 0 | 748000 | 0.3744 | 30251520 | 931.0566 | 646.2616 | 0.152974 | 3.439155 | 1.094029 | 2992000 | 7.64204 | 2.68E+08 | 29.8947 | 0.403247 | 646.9065 |
| 190000 | 2.68E+06 | 646.2616 | 29920 | 0.30424 | 22484000 | 168.7855 | 0 | 0 | 748000 | 0.3744 | 30251520 | 1171.2265 | 778.2457 | 0.112825 | 4.592655 | 1.391613 | 2992000 | 9.08921 | 2.68E+08 | 29.8947 | 0.509899 | 778.7407 |
| 200000 | 2.68E+06 | 778.2457 | 29920 | 0.358984 | 22484000 | 193.9114 | 0 | 0 | 748000 | 0.3744 | 30251520 | 1467.2688 | 978.2488 | 0.083773 | 6.148111 | 1.846881 | 2992000 | 10.83979 | 2.68E+08 | 29.8947 | 0.640881 | 978.7124 |
| 210000 | 2.68E+06 | 978.2488 | 29920 | 0.423469 | 22484000 | 221.3469 | 0 | 0 | 748000 | 0.3744 | 30251520 | 1810.435 | 1193.136 | 0.063003 | 8.11304 | 2.482010 | 2992000 | 12.95779 | 2.68E+08 | 29.8947 | 0.804726 | 1193.614 |
| 220000 | 2.68E+06 | 1193.136 | 29920 | 0.514258 | 22484000 | 250.6777 | 0 | 0 | 748000 | 0.3744 | 30251520 | 2340.935 | 1540.173 | 0.046176 | 10.81678 | 3.147096 | 2992000 | 15.41279 | 2.68E+08 | 29.8947 | 0.994711 | 1540.814 |
| 230000 | 2.68E+06 | 1540.173 | 29920 | 0.621121 | 22484000 | 282.6131 | 0 | 0 | 748000 | 0.3744 | 30251520 | 2993.801 | 1888.5 | 0.035013 | 14.606643 | 4.091175 | 2992000 | 18.25276 | 2.68E+08 | 29.8947 | 1.214566 | 1888.244 |
| 240000 | 2.68E+06 | 1888.5 | 29920 | 0.745599 | 22484000 | 316.9564 | 0 | 0 | 748000 | 0.3744 | 30251520 | 3816.205 | 2176.232 | 0.026376 | 19.68796 | 5.297521 | 2992000 | 21.61123 | 2.68E+08 | 29.8947 | 1.471232 | 2176.093 |
| 250000 | 2.68E+06 | 2176.232 | 29920 | 0.881128 | 22484000 | 352.8429 | 0 | 0 | 748000 | 0.3744 | 30251520 | 4873.203 | 2573.193 | 0.019367 | 26.42634 | 7.030154 | 2992000 | 25.61232 | 2.68E+08 | 29.8947 | 1.774446 | 2573.466 |
| 260000 | 2.68E+06 | 2573.193 | 29920 | 1.029462 | 22484000 | 399.5698 | 0 | 0 | 748000 | 0.3744 | 30251520 | 6232.177 | 2952.232 | 0.014375 | 35.424267 | 9.388341 | 2992000 | 30.21894 | 2.68E+08 | 29.8947 | 2.128094 | 2952.466 |
| 270000 | 2.68E+06 | 2952.232 | 29920 | 1.182934 | 22484000 | 432.1534 | 0 | 0 | 748000 | 0.3744 | 30251520 | 7893.918 | 3356.684 | 0.010944 | 47.619424 | 12.37629 | 2992000 | 35.52038 | 2.68E+08 | 29.8947 | 2.526796 | 3356.964 |
| 280000 | 2.68E+06 | 3356.684 | 29920 | 1.353659 | 22484000 | 475.3414 | 0 | 0 | 748000 | 0.3744 | 30251520 | 9936.59 | 3839.56 | 0.008452 | 63.86524 | 16.26669 | 2992000 | 41.6258 | 2.68E+08 | 29.8947 | 2.980166 | 3839.964 |
| 290000 | 2.68E+06 | 3839.56 | 29920 | 1.546299 | 22484000 | 520.8366 | 0 | 0 | 748000 | 0.3744 | 30251520 | 12711.162 | 4325.84 | 0.006209 | 86.2009 | 21.21305 | 2992000 | 48.58201 | 2.68E+08 | 29.8947 | 3.502757 | 4325.964 |
| 300000 | 2.68E+06 | 4325.84 | 29920 | 1.762929 | 22484000 | 569.6791 | 0 | 0 | 748000 | 0.3744 | 30251520 | 16316.623 | 4893.652 | 0.004652 | 113.669 | 28.07511 | 2992000 | 56.51821 | 2.68E+08 | 29.8947 | 4.116771 | 4893.964 |
| 310000 | 2.68E+06 | 4893.652 | 29920 | 1.991871 | 22484000 | 618.0761 | 0 | 0 | 748000 | 0.3744 | 30251520 | 20233.922 | 5494.804 | 0.003438 | 151.2512 | 37.11169 | 2992000 | 65.89209 | 2.68E+08 | 29.8947 | 4.810259 | 5494.171 |
| 320000 | 2.68E+06 | 5494.804 | 29920 | 2.234929 | 22484000 | 671.4321 | 0 | 0 | 748000 | 0.3744 | 30251520 | 25421.916 | 6166.497 | 0.002474 | 194.91429 | 48.71929 | 2992000 | 76.89729 | 2.68E+08 | 29.8947 | 5.59749 | 6166.497 |
| 330000 | 2.68E+06 | 6166.497 | 29920 | 2.491894 | 22484000 | 726.3467 | 0 | 0 | 748000 | 0.3744 | 30251520 | 32044.472 | 6927.689 | 0.001769 | 251.1107 | 63.91623 | 2992000 | 89.81818 | 2.68E+08 | 29.8947 | 6.48418 | 6927.689 |
| 340000 | 2.68E+06 | 6927.689 | 29920 | 2.763181 | 22484000 | 783.6263 | 0 | 0 | 748000 | 0.3744 | 30251520 | 39259.56 | 7762.09 | 0.001269 | 322.62694 | 81.82486 | 2992000 | 104.5759 | 2.68E+08 | 29.8947 | 7.484032 | 7762.09 |
| 350000 | 2.68E+06 | 7762.09 | 29920 | 3.049945 | 22484000 | 843.2569 | 0 | 0 | 748000 | 0.3744 | 30251520 | 48136.436 | 8633.707 | 0.000903 | 414.7316 | 100.0737 | 2992000 | 122.1146 | 2.68E+08 | 29.8947 | 8.60426 | 8633.707 |
| 360000 | 2.68E+06 | 8633.707 | 29920 | 3.3417145 | 22484000 | 905.2443 | 0 | 0 | 748000 | 0.3744 | 30251520 | 59232.343 | 9596.513 | 0.000661 | 531.8123 | 124.62769 | 2992000 | 142.5062 | 2.68E+08 | 29.8947 | 9.85632 | 9596.513 |
| 370000 | 2.68E+06 | 9596.513 | 29920 | 3.639632 | 22484000 | 969.5749 | 0 | 0 | 748000 | 0.3744 | 30251520 | 72717.796 | 10730.612 | 0.000491 | 684.6822 | 151.1781 | 2992000 | 165.9229 | 2.68E+08 | 29.8947 | 11.24633 | 10730.612 |
| 380000 | 2.68E+06 | 10730.612 | 29920 | 3.943332 | 22484000 | 1036.239 | 0 | 0 | 748000 | 0.3744 | 30251520 | 8847.407 | 11927.21 | 0.000362 | 880.217 | 193.1362 | 2992000 | 192.4375 | 2.68E+08 | 29.8947 | 12.78127 | 11927.21 |
| 390000 | 2.68E+06 | 11927.21 | 29920 | 4.252932 | 22484000 | 1105.229 | 0 | 0 | 748000 | 0.3744 | 30251520 | 10699.807 | 13288.31 | 0.000263 | 1134.337 | 250.0881 | 2992000 | 224.1676 | 2.68E+08 | 29.8947 | 14.46174 | 13288.31</ |

| Time year | Initial solids ton | Initial chemical in acid ton | Initial water in water ton | Incoming water from cell above ton | Incoming chemical from cell above ton | Incoming water from side ton | Incoming chemical from side ton | Incoming water from infiltration ton | Incoming chemical from infiltration ton | Total water in cell ton | Total chemical in cell ton | Mass on solids ton | Mass in liquids ton | Concentration in solids mg/kg | Concentration in liquids mg/L | Outgoing liquid to next cell ton | Outgoing chemical to next cell ton | Final liquid in cell ton | Final chemical on solid ton | Final chemical in liquid ton | Final chemical in cell ton | |
|-----------|--------------------|------------------------------|----------------------------|------------------------------------|---------------------------------------|------------------------------|---------------------------------|--------------------------------------|---|-------------------------|----------------------------|--------------------|---------------------|-------------------------------|-------------------------------|----------------------------------|------------------------------------|--------------------------|-----------------------------|------------------------------|----------------------------|----------|
| 0 | | | | | | | | | | | | | | | | | | | | | | |
| 10000 | 2.66E+01 | 29.6947 | 299520 | 0.014975 | 29952000 | 1.4976 | 0 | 7486000 | 0.3744 | 37739520 | 31.7845 | 29.6947 | 1.988976 | 0.1126 | 0.06 | 3744000 | 1.877 | 2.66E+01 | 299520 | 29.6947 | 0.014975 | 29.91445 |
| 20000 | 2.66E+01 | 29.6947 | 299520 | 0.014975 | 29952000 | 1.505369 | 0 | 7489000 | 0.3744 | 37739520 | 31.7922 | 29.6947 | 1.997497 | 0.1126 | 0.06 | 3744000 | 1.87516 | 2.66E+01 | 299520 | 29.6947 | 0.014975 | 29.9277 |
| 30000 | 2.66E+01 | 29.90772 | 299520 | 0.01498 | 29952000 | 1.540739 | 0 | 7486000 | 0.3744 | 37739520 | 31.83764 | 29.84761 | 1.890027 | 0.1126 | 0.06 | 3744000 | 1.876027 | 2.66E+01 | 299520 | 29.84761 | 0.015 | 29.96281 |
| 40000 | 2.66E+01 | 29.47871 | 299520 | 0.01495 | 29952000 | 1.624726 | 0 | 7489000 | 0.3744 | 37739520 | 31.96194 | 30.08454 | 1.697394 | 0.11321 | 0.050276 | 3744000 | 1.882335 | 2.66E+01 | 299520 | 30.08454 | 0.015039 | 30.0796 |
| 50000 | 2.66E+01 | 30.05454 | 299520 | 0.015059 | 29952000 | 1.709697 | 0 | 7490000 | 0.3744 | 37739520 | 32.2427 | 30.32964 | 1.914063 | 0.114116 | 0.050719 | 3744000 | 1.88687 | 2.66E+01 | 299520 | 30.32964 | 0.015191 | 30.34903 |
| 60000 | 2.66E+01 | 30.52664 | 299520 | 0.015191 | 29952000 | 1.806939 | 0 | 7486000 | 0.3744 | 37739520 | 32.58893 | 30.84047 | 1.946365 | 0.115341 | 0.051574 | 3744000 | 1.893916 | 2.66E+01 | 299520 | 30.84047 | 0.01547 | 30.85632 |
| 70000 | 2.66E+01 | 30.84047 | 299520 | 0.015447 | 29952000 | 1.865271 | 0 | 7486000 | 0.3744 | 37739520 | 33.12559 | 31.76529 | 2.002685 | 0.116588 | 0.052066 | 3744000 | 1.906791 | 2.66E+01 | 299520 | 31.76529 | 0.015894 | 31.7488 |
| 80000 | 2.66E+01 | 31.7329 | 299520 | 0.015994 | 29952000 | 1.943747 | 0 | 7486000 | 0.3744 | 37739520 | 33.26934 | 33.17335 | 2.095939 | 0.124818 | 0.055475 | 3744000 | 2.016977 | 2.66E+01 | 299520 | 33.17335 | 0.016616 | 33.18997 |
| 90000 | 2.66E+01 | 33.17335 | 299520 | 0.016616 | 29952000 | 2.032955 | 0 | 7489000 | 0.3744 | 37739520 | 33.69735 | 35.3513 | 2.231918 | 0.133065 | 0.05914 | 3744000 | 2.124304 | 2.66E+01 | 299520 | 35.3513 | 0.01774 | 35.30366 |
| 100000 | 2.66E+01 | 35.3513 | 299520 | 0.01774 | 29952000 | 2.223795 | 0 | 7486000 | 0.3744 | 37739520 | 40.98104 | 36.54264 | 2.432826 | 0.146047 | 0.064463 | 3744000 | 2.214268 | 2.66E+01 | 299520 | 36.54264 | 0.019303 | 36.69252 |
| 110000 | 2.66E+01 | 36.54264 | 299520 | 0.019303 | 29952000 | 2.471318 | 0 | 7486000 | 0.3744 | 37739520 | 45.71326 | 42.99932 | 2.719373 | 0.16179 | 0.071907 | 3744000 | 2.269182 | 2.66E+01 | 299520 | 42.99932 | 0.021536 | 43.02107 |
| 120000 | 2.66E+01 | 42.99932 | 299520 | 0.021536 | 29952000 | 2.731566 | 0 | 7490000 | 0.3744 | 37739520 | 52.12703 | 49.03256 | 3.084478 | 0.18449 | 0.081956 | 3744000 | 2.369919 | 2.66E+01 | 299520 | 49.03256 | 0.024659 | 49.05711 |
| 130000 | 2.66E+01 | 49.03256 | 299520 | 0.024659 | 29952000 | 3.016244 | 0 | 7486000 | 0.3744 | 37739520 | 60.99335 | 56.99884 | 3.697109 | 0.214457 | 0.095314 | 3744000 | 2.566561 | 2.66E+01 | 299520 | 56.99884 | 0.028648 | 57.02539 |
| 140000 | 2.66E+01 | 56.99884 | 299520 | 0.028648 | 29952000 | 3.412312 | 0 | 7486000 | 0.3744 | 37739520 | 71.5229 | 67.277 | 4.246667 | 0.263137 | 0.112605 | 3744000 | 2.7122 | 2.66E+01 | 299520 | 67.277 | 0.033636 | 67.3107 |
| 150000 | 2.66E+01 | 67.277 | 299520 | 0.033636 | 29952000 | 3.76736 | 0 | 7489000 | 0.3744 | 37739520 | 85.3997 | 80.28145 | 5.057248 | 0.302106 | 0.134289 | 3744000 | 2.927032 | 2.66E+01 | 299520 | 80.28145 | 0.040216 | 80.33167 |
| 160000 | 2.66E+01 | 80.28145 | 299520 | 0.040216 | 29952000 | 4.174427 | 0 | 7486000 | 0.3744 | 37739520 | 102.6915 | 96.49308 | 6.069633 | 0.363057 | 0.161369 | 3744000 | 3.140476 | 2.66E+01 | 299520 | 96.49308 | 0.04833 | 96.61479 |
| 170000 | 2.66E+01 | 96.49308 | 299520 | 0.04833 | 29952000 | 4.639639 | 0 | 7489000 | 0.3744 | 37739520 | 123.6919 | 116.3506 | 7.349344 | 0.439704 | 0.19459 | 3744000 | 3.265004 | 2.66E+01 | 299520 | 116.3506 | 0.058021 | 116.4191 |
| 180000 | 2.66E+01 | 116.3506 | 299520 | 0.058021 | 29952000 | 5.173704 | 0 | 7486000 | 0.3744 | 37739520 | 149.2933 | 140.3907 | 8.969065 | 0.528265 | 0.234795 | 3744000 | 3.479033 | 2.66E+01 | 299520 | 140.3907 | 0.070273 | 140.495 |
| 190000 | 2.66E+01 | 140.3907 | 299520 | 0.070273 | 29952000 | 5.782939 | 0 | 7489000 | 0.3744 | 37739520 | 181.8288 | 163.152 | 10.89674 | 0.63846 | 0.282011 | 3744000 | 3.694033 | 2.66E+01 | 299520 | 163.152 | 0.084726 | 163.7385 |
| 200000 | 2.66E+01 | 163.152 | 299520 | 0.084726 | 29952000 | 6.463799 | 0 | 7486000 | 0.3744 | 37739520 | 219.0888 | 203.1929 | 12.92338 | 0.784201 | 0.339778 | 3744000 | 3.921726 | 2.66E+01 | 299520 | 203.1929 | 0.10177 | 203.8555 |
| 210000 | 2.66E+01 | 203.1929 | 299520 | 0.10177 | 29952000 | 7.22079 | 0 | 7486000 | 0.3744 | 37739520 | 269.4127 | 243.0722 | 15.34306 | 0.914565 | 0.406463 | 3744000 | 4.16187 | 2.66E+01 | 299520 | 243.0722 | 0.12175 | 243.914 |
| 220000 | 2.66E+01 | 243.0722 | 299520 | 0.12175 | 29952000 | 8.112599 | 0 | 7489000 | 0.3744 | 37739520 | 337.8895 | 299.4237 | 18.26573 | 1.088993 | 0.483996 | 3744000 | 4.42076 | 2.66E+01 | 299520 | 299.4237 | 0.148966 | 299.6587 |
| 230000 | 2.66E+01 | 299.4237 | 299520 | 0.148966 | 29952000 | 9.145574 | 0 | 7486000 | 0.3744 | 37739520 | 364.4999 | 342.6071 | 21.63011 | 1.290061 | 0.573356 | 3744000 | 4.69444 | 2.66E+01 | 299520 | 342.6071 | 0.171732 | 343.0234 |
| 240000 | 2.66E+01 | 342.6071 | 299520 | 0.171732 | 29952000 | 10.31261 | 0 | 7489000 | 0.3744 | 37739520 | 450.5195 | 404.9216 | 25.49907 | 1.520714 | 0.675633 | 3744000 | 4.97297 | 2.66E+01 | 299520 | 404.9216 | 0.202366 | 404.2230 |
| 250000 | 2.66E+01 | 404.9216 | 299520 | 0.202366 | 29952000 | 11.748024 | 0 | 7486000 | 0.3744 | 37739520 | 553.4444 | 473.5578 | 29.86628 | 1.781913 | 0.791917 | 3744000 | 5.264956 | 2.66E+01 | 299520 | 473.5578 | 0.237195 | 473.795 |
| 260000 | 2.66E+01 | 473.5578 | 299520 | 0.237195 | 29952000 | 13.40804 | 0 | 7489000 | 0.3744 | 37739520 | 685.9789 | 562.1334 | 34.84851 | 2.077462 | 0.923916 | 3744000 | 5.56988 | 2.66E+01 | 299520 | 562.1334 | 0.276557 | 562.8098 |
| 270000 | 2.66E+01 | 562.1334 | 299520 | 0.276557 | 29952000 | 15.28036 | 0 | 7486000 | 0.3744 | 37739520 | 840.8301 | 640.4207 | 40.41739 | 2.408622 | 1.079597 | 3744000 | 6.049661 | 2.66E+01 | 299520 | 640.4207 | 0.320773 | 640.7415 |
| 280000 | 2.66E+01 | 640.4207 | 299520 | 0.320773 | 29952000 | 17.446289 | 0 | 7489000 | 0.3744 | 37739520 | 1036.7447 | 738.0897 | 46.54463 | 2.780943 | 1.236594 | 3744000 | 6.274487 | 2.66E+01 | 299520 | 738.0897 | 0.370189 | 739.4689 |
| 290000 | 2.66E+01 | 738.0897 | 299520 | 0.370189 | 29952000 | 19.92628 | 0 | 7486000 | 0.3744 | 37739520 | 1302.4721 | 848.8622 | 53.67193 | 3.19391 | 1.419515 | 3744000 | 6.314666 | 2.66E+01 | 299520 | 848.8622 | 0.425173 | 849.290 |
| 300000 | 2.66E+01 | 848.8622 | 299520 | 0.425173 | 29952000 | 22.813617 | 0 | 7489000 | 0.3744 | 37739520 | 1591.6117 | 970.3759 | 61.24106 | 3.651143 | 1.622773 | 3744000 | 6.269033 | 2.66E+01 | 299520 | 970.3759 | 0.483004 | 970.8615 |
| 310000 | 2.66E+01 | 970.3759 | 299520 | 0.483004 | 29952000 | 26.230399 | 0 | 7486000 | 0.3744 | 37739520 | 1974.0495 | 1104.39 | 83.86326 | 4.155225 | 1.846771 | 3744000 | 6.1431 | 2.66E+01 | 299520 | 1104.39 | 0.553145 | 1104.903 |
| 320000 | 2.66E+01 | 1104.39 | 299520 | 0.553145 | 29952000 | 30.29197 | 0 | 7489000 | 0.3744 | 37739520 | 2420.447 | 1251.487 | 99.18967 | 4.789785 | 2.092769 | 3744000 | 5.914803 | 2.66E+01 | 299520 | 1251.487 | 0.638923 | 1252.093 |
| 330000 | 2.66E+01 | 1251.487 | 299520 | 0.638923 | 29952000 | 35.03816 | 0 | 7486000 | 0.3744 | 37739520 | 2951.544 | 1412.63 | 119.3448 | 5.514348 | 2.361033 | 3744000 | 5.584375 | 2.66E+01 | 299520 | 1412.63 | 0.737445 | 1413.118 |
| 340000 | 2.66E+01 | 1412.63 | 299520 | 0.737445 | 29952000 | 40.59455 | 0 | 7489000 | 0.3744 | 37739520 | 3589.687 | 1587.089 | 139.1113 | 6.374517 | 2.652341 | 3744000 | 5.14166 | 2.66E+01 | 299520 | 1587.089 | 0.863816 | 1589.561 |
| 350000 | 2.66E+01 | 1587.089 | 299520 | 0.863816 | 29952000 | 47.91145 | 0 | 7486000 | 0.3744 | 37739520 | 4390.755 | 1778.607 | 170.2408 | 7.324066 | 2.974145 | 3744000 | 4.11132 | 2.66E+01 | 299520 | 1778.607 | 0.983816 | 1780.396 |
| 360000 | 2.66E+01 | 1778.607 | 299520 | 0.983816 | 29952000 | 56.30562 | 0 | 7489000 | 0.3744 | 37739520 | 5361.279 | 1965.004 | 215.7449 | 8.466791 | 3.319493 | 3744000 | 3.24287 | 2.66E+01 | 299520 | 1965.004 | 1.109425 | 1965.999 |
| 370000 | 2.66E+01 | 1965.004 | 299520 | 1.109425 | 29952000 | 65.99222 | 0 | 7486000 | 0.3744 | 37739520 | 6478.813 | 2205.019 | 251.3493 | 9.307956 | 3.692386 | 3744000 | 2.362434 | 2.66E+01 | 299520 | 2205.019 | 1.256947 | 2205.121 |
| 380000 | 2.66E+01 | 2205.019 | 299520 | 1.256947 | 29952000 | 77.03232 | 0 | 7489000 | 0.3744 | 37739520 | 7802.699 | 2448.195 | 314.507 | 9.211586 | 4.054038 | 3744000 | 1.932806 | 2.66E+01 | 299520 | 2448.195 | 1.426245 | 2449.418 |
| 390000 | 2.66E+01 | 2448.195 | 299520 | 1.426245 | 29952000 | 89.5776 | 0 | 7486000 | 0.3744 | | | | | | | | | | | | | |

| Time year | Initial solid ton | Initial chemical in solid ton | Initial water ton | Initial chemical in water ton | Incoming water from cell above ton | Incoming chemical from cell above ton | Incoming water from side ton | Incoming chemical from side ton | Incoming water from infiltration ton | Incoming chemical from infiltration ton | Total water in cell ton | Total chemical in cell ton | Mass on solids ton | Mass in liq. ton | Concentration in liq. mg/kg | Concentration in liq. mg/kg | Outgoing liquid to next cell ton | Outgoing chemical to next cell ton | Final solid ton | Final chemical in solid ton | Final water ton | Final chemical in water ton | Final chemical in liq. ton | Final chemical in cell ton | |
|-----------|-------------------|-------------------------------|-------------------|-------------------------------|------------------------------------|---------------------------------------|------------------------------|---------------------------------|--------------------------------------|---|-------------------------|----------------------------|--------------------|------------------|-----------------------------|-----------------------------|----------------------------------|------------------------------------|-----------------|-----------------------------|-----------------|-----------------------------|----------------------------|----------------------------|----------|
| 0 | | | | | | | | | | | 500000 | 0.166 | | | 0.09 | 0.03 | | | | | | | | | |
| 10000 | 166256 | 0.10463 | 187200 | 0.005516 | 120640000 | 68.91665 | 2.495E+10 | 715.1731 | 5000000 | 0.15876255027200 | 704.3654 | 0.10453 | 704.2618 | 0.089638 | 0.029669 | 2.626E+10 | 704.2463 | 166256 | 0.10453 | 187200 | 0.005516 | 120640000 | 68.91665 | 2.495E+10 | 715.1731 |
| 20000 | 166256 | 0.10456 | 187200 | 0.005559 | 120640000 | 68.91662 | 2.495E+10 | 715.1731 | 5000000 | 0.15876255027200 | 704.3679 | 0.10452 | 704.2634 | 0.089638 | 0.029669 | 2.626E+10 | 704.2470 | 166256 | 0.10452 | 187200 | 0.005559 | 120640000 | 68.91662 | 2.495E+10 | 715.1731 |
| 30000 | 166256 | 0.10450 | 187200 | 0.005532 | 120640000 | 68.92113 | 2.495E+10 | 715.1731 | 5000000 | 0.15876255027200 | 704.3604 | 0.10457 | 704.2559 | 0.089638 | 0.02967 | 2.626E+10 | 704.2503 | 166256 | 0.10450 | 187200 | 0.005532 | 120640000 | 68.92113 | 2.495E+10 | 715.1731 |
| 40000 | 166256 | 0.10452 | 187200 | 0.005552 | 120640000 | 68.92843 | 2.495E+10 | 715.1731 | 5000000 | 0.15876255027200 | 704.3677 | 0.10453 | 704.2632 | 0.08961 | 0.02967 | 2.626E+10 | 704.2576 | 166256 | 0.10452 | 187200 | 0.005552 | 120640000 | 68.92843 | 2.495E+10 | 715.1731 |
| 50000 | 166256 | 0.10450 | 187200 | 0.005522 | 120640000 | 68.94433 | 2.495E+10 | 715.1731 | 5000000 | 0.15876255027200 | 704.3642 | 0.10451 | 704.2717 | 0.089611 | 0.02967 | 2.626E+10 | 704.2741 | 166256 | 0.10450 | 187200 | 0.005522 | 120640000 | 68.94433 | 2.495E+10 | 715.1731 |
| 60000 | 166256 | 0.10451 | 187200 | 0.005522 | 120640000 | 68.97994 | 2.495E+10 | 715.1731 | 5000000 | 0.15876255027200 | 704.4162 | 0.10454 | 704.3117 | 0.089615 | 0.02967 | 2.626E+10 | 704.3017 | 166256 | 0.10451 | 187200 | 0.005522 | 120640000 | 68.97994 | 2.495E+10 | 715.1731 |
| 70000 | 166256 | 0.10451 | 187200 | 0.005522 | 120640000 | 68.10374 | 2.495E+10 | 715.1731 | 5000000 | 0.15876255027200 | 704.4721 | 0.10452 | 704.3675 | 0.089621 | 0.02967 | 2.626E+10 | 704.3519 | 166256 | 0.10451 | 187200 | 0.005522 | 120640000 | 68.10374 | 2.495E+10 | 715.1731 |
| 80000 | 166256 | 0.10452 | 187200 | 0.005522 | 120640000 | 69.12293 | 2.495E+10 | 715.1731 | 5000000 | 0.15876255027200 | 704.4971 | 0.10454 | 704.4778 | 0.089632 | 0.02967 | 2.626E+10 | 704.452 | 166256 | 0.10452 | 187200 | 0.005522 | 120640000 | 69.12293 | 2.495E+10 | 715.1731 |
| 90000 | 166256 | 0.10453 | 187200 | 0.005522 | 120640000 | 69.22592 | 2.495E+10 | 715.1731 | 5000000 | 0.15876255027200 | 704.4992 | 0.10452 | 704.4946 | 0.089647 | 0.02967 | 2.626E+10 | 704.4599 | 166256 | 0.10453 | 187200 | 0.005522 | 120640000 | 69.22592 | 2.495E+10 | 715.1731 |
| 100000 | 166256 | 0.10452 | 187200 | 0.005534 | 120640000 | 69.42604 | 2.495E+10 | 715.1731 | 5000000 | 0.15876255027200 | 704.4993 | 0.10458 | 704.4926 | 0.089657 | 0.02967 | 2.626E+10 | 704.4602 | 166256 | 0.10452 | 187200 | 0.005534 | 120640000 | 69.42604 | 2.495E+10 | 715.1731 |
| 110000 | 166256 | 0.10457 | 187200 | 0.00563 | 120640000 | 69.73751 | 2.495E+10 | 715.1731 | 5000000 | 0.15876255027200 | 706.1728 | 0.10415 | 705.0722 | 0.089702 | 0.02969 | 2.626E+10 | 706.1668 | 166256 | 0.10457 | 187200 | 0.00563 | 120640000 | 69.73751 | 2.495E+10 | 715.1731 |
| 120000 | 166256 | 0.10451 | 187200 | 0.005522 | 120640000 | 70.11495 | 2.495E+10 | 715.1731 | 5000000 | 0.15876255027200 | 706.5543 | 0.10465 | 705.4486 | 0.089745 | 0.029915 | 2.626E+10 | 706.444 | 166256 | 0.10451 | 187200 | 0.005522 | 120640000 | 70.11495 | 2.495E+10 | 715.1731 |
| 130000 | 166256 | 0.10468 | 187200 | 0.0058 | 120640000 | 70.61325 | 2.495E+10 | 715.1731 | 5000000 | 0.15876255027200 | 706.0527 | 0.10473 | 705.9479 | 0.089802 | 0.029934 | 2.626E+10 | 706.9423 | 166256 | 0.10468 | 187200 | 0.0058 | 120640000 | 70.61325 | 2.495E+10 | 715.1731 |
| 140000 | 166256 | 0.10473 | 187200 | 0.00594 | 120640000 | 71.25647 | 2.495E+10 | 715.1731 | 5000000 | 0.15876255027200 | 706.786 | 0.10481 | 706.6911 | 0.089875 | 0.029995 | 2.626E+10 | 706.6955 | 166256 | 0.10473 | 187200 | 0.00594 | 120640000 | 71.25647 | 2.495E+10 | 715.1731 |
| 150000 | 166256 | 0.10481 | 187200 | 0.00608 | 120640000 | 72.07082 | 2.495E+10 | 715.1731 | 5000000 | 0.15876255027200 | 707.6104 | 0.10492 | 707.4026 | 0.089869 | 0.02998 | 2.626E+10 | 707.3968 | 166256 | 0.10481 | 187200 | 0.00608 | 120640000 | 72.07082 | 2.495E+10 | 715.1731 |
| 160000 | 166256 | 0.10482 | 187200 | 0.00614 | 120640000 | 73.08449 | 2.495E+10 | 715.1731 | 5000000 | 0.15876255027200 | 708.6242 | 0.10501 | 708.4191 | 0.089904 | 0.030025 | 2.626E+10 | 708.4135 | 166256 | 0.10482 | 187200 | 0.00614 | 120640000 | 73.08449 | 2.495E+10 | 715.1731 |
| 170000 | 166256 | 0.10506 | 187200 | 0.00621 | 120640000 | 74.32763 | 2.495E+10 | 715.1731 | 5000000 | 0.15876255027200 | 709.1755 | 0.10527 | 709.6822 | 0.090226 | 0.030075 | 2.626E+10 | 709.6856 | 166256 | 0.10506 | 187200 | 0.00621 | 120640000 | 74.32763 | 2.495E+10 | 715.1731 |
| 180000 | 166256 | 0.10527 | 187200 | 0.00653 | 120640000 | 76.03715 | 2.495E+10 | 715.1731 | 5000000 | 0.15876255027200 | 711.2721 | 0.10542 | 710.9657 | 0.090396 | 0.030133 | 2.626E+10 | 711.1611 | 166256 | 0.10527 | 187200 | 0.00653 | 120640000 | 76.03715 | 2.495E+10 | 715.1731 |
| 190000 | 166256 | 0.10542 | 187200 | 0.00664 | 120640000 | 77.63166 | 2.495E+10 | 715.1731 | 5000000 | 0.15876255027200 | 713.0719 | 0.10557 | 712.9662 | 0.090604 | 0.030201 | 2.626E+10 | 712.9608 | 166256 | 0.10542 | 187200 | 0.00664 | 120640000 | 77.63166 | 2.495E+10 | 715.1731 |
| 200000 | 166256 | 0.10567 | 187200 | 0.00664 | 120640000 | 79.76132 | 2.495E+10 | 715.1731 | 5000000 | 0.15876255027200 | 715.2016 | 0.10581 | 715.0958 | 0.091047 | 0.030282 | 2.626E+10 | 715.0902 | 166256 | 0.10567 | 187200 | 0.00664 | 120640000 | 79.76132 | 2.495E+10 | 715.1731 |
| 210000 | 166256 | 0.10581 | 187200 | 0.00668 | 120640000 | 82.87589 | 2.495E+10 | 715.1731 | 5000000 | 0.15876255027200 | 717.6965 | 0.10605 | 717.5927 | 0.091152 | 0.030377 | 2.626E+10 | 717.5855 | 166256 | 0.10581 | 187200 | 0.00668 | 120640000 | 82.87589 | 2.495E+10 | 715.1731 |
| 220000 | 166256 | 0.10574 | 187200 | 0.00657 | 120640000 | 85.15529 | 2.495E+10 | 715.1731 | 5000000 | 0.15876255027200 | 720.4993 | 0.10629 | 720.4993 | 0.091164 | 0.030486 | 2.626E+10 | 720.4993 | 166256 | 0.10574 | 187200 | 0.00657 | 120640000 | 85.15529 | 2.495E+10 | 715.1731 |
| 230000 | 166256 | 0.10587 | 187200 | 0.0067 | 120640000 | 89.6103 | 2.495E+10 | 715.1731 | 5000000 | 0.15876255027200 | 803.9446 | 0.10716 | 803.9446 | 0.091946 | 0.030615 | 2.626E+10 | 803.9446 | 166256 | 0.10587 | 187200 | 0.0067 | 120640000 | 89.6103 | 2.495E+10 | 715.1731 |
| 240000 | 166256 | 0.10716 | 187200 | 0.00731 | 120640000 | 92.33008 | 2.495E+10 | 715.1731 | 5000000 | 0.15876255027200 | 807.7728 | 0.10726 | 807.6622 | 0.092293 | 0.030751 | 2.626E+10 | 807.6695 | 166256 | 0.10716 | 187200 | 0.00731 | 120640000 | 92.33008 | 2.495E+10 | 715.1731 |
| 250000 | 166256 | 0.10726 | 187200 | 0.00756 | 120640000 | 96.69304 | 2.495E+10 | 715.1731 | 5000000 | 0.15876255027200 | 812.1226 | 0.10825 | 812.0174 | 0.092701 | 0.030922 | 2.626E+10 | 812.0118 | 166256 | 0.10726 | 187200 | 0.00756 | 120640000 | 96.69304 | 2.495E+10 | 715.1731 |
| 260000 | 166256 | 0.10826 | 187200 | 0.00767 | 120640000 | 101.601 | 2.495E+10 | 715.1731 | 5000000 | 0.15876255027200 | 817.0442 | 0.10861 | 817.0442 | 0.093343 | 0.031114 | 2.626E+10 | 817.0442 | 166256 | 0.10826 | 187200 | 0.00767 | 120640000 | 101.601 | 2.495E+10 | 715.1731 |
| 270000 | 166256 | 0.10861 | 187200 | 0.00825 | 120640000 | 107.1269 | 2.495E+10 | 715.1731 | 5000000 | 0.15876255027200 | 822.5708 | 0.10968 | 822.4622 | 0.093974 | 0.031325 | 2.626E+10 | 822.4653 | 166256 | 0.10861 | 187200 | 0.00825 | 120640000 | 107.1269 | 2.495E+10 | 715.1731 |
| 280000 | 166256 | 0.10969 | 187200 | 0.00864 | 120640000 | 113.3034 | 2.495E+10 | 715.1731 | 5000000 | 0.15876255027200 | 828.748 | 0.11042 | 828.6375 | 0.09449 | 0.03155 | 2.626E+10 | 828.6316 | 166256 | 0.10969 | 187200 | 0.00864 | 120640000 | 113.3034 | 2.495E+10 | 715.1731 |
| 290000 | 166256 | 0.11042 | 187200 | 0.00908 | 120640000 | 120.1732 | 2.495E+10 | 715.1731 | 5000000 | 0.15876255027200 | 835.8166 | 0.11139 | 835.6707 | 0.09465 | 0.031822 | 2.626E+10 | 835.6707 | 166256 | 0.11042 | 187200 | 0.00908 | 120640000 | 120.1732 | 2.495E+10 | 715.1731 |
| 300000 | 166256 | 0.11139 | 187200 | 0.00937 | 120640000 | 127.7794 | 2.495E+10 | 715.1731 | 5000000 | 0.15876255027200 | 843.298 | 0.11236 | 843.1136 | 0.095334 | 0.032111 | 2.626E+10 | 843.1075 | 166256 | 0.11139 | 187200 | 0.00937 | 120640000 | 127.7794 | 2.495E+10 | 715.1731 |
| 310000 | 166256 | 0.11235 | 187200 | 0.00971 | 120640000 | 136.1553 | 2.495E+10 | 715.1731 | 5000000 | 0.15876255027200 | 851.6728 | 0.11347 | 851.4972 | 0.096292 | 0.032431 | 2.626E+10 | 851.4932 | 166256 | 0.11235 | 187200 | 0.00971 | 120640000 | 136.1553 | 2.495E+10 | 715.1731 |
| 320000 | 166256 | 0.11347 | 187200 | 0.01018 | 120640000 | 145.2708 | 2.495E+10 | 715.1731 | 5000000 | 0.15876255027200 | 860.6971 | 0.11464 | 860.7078 | 0.097344 | 0.032778 | 2.626E+10 | 860.7017 | 166256 | 0.11347 | 187200 | 0.01018 | 120640000 | 145.2708 | 2.495E+10 | 715.1731 |
| 330000 | 166256 | 0.11464 | 18720 | | | | | | | | | | | | | | | | | | | | | | |

| Time year | Initial solids ton | Initial chemical in solid ton | Initial water ton | Initial chemical in water ton | Initial water above cell ton | Incoming chemical from cell above | Incoming water from side ton | Incoming chemical from side ton | Incoming water infiltration ton | Incoming chemical infiltration ton | Total water in cell ton | Total chemical in cell ton | Mass on solids ton | Mass in liquids ton | Concentration in solids mg/kg | Concentration in liquids mg/L | Outgoing liquid to next cell tons | Outgoing chemical to next cell tons | Final solid in cell tons | Final liquid in cell tons | Final chemical on solid tons | Final chemical in liquid tons | Final chemical in cell tons | | | |
|-----------|--------------------|-------------------------------|-------------------|-------------------------------|------------------------------|-----------------------------------|------------------------------|---------------------------------|---------------------------------|------------------------------------|-------------------------|----------------------------|--------------------|---------------------|-------------------------------|-------------------------------|-----------------------------------|-------------------------------------|--------------------------|---------------------------|------------------------------|-------------------------------|-----------------------------|---|---|---|
| 0 | 0 | 0 | 0 | 0 | 0 | 0.029069 | 3.28E+11 | 1193.444 | 0 | 0 | 0.005578 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| 10000 | 0 | 0 | 624000 | 0.003494 | 2.63E+10 | 784.2478 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 1974.696 | 0 | 1974.696 | 0 | 0.005578 | 3.54E+11 | 1974.696 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | |
| 20000 | 0 | 0 | 624000 | 0.003481 | 2.63E+10 | 784.2478 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 1973.696 | 0 | 1973.696 | 0 | 0.005578 | 3.54E+11 | 1973.696 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 30000 | 0 | 0 | 624000 | 0.003491 | 2.63E+10 | 784.2493 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 1973.696 | 0 | 1973.696 | 0 | 0.005578 | 3.54E+11 | 1973.696 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 40000 | 0 | 0 | 624000 | 0.003481 | 2.63E+10 | 784.2576 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 1973.705 | 0 | 1973.705 | 0 | 0.005578 | 3.54E+11 | 1973.705 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 50000 | 0 | 0 | 624000 | 0.003491 | 2.63E+10 | 784.2711 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 1973.722 | 0 | 1973.722 | 0 | 0.005578 | 3.54E+11 | 1973.722 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 60000 | 0 | 0 | 624000 | 0.003481 | 2.63E+10 | 784.3361 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 1973.754 | 0 | 1973.754 | 0 | 0.005578 | 3.54E+11 | 1973.754 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 70000 | 0 | 0 | 624000 | 0.003481 | 2.63E+10 | 784.3819 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 1973.811 | 0 | 1973.811 | 0 | 0.005578 | 3.54E+11 | 1973.811 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 80000 | 0 | 0 | 624000 | 0.003481 | 2.63E+10 | 784.452 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 1973.9 | 0 | 1973.9 | 0 | 0.005578 | 3.54E+11 | 1973.9 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 90000 | 0 | 0 | 624000 | 0.003481 | 2.63E+10 | 784.589 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 1974.037 | 0 | 1974.037 | 0 | 0.005578 | 3.54E+11 | 1974.037 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 100000 | 0 | 0 | 624000 | 0.003482 | 2.63E+10 | 784.7862 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 1974.236 | 0 | 1974.236 | 0 | 0.005578 | 3.54E+11 | 1974.236 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 110000 | 0 | 0 | 624000 | 0.003482 | 2.63E+10 | 785.0566 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 1974.514 | 0 | 1974.514 | 0 | 0.005578 | 3.54E+11 | 1974.514 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 120000 | 0 | 0 | 624000 | 0.003482 | 2.63E+10 | 786.444 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 1974.892 | 0 | 1974.892 | 0 | 0.005578 | 3.54E+11 | 1974.892 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 130000 | 0 | 0 | 624000 | 0.003483 | 2.63E+10 | 785.9423 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 1976.39 | 0 | 1976.39 | 0 | 0.005578 | 3.54E+11 | 1976.39 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 140000 | 0 | 0 | 624000 | 0.003484 | 2.63E+10 | 786.5265 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 1976.033 | 0 | 1976.033 | 0 | 0.005578 | 3.54E+11 | 1976.033 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 150000 | 0 | 0 | 624000 | 0.003485 | 2.63E+10 | 787.3999 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 1976.848 | 0 | 1976.848 | 0 | 0.005578 | 3.54E+11 | 1976.848 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 160000 | 0 | 0 | 624000 | 0.003487 | 2.63E+10 | 788.4135 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 1977.851 | 0 | 1977.851 | 0 | 0.005578 | 3.54E+11 | 1977.851 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 170000 | 0 | 0 | 624000 | 0.003488 | 2.63E+10 | 789.6566 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 1980.609 | 0 | 1980.609 | 0 | 0.005578 | 3.54E+11 | 1980.609 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 180000 | 0 | 0 | 624000 | 0.003489 | 2.63E+10 | 791.8111 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 1986.808 | 0 | 1986.808 | 0 | 0.005578 | 3.54E+11 | 1986.808 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 190000 | 0 | 0 | 624000 | 0.003493 | 2.63E+10 | 792.8636 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 1992.478 | 0 | 1992.478 | 0 | 0.005578 | 3.54E+11 | 1992.478 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 200000 | 0 | 0 | 624000 | 0.003495 | 2.63E+10 | 795.0682 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 1994.536 | 0 | 1994.536 | 0 | 0.005578 | 3.54E+11 | 1994.536 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 210000 | 0 | 0 | 624000 | 0.0035 | 2.63E+10 | 797.5865 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 1997.034 | 0 | 1997.034 | 0 | 0.005578 | 3.54E+11 | 1997.034 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 220000 | 0 | 0 | 624000 | 0.003505 | 2.63E+10 | 800.4873 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 1999.935 | 0 | 1999.935 | 0 | 0.005578 | 3.54E+11 | 1999.935 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 230000 | 0 | 0 | 624000 | 0.00351 | 2.63E+10 | 803.8317 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 1993.28 | 0 | 1993.28 | 0 | 0.005578 | 3.54E+11 | 1993.28 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 240000 | 0 | 0 | 624000 | 0.003516 | 2.63E+10 | 807.6995 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 1997.107 | 0 | 1997.107 | 0 | 0.005578 | 3.54E+11 | 1997.107 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 250000 | 0 | 0 | 624000 | 0.003522 | 2.63E+10 | 812.0116 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 2001.459 | 0 | 2001.459 | 0 | 0.005578 | 3.54E+11 | 2001.459 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 260000 | 0 | 0 | 624000 | 0.00353 | 2.63E+10 | 816.9295 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 2006.377 | 0 | 2006.377 | 0 | 0.005578 | 3.54E+11 | 2006.377 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 270000 | 0 | 0 | 624000 | 0.003539 | 2.63E+10 | 822.4563 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 2011.303 | 0 | 2011.303 | 0 | 0.005578 | 3.54E+11 | 2011.303 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 280000 | 0 | 0 | 624000 | 0.003548 | 2.63E+10 | 828.6316 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 2018.08 | 0 | 2018.08 | 0 | 0.005578 | 3.54E+11 | 2018.08 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 290000 | 0 | 0 | 624000 | 0.003559 | 2.63E+10 | 835.5013 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 2024.949 | 0 | 2024.949 | 0 | 0.005578 | 3.54E+11 | 2024.949 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 300000 | 0 | 0 | 624000 | 0.003574 | 2.63E+10 | 843.1076 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 2032.656 | 0 | 2032.656 | 0 | 0.005578 | 3.54E+11 | 2032.656 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 310000 | 0 | 0 | 624000 | 0.003586 | 2.63E+10 | 851.4522 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 2040.941 | 0 | 2040.941 | 0 | 0.005578 | 3.54E+11 | 2040.941 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 320000 | 0 | 0 | 624000 | 0.003598 | 2.63E+10 | 860.7017 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 2050.15 | 0 | 2050.15 | 0 | 0.005578 | 3.54E+11 | 2050.15 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 330000 | 0 | 0 | 624000 | 0.003616 | 2.63E+10 | 870.7758 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 2060.224 | 0 | 2060.224 | 0 | 0.005578 | 3.54E+11 | 2060.224 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 340000 | 0 | 0 | 624000 | 0.003634 | 2.63E+10 | 881.7893 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 2071.206 | 0 | 2071.206 | 0 | 0.005578 | 3.54E+11 | 2071.206 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 350000 | 0 | 0 | 624000 | 0.003663 | 2.63E+10 | 893.6915 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 2083.14 | 0 | 2083.14 | 0 | 0.005578 | 3.54E+11 | 2083.14 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 360000 | 0 | 0 | 624000 | 0.003674 | 2.63E+10 | 906.6172 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 2096.065 | 0 | 2096.065 | 0 | 0.005578 | 3.54E+11 | 2096.065 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 370000 | 0 | 0 | 624000 | 0.003697 | 2.63E+10 | 920.5768 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 2110.025 | 0 | 2110.025 | 0 | 0.005578 | 3.54E+11 | 2110.025 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 380000 | 0 | 0 | 624000 | 0.003721 | 2.63E+10 | 936.611 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 2125.069 | 0 | 2125.069 | 0 | 0.005578 | 3.54E+11 | 2125.069 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 390000 | 0 | 0 | 624000 | 0.003748 | 2.63E+10 | 951.7897 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 2141.208 | 0 | 2141.208 | 0 | 0.005578 | 3.54E+11 | 2141.208 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 400000 | 0 | 0 | 624000 | 0.003776 | 2.63E+10 | 969.0522 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 2158.51 | 0 | 2158.51 | 0 | 0.005578 | 3.54E+11 | 2158.51 | 0 | 624000 | 0 | 0 | 0 | 0 | 0 | 0 |
| 410000 | 0 | 0 | 624000 | 0.003807 | 2.63E+10 | 987.6567 | 3.28E+11 | 1193.444 | 0 | 0 | 353804497280 | 217 | | | | | | | | | | | | | | |